

Depth Dependent Fault Zone Damage in 3D Simulations of Dynamic Rupture on a frictional fault with brittle Damage Breakage Rheology in the bulk Progress Report

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1 Background

Earthquakes and fault zones exhibit complex multi-scale, multi-phase interactions that govern source physics but remain poorly understood. Fault damage zones influence nucleation, rupture propagation, energy partitioning, and arrest, while earthquakes in turn generate co-seismic off-fault damage that modifies fault zone geometry, elasticity, and rheology. The understanding of this co-evolution is hindered by sparse near-fault observations: seismic and geodetic inversions rely on far-field data and linear elastic assumptions that cannot resolve near-fault inelastic response or fine-scale heterogeneity. Furthermore, depth-dependent variations in overburden stress, pore pressure, and seismic properties (V_s , V_p , ρ) likely exert first-order controls on rupture dynamics, ground motion, and low-velocity zone evolution.

Field and high-resolution studies report non-unique damage-zone structures. Part of this disagreement reflects definitional inconsistency: damage zone is defined by seismicity distribution, low-velocity fault zones from tomography, or fracture density from geology, and part reflects genuine hierarchical structure across scales. Reconciling these observations requires 3D physics-based modeling, yet existing 3D fault-zone simulations almost exclusively use elastoplastic rheology, which cannot capture the elastic-modulus reductions documented in lab experiments and field studies. The few 3D damage-rheology models are either quasi-static or use depth-invariant stress profiles, and prior 2D plane strain studies cannot represent stress redistribution and rupture-front distortion that arise from non-uniform damage across depth.

We perform 3D dynamic rupture simulations on a preexisting fault governed by linear slip-weakening friction, with off-fault response described by a continuum damage-breakage (CDB) rheology that tracks both cracking and granulation state variables, captures elastic-modulus evolution, and transitions spontaneously to granular flow at critical damage. The simulations consider effects with depth-dependent properties and strain rate dependent damage accumulation. This framework lets us examine how damage-zone structures evolve during rupture, identify the controlling factors behind their variability, and connect the simulations to field observations of fault damage architecture.

2 Problem Setup

A static solver establishes initial equilibrium and resolves the depth-dependent stress gradient, dynamic solver then uses the resultant field as initial condition for dynamic rupture simulation. As shown in Figure 1[1], boundary traction T is applied consistent with the prescribed stress field, while an eigenstrain field converted from the initial stress guides the system toward the target solution; rigid body motion is eliminated by constraining the four corner points in all directions and fixing the bottom boundary in z . The procedure and the resultant fields are verified against the SCEC TPV26 benchmark. Figure 1[2] shows the resulting depth profiles of seismic properties (V_s , V_p , ρ), effective stress (σ'), and the initial strain invariant ratio $\xi(t = 0)$ for three cases. Case 1 (baseline) uses depth-constant seismic properties and a linearly varying effective stress down to 15 km, yielding linearly depth-varying on-fault shear stress and strength and a depth-uniform $\xi(t = 0)$. Case 2 introduces an overpressurized zone

between 7–15 km, producing depth-constant effective normal and on-fault shear stresses within that interval. Case 3 adopts a 1D velocity structure with reduced seismic properties near the free surface (following SCEC Benchmark TPV32), yielding a depth-varying $\xi(t = 0)$ that, as shown later, exerts a deterministic influence on the off-fault damage pattern. The problem setup is summarized in Table 1.

Case	Pore Pressure Condition	Material Properties	Notes
1	Constant hydrostatic pore pressure	Constant with depth (uniform)	Baseline reference case
2	Hydrostatic-to-lithostatic transition	Constant with depth (uniform)	Effect of pore-pressure transition
3	Constant hydrostatic pore pressure	1D velocity structure (depth-dependent)	Effect of seismic property variation

Table 1: Summary of simulation cases considered in this study.

