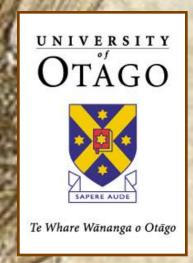
Earthquakes on Compressional Inversion Structures -Problems in Mechanics and in Hazard Assessment



Richard H. Sibson University of Otago

"WATER IS THE DRIVING FORCE OF ALL NATURE"

- Leonardo da Vinci



SC//EC



Fault-Infill Vein, Elandshoogte Mine, Sth. Africa

What Drives Fault Failure?

• Shear Failure of Intact Rock (Coulomb Criterion)

$$\tau = C_i + \mu_s(\sigma_n - P_f)$$

Griffith Failure Criterion

 $\tau^2 = 4T_o \left(\sigma_n - P_f\right) + 4T_o^2$

Reshear of Existing Faults

 $\tau = c + \mu_s(\sigma_n - P_f)$

Hydraulic Extension Fracturing

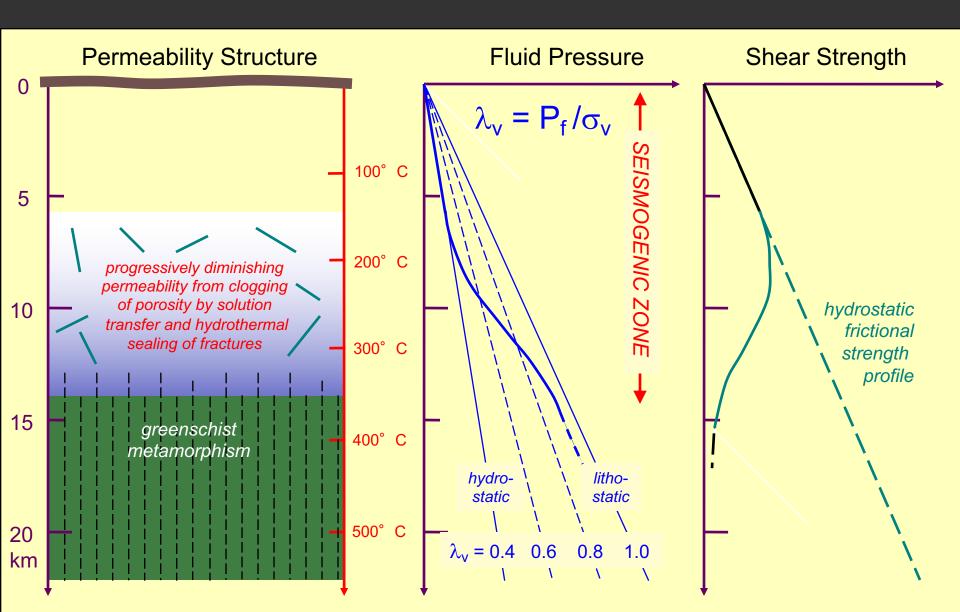
$$P_f = \sigma_3 + T_o$$
when $(\sigma_1 - \sigma_3) < 4T_o$

TWO drivers to failure – $\Delta(\sigma_1 - \sigma_3)$ and ΔP_f

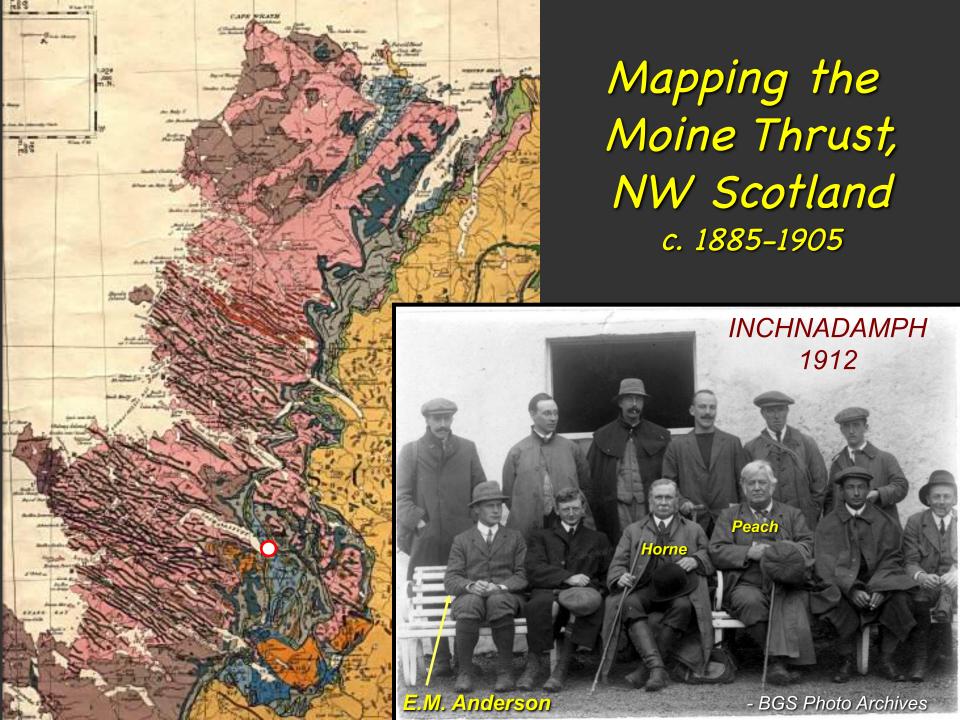
Increasing Stress $(\sigma_1 - \sigma_3)$, τ at constant P_f