3 Results

3.1 3D Damage pattern and spatial heterogeneity

Figure 3 presents selected time snapshots of off-fault damage evolution, where the gray surfaces denote 2D fault plane and iso-contours of high breakage state ($B > 0.8$). As indicated in Figure 2(a)[1], the fault plane is oriented such that the tensile side ("T") where the off-fault damage preferentially develops, is visible for direct observation. The continuum damage-breakage model predicts high breakage states reduce the effective shear modulus μ_{eff} , decrease the shear wave speed ratio c_s/c_s^0 value. Regions exhibiting reduced wave speed are thus identified as the fault damage zone, which creates a strong modulus contrast compared with the surrounding medium. Figure 2(a) illustrates the damage evolution pattern for Case 1, which assumes a depth-constant seismic properties and linearly varying effective stress profile. Damage band evolution appears on the tensile-side ("T") off-fault medium, initiates as short, curved branches (see Figure 2(a)[1]) that progressively coalesce (see Figure 2(a)[2]-[4]), producing a spatially asymmetric damage pattern. These off-fault bands appear repetitive, staggered, and discontinuous along strike. In contrast, Figure 2(b) highlights markedly different structures in Case 2, with constant stress drop due to over-pressurization: damage zones extend throughout the depth, and the associated off-fault branches are long, straight, and vertically continuous. Such depth-invariant damage patterns have been reported in recent field studies, and may be explained by a depth-independent stress drop due to fluid pressurization that smears the depth variation of off-fault damage, and yields damage bands of comparable width across depth. Figure 2(c) demonstrates the influence of depth-dependent seismic properties (V_s, V_p, ρ) on damage generation, leading to strong localization in shallower depth, symmetrically around the fault plane. This flower-like structure align with the field observations, and it is determined by the in-depth local strain field, due to introduction of 1D velocity structure, the seismic properties in Case 3 reduces its value near the free surface, generating a tensile strain condition which is plausible for damage accumulation and localization on both sides of the fault. We conclude that the pre-event strain field and stress field have deterministic effects on the off-fault damage pattern.