Increasing P_f at constant $(\sigma_1 - \sigma_3)$, τ

Fluid Overpressure - Another Variable?



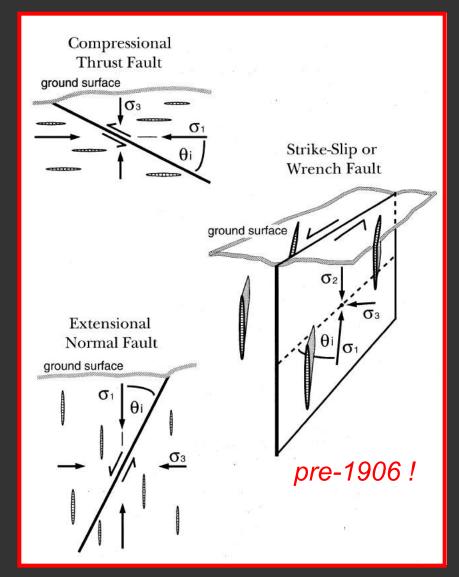
1. THE ORIGINAL FAULT MECHANIC



E.M. Anderson - 'The Dynamics of Faulting' (1905)

Trans. Geol. Soc. Edin. 8, 387-402 - foundation paper in frictional fault mechanics)

- No shear stress along the rock-air interface at Earth's surface
- One principal stress subvertical stress trajectories generally vertical or horizontal
- There are therefore **THREE**fundamental stress regimes in
 the Earth's crust depending
 whether ?_v = ?₁, ?₂, or ?₃
- Faults develop in homogeneous, isotropic, intact crust in accordance with the Coulomb shear failure criterion, forming along planes containing ? 2 lying at c. 25-30° to ?1
- THREE fundamental fault types: NORMAL Faults (?_v = ?₁), THRUST Faults (?_v = ?₃), and WRENCH (Strike-Slip) Faults (?_v = ?₂).