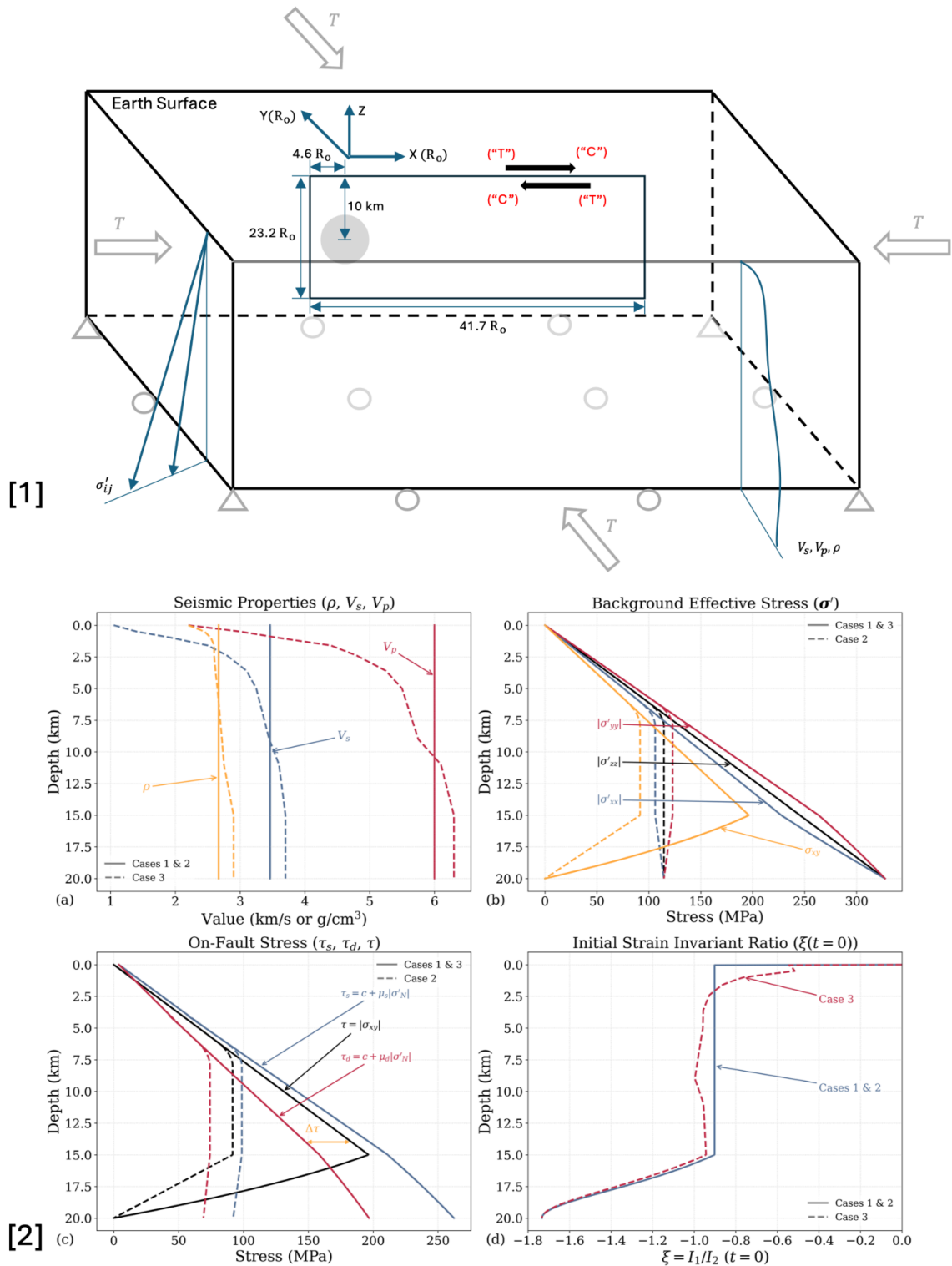


Figure 1: (1) Simulation domain. A 2D fault plane is centered in the domain, with a free surface on top, applied traction T on the sides, and fixed support at the bottom. Rupture nucleates within the gray circular region centered at 10 km depth, with the coordinate origin at the free surface directly above. Black arrows indicate right-lateral strike-slip motion; "T" and "C" mark the off-fault tensile and compressive sides. (2) Depth profiles for the three cases: (a) seismic properties — uniform in Cases 1–2, depth-varying in Case 3; (b) background effective stress — linearly increasing in Cases 1 and 3, with fluid over-pressurization at 7–15 km in Case 2, and reduced shear stress below 15 km reflecting the brittle–ductile transition; (c) on-fault peak and residual shear strengths (τ_s , τ_d) from slip-weakening friction and fault-normal stress, with stress drop $\Delta\tau = \tau - \tau_d$ driving rupture; (d) strain invariant ratio ξ — depth-uniform in Cases 1–2, elevated near the free surface in Case 3.