- relates to fault initiation — works well for low-displacement faults

Low-Displacement Reverse Faults Commonly Exhibit 'Andersonian' Relationships

Holocene Thrust, SE Iran



Quartz Veins associated with Thrust Fault, Oguf Gynfor, Anglesey



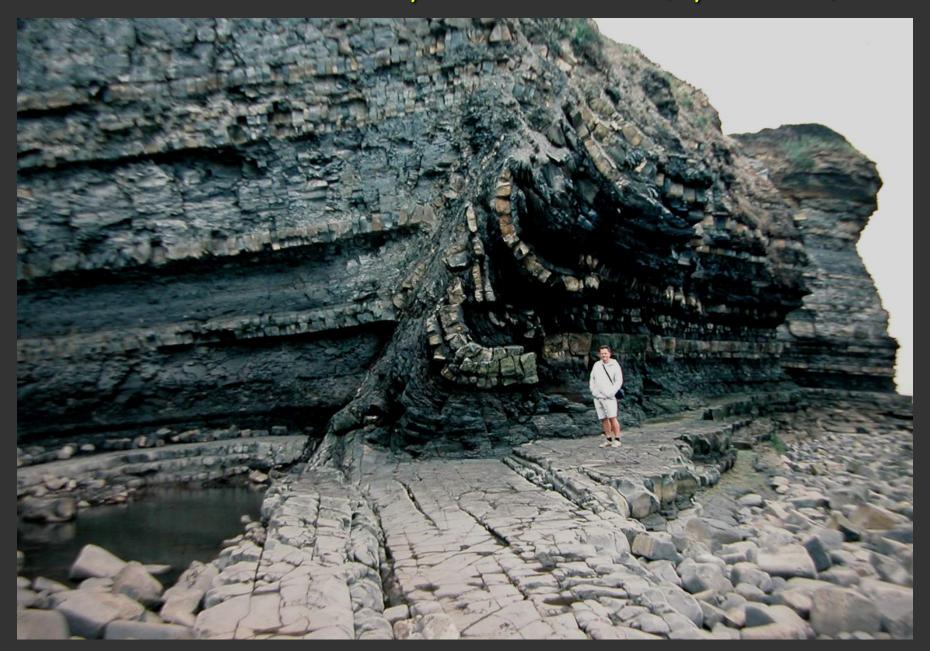
Minor Thrust, SE Otago, NZ



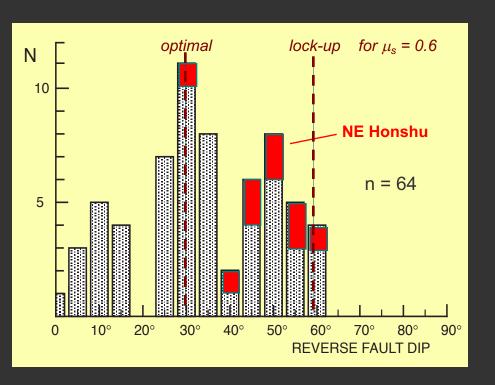
Conjugate Thrusts in Porous Sandstone, Pismo Beach, California



Non-Andersonian Steep Reverse Faults (dips > 45°)



Global Dip Distribution for Intracontinental Reverse Fault Ruptures



- $M_w > 5.5$ reverse-slip ruptures
- slip vector within ±30° of dip direction
- positive discrimination of rupture plane from surface break, from aftershock distribution, or topography
- 3 clusters at dips of $30\pm5^{\circ}$, $50\pm5^{\circ}$, and $10\pm5^{\circ}$
- NO ruptures dipping >60°

Sibson, 2009: Tectonophysics 493, 404-416

- dip distribution consistent with $\mu_s \approx 0.6$ assuming horizontal σ_1

2. WHAT IS COMPRESSIONAL INVERSION?

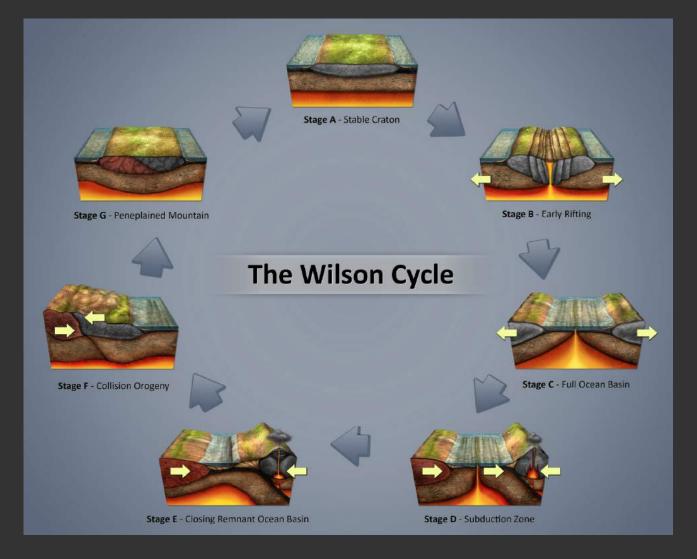
"Every valley shall be exalted And every mountain and hill made low"

- Isaiah 40: 4

COMPRESSIONAL INVERSION - SHORTENING OF FORMERLY EXTENDED CRUST

- involves Reverse-Slip reactivation under compression of inherited Normal Faults
- Bert Bally (1983) Seismic Expression of Structural Styles reflection profiling shows compressional inversion is widespread
- Characteristic Structural-Stratigraphic signature growth normal fault with abrupt thickening of syn-rift sediment on hanging-wall – harpoon-head structure
- PLANAR vs. LISTRIC faults?
- Coaxial vs. Non-Coaxial inversion strike-slip component?
- Reactivation of inherited faults is extremely selective
- GSL Spec. Publ. 44 Inversion Tectonics (1989)
 GSL Spec. Publ. 88 Basin Inversion (1995)

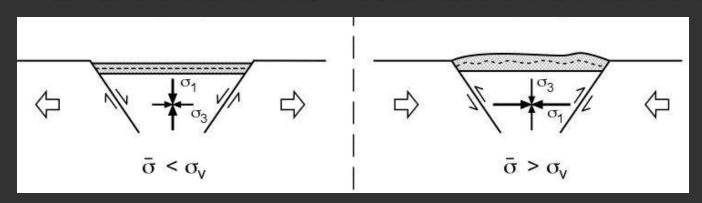
Compressional Inversion – Inevitable Consequence of Wilson Cycle of Ocean/Marginal-Sea Opening and Closure



- easier to impose brittle structure during crustal extension

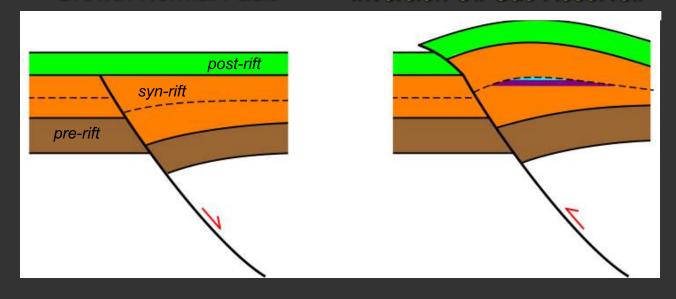
Compressional Inversion

EXTENSIONAL RIFTING COMPRESSIONAL INVERSION

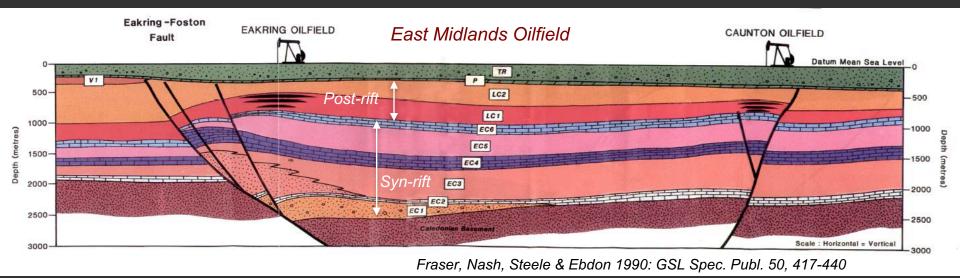


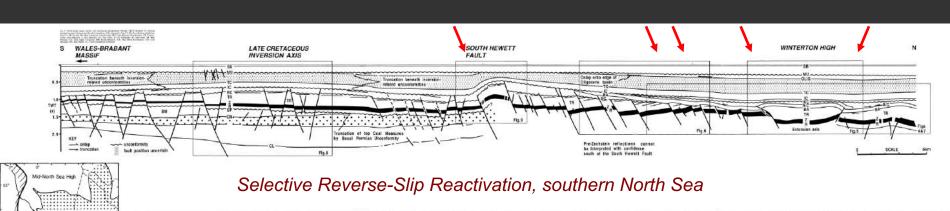
Growth Normal Fault

Inversion Oil-Gas Reservoir



Characteristics of Compressional Inversion



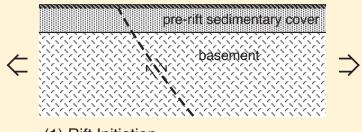


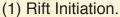
Badley, Price & Backshall, 1989: GSL Spec. Publ. 44, 201-219

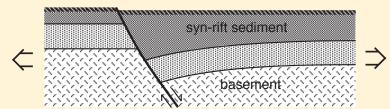
Truncation Limit

Structure Contours

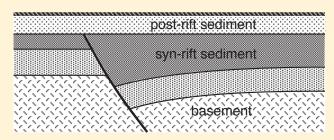
Structural / Stratigraphic Characteristics of Compressional Inversion Faults



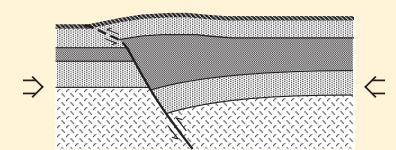




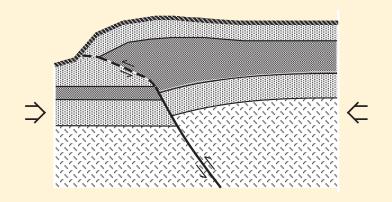
(2) Progressive Extension with deposition of syn-rift sediments.



(3) Deposition of post-rift sediments during sag phase.



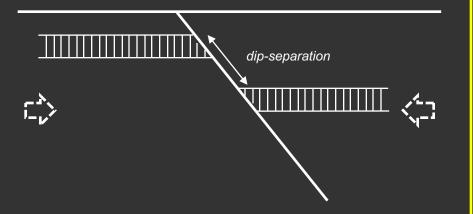
(4) Onset of compressional inversion - variable dip separations - optimal thrust forms in post-rift sediments.



(5) Continued shortening - variable reverse separations.