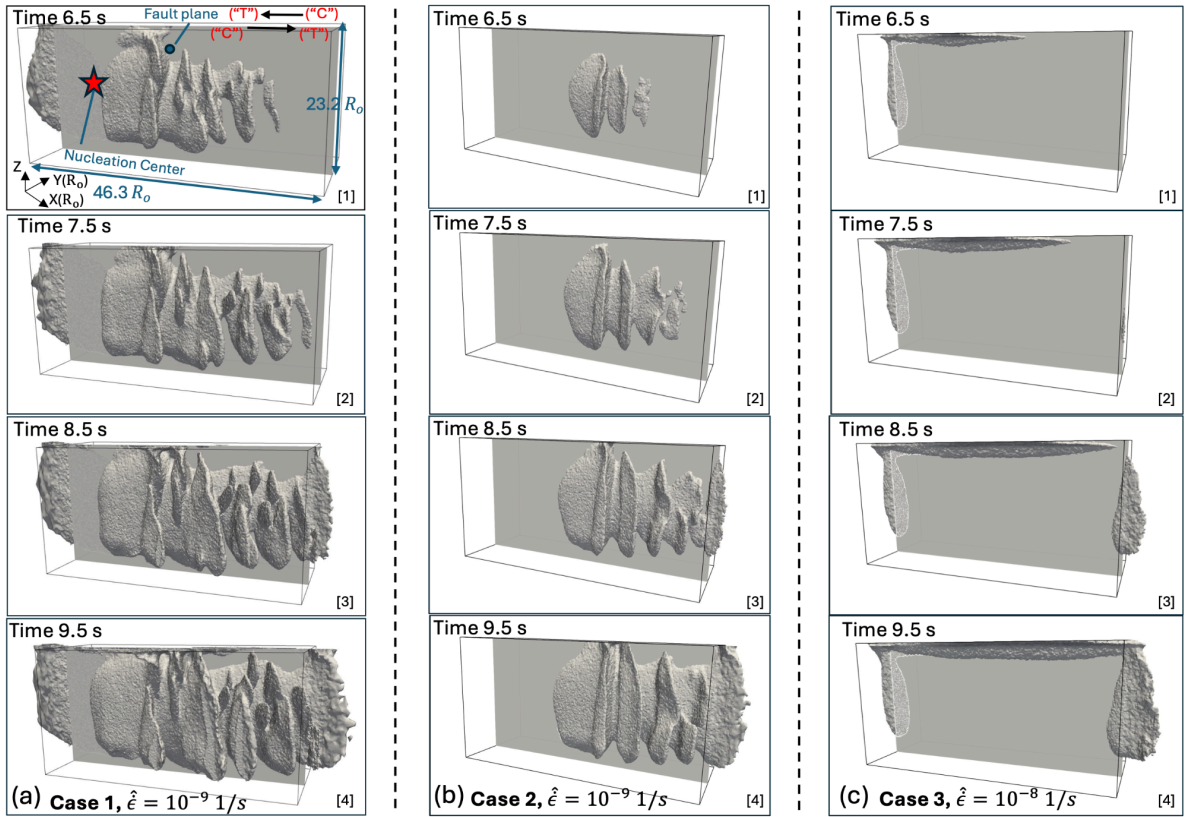


Figure 2: Three-dimensional temporal and spatial evolution of off-fault damage for the three cases. The top panel of (a) at $t = 6.5$ s shows the model configuration: nucleation center (red star), fault plane (gray surface), slip direction (black arrow), tensile and compressive sides ("T", "C"), and fault length and width scaled by process-zone size R_o . All geometries are iso-surfaces of $B > 0.8$; the black frame marks the region of interest, not the domain boundaries. (a) Case 1: short, staggered branches form along strike, with localization initiating at depth and propagating upward. (b) Case 2: long, planar branches develop continuously throughout depth, populating the entire tensile side. Both Cases 1 and 2 show discontinuous off-fault fracturing, with isolated branches forming intermittently along the rupture path. (c) Case 3 (depth-dependent seismic properties): damage localizes near the free surface and evolves as a continuous, coherent band before reaching the fault boundary. Unlike Cases 1 and 2, which produce asymmetric damage on the tensile side, Case 3 preserves symmetry across the fault (see Figure 5 for strike-perpendicular slices).

3.2 Effects of stress drop and depth-varying damage structure

Figure 3 illustrates the effect of stress drop by comparing strike slices of Case 1 (hydrostatic pore pressure with linearly increasing stress drop with depth) and Case 2 (over-pressurization with constant stress drop); see also Figure 3(c). Figures 3(a) and 3(b) show the shear wave speed ratio along depth at a strike distance of $20 R_o$ for the two cases. Along depth, both cases exhibit similar trends: maximum shear wave speed reduction occurs near the free surface, with progressively less reduction at greater depth. In terms of damage zone width, Case 1, which has a higher stress drop, produces a wider damage zone ($W = 6 R_o$) than Case 2 ($W = 3 R_o$). However, both cases exhibit depth-independent damage zone width, which is quantitatively distinct from the flower-like structure observed in Case 3. The results suggest that on-fault stress drop, which is directly linked to energy dissipation during rupture, governs the width of damage band growth, rather than the reduced frictional resistance that promotes fault sliding under over-pressurization conditions. The emergence of damage bands, growth and variation along the depth due to the stress redistribution, can only be captured through a

full three dimensional numerical model.

From the shear wave speed ratio plots in Figure 3 (a)-(b), we observe whether the damage zone developed during dynamic rupture possess depth variance or not depends on the definition of "damage zone": if we interpret damage zone as grain size distribution (related to breakage variable B) or fracture density (related to damage variable α), the damage zone doesn't have a clear depth variance. However from a seismic tomography perspective, the low velocity fault zones have the greatest reduction near free surface due to the dominant tensile strain and increased velocity value at greater depth located within the compressive strain state. Our numerical study is able to produce both interpretations within a unified framework.

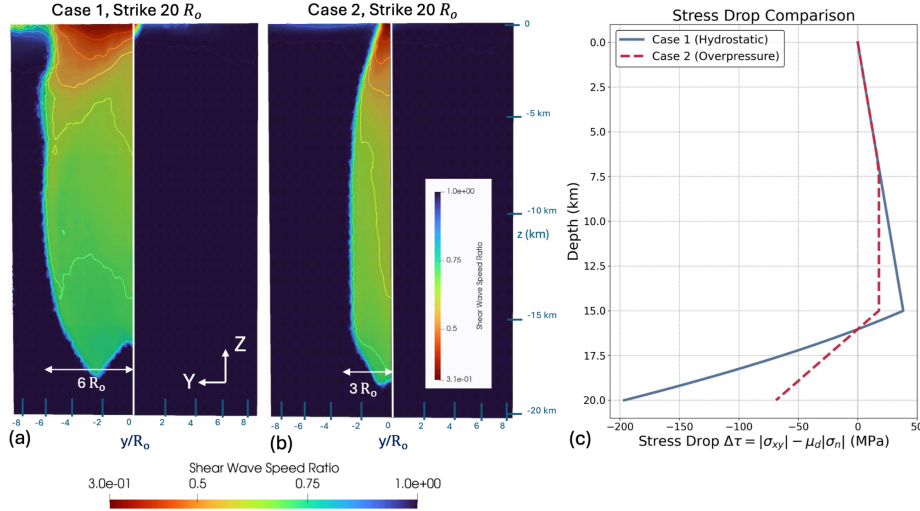


Figure 3: Slice at strike 20 R_0 , illustrating the effects of stress drop and depth-independent damage structure, both cases use the same C_d . (a) Case 1 damage zone structure. (b) Case 2 damage zone structure. (c) Comparison of stress drop between Case 1 and Case 2.

5 Discussion and Future Work

We extend our MOOSE-FARMS dynamic rupture simulator to 3D by coupling an off-fault continuum damage-breakage rheology with on-fault linear slip-weakening friction, and use it to investigate how depth-dependent seismic properties and stress profiles govern off-fault damage evolution. The simulations reproduce field-observed asymmetric and symmetric damage patterns, depth-dependent shear-wave-speed reduction, and en echelon fracture geometries or flow-like structures. Damage symmetry is controlled by the competition between the initial stress/strain state and the internal friction angle: $\xi(t = 0) < \xi_0$ produces classic asymmetric damage on the tensile side, while $\xi(t = 0) > \xi_0$ near the free surface enables bilateral accumulation and a flower-like structure. Shear-wave-speed reduction in the fully granular state is largest near the surface and diminishes with depth, reflecting the depth-dependent ξ profile inherited through the granular free energy $\Psi B(\xi)$. Stress drop, not frictional strength, is the dominant control on damage band morphology and width, with both configurations ultimately developing depth-independent damage patterns.

Future work will extend this framework along four directions: (i) two-way hydro-mechanical coupling via a thermodynamically consistent visco-poro-damage formulation; (ii) earthquake cycle simulations with rate-and-state friction to capture interseismic healing and history-dependent damage evolution; (iii) thermal effects through slip-induced heat generation and temperature-dependent healing parameters; and (iv) better experimental constraints on healing parameters to enable predictive modeling of long-term fault zone recovery.

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