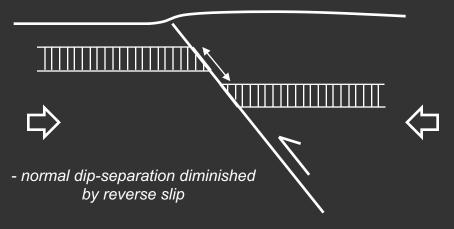
Misleading Dip-Separations

1) Inherited Normal Fault

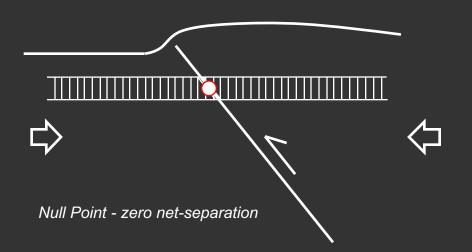


2) Incipient Compressional Inversion

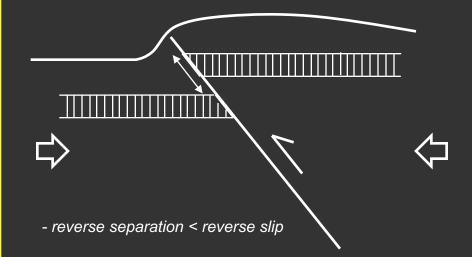
topographic expression of inversion



3) Ongoing Inversion

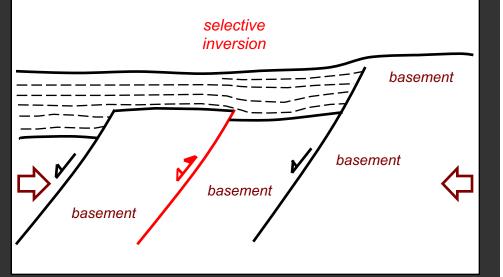


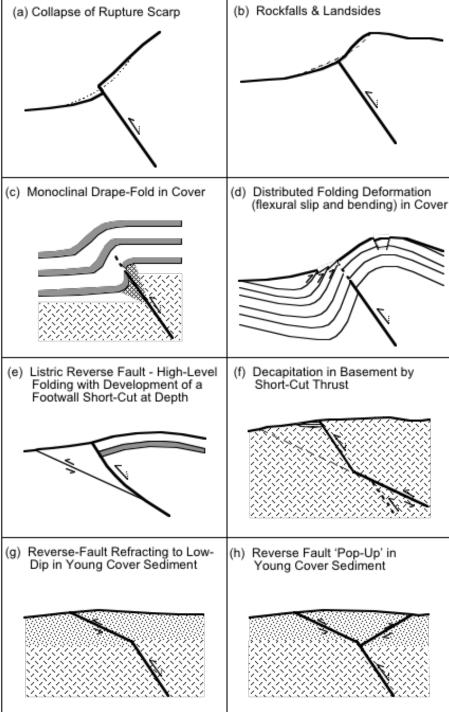
4) Advanced Inversion



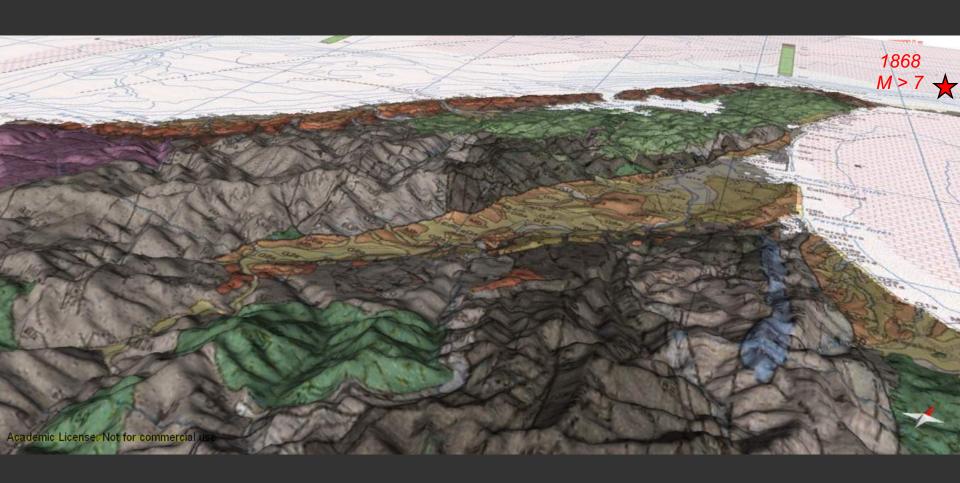
Near-Surface Structural Complications

<u>Incipient Inversion</u> – seismogenic structures 'lurking' below young sedimentary cover along margins of former extensional basins





Wakamarama Fault Trace, NW South Island



Finite Strain from Compressional Inversion, NW South Island

172°

- 'THICK-SKINNED' deformation involving basement as well as sedimentary cover
- WNW-ESE finite shortening locally <40% or more

PAC 43° mm/yr 172°E 📉 174° 176° σ_{H1} Western Platform Neogene sedimentary basins Pakawau and Paparoa coal measures (Late Cretaceous-Paleocene) Pororari Group (late Early Cretaceous) σ_{H1} Core complex overprint P: Paparoa V: Victoria Range Cretaceous batholiths F: Fraser Eastern Province Separation Point Suite Paleozoic batholiths (Brook Street, Dun Mountain-Western Province (Karamea and Paparoa) Maitai, Torlesse terranes) Takaka terrane Anatoki Fault Buller terrane Major faults Detachments (Pi: Pike; Oh:Ohika) 100 km 171° 172° 173° 174°E

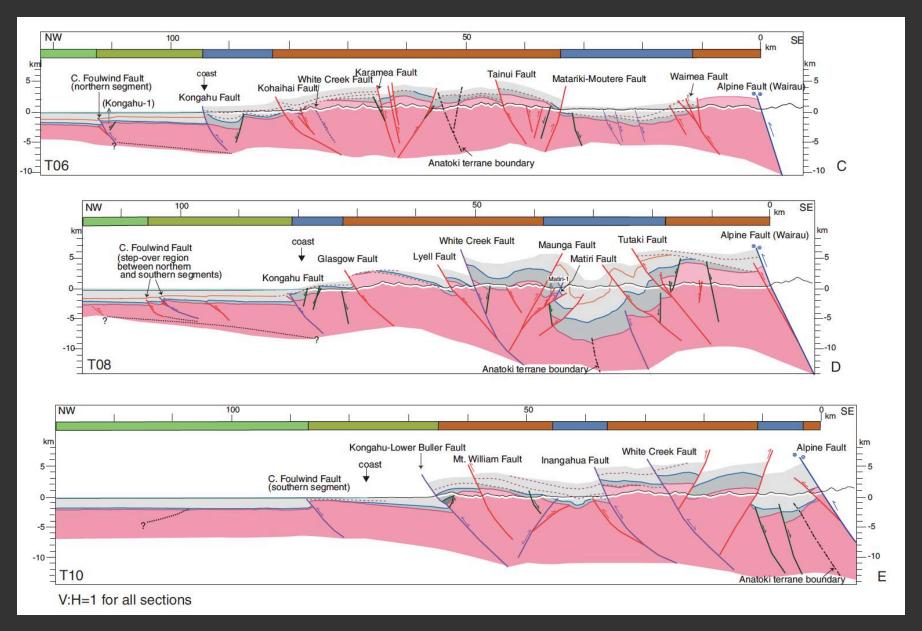
174°E

Ghisetti, Barnes & Sibson, 2014: NZJGG 57 271-294

Inversion History, NW South Island

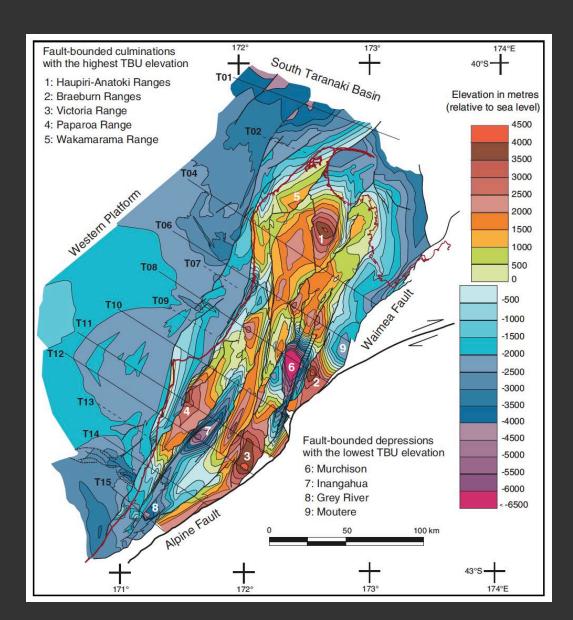
PERIOD	TECTONICS	ACTIVE STRUCTURES
6 - 0 Ma	Progressive E-W shortening of NW South Island following initiation of convergence across Alpine Fault and uplift of Southern Alps	REVERSE FAULTING & FOLDING
< 25 Ma	Initiation of ALPINE FAULT with ensuing dextral strike-slip	NE-SW Alpine Fault transform
45 – 35 Ma	Rifting and subsidence associated with opening of Emerald Basin	Enhancement of N-S to NNE-SSW NORMAL FAULT fabric
85 – 65 Ma	Rifting and subsidence accompanying opening of Tasman Sea between Zealandia & Australia	Imposition of N-S to NNE-SSW NORMAL FAULT fabric

Structural Cross-Sections, NW South Island

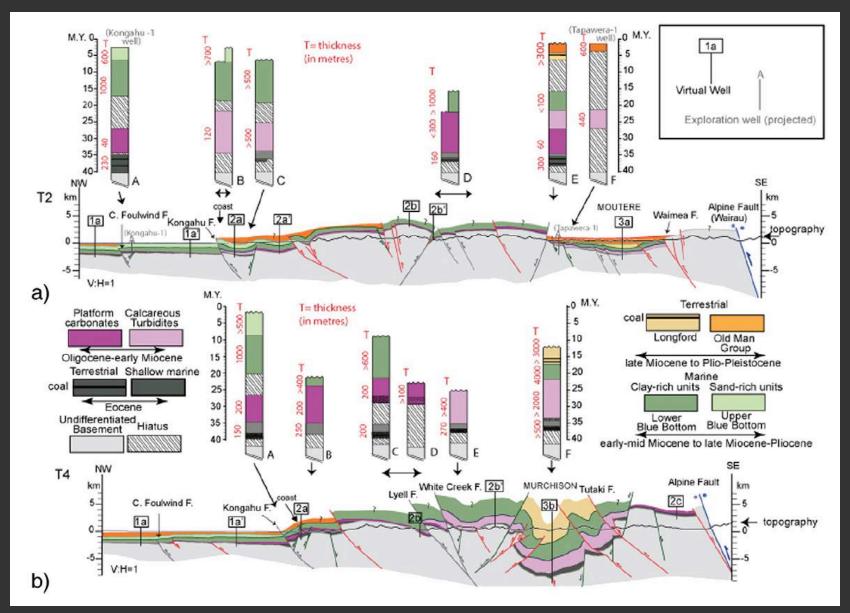


Contours on Top Basement Unconformity, NW South Island

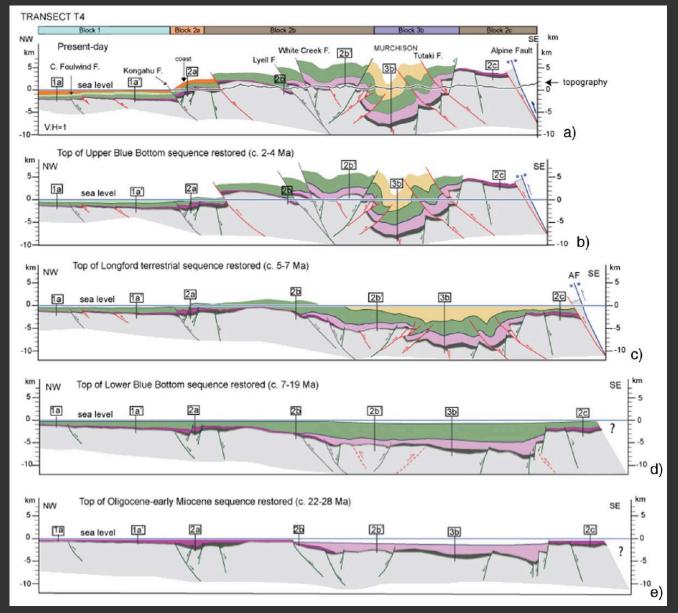
- THICK-SKINNED deformation
- WNW-ESE finite shortening locally <40% or more
- TBU ranges from 6500 m b.s.l. to 4500 m a.s.l.



Stratigraphy and Structure, NW South Island



Progressively Restored NW-SE Cross-Sections, NW South Island



3. FRICTIONAL MECHANICS OF COMPRESSIONAL INVERSION

Stress Ratio for Frictional Reactivation (2D)

- for a cohesionless fault

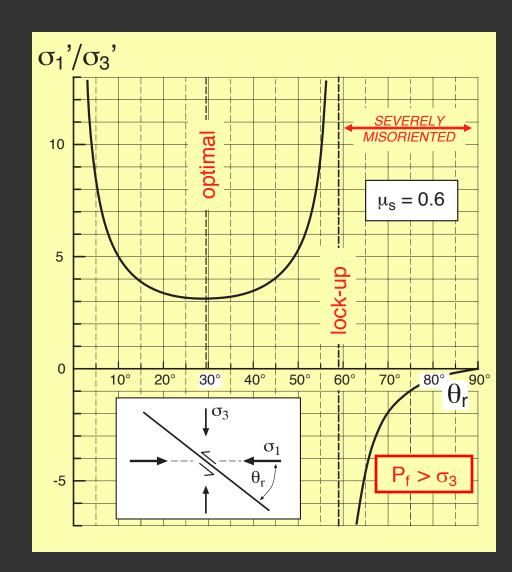
$$\tau = \mu_s.\sigma_n' = \mu_s(\sigma_n - P_f)$$

$$\frac{\sigma_1'}{\sigma_3'} = \frac{(\sigma_1 - P_f)}{(\sigma_3 - P_f)} = \frac{(1 + \mu_s \cot \theta_r)}{(1 - \mu_s \tan \theta_r)}$$

OPTIMAL -
$$\theta_r^* = 0.5 tan^{-1} (1/\mu_s)$$

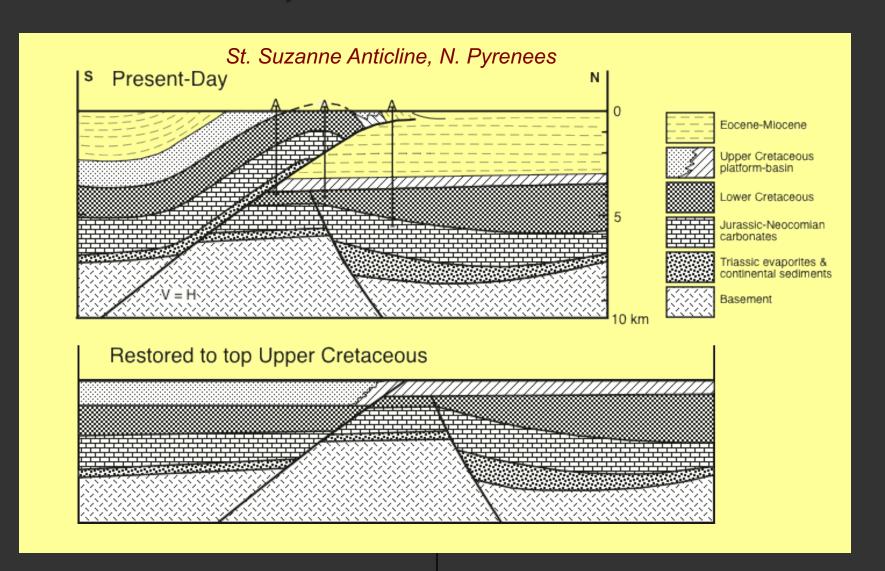
LOCK-UP - $\theta_r = 2\theta_r^* = tan^{-1} (1/\mu_s)$

As $P_f \rightarrow \sigma_3$, $(\sigma_1'/\sigma_3') \rightarrow \infty$, allowing badly oriented faults to reactivate in the absence of well-oriented structures



- for Byerlee friction, optimal reactivation occurs at 25° < $\delta_r = \theta_r < 30^{\circ}$

Preferential Reactivation During Compressional Inversion

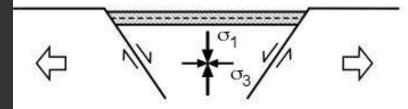


<u>COMPETITION</u> – Steep Reverse Faults vs. Thrusts in Compressional Regimes

Compressional Inversion of Inherited Normal Faults $(\theta_r < 60^{\circ} ?)$

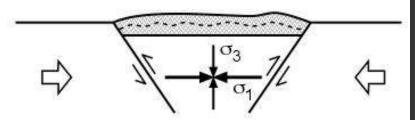


$$\sigma_v = \sigma_1$$



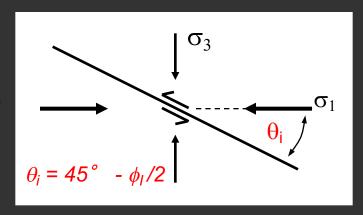
COMPRESSIONAL INVERSION

$$\sigma_{V} = \sigma_{3}$$



Reverse-Slip reactivation at $\delta = \theta_r > 45^\circ$ requires $P_f \to \sigma_3$

New-Forming 'Andersonian' Thrust $(\theta_i < 45^\circ)$

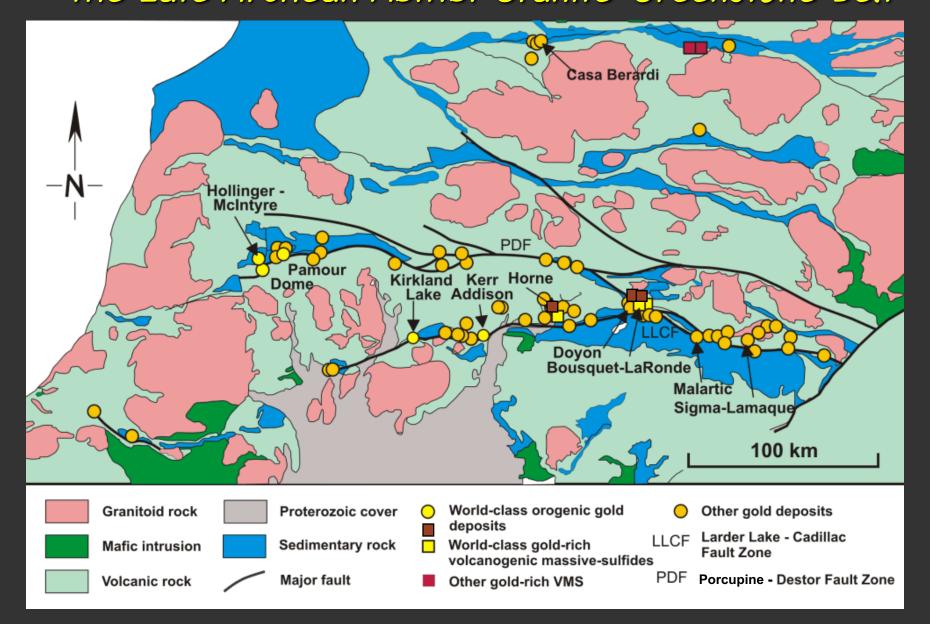


4. A BRIEF DIVERSION TO THE BASE OF THE SEISMOGENIC ZONE

"To a shower of gold most things are penetrable"

- Thomas Carlyle

Exhumed Base of the Seismogenic Zone at c. 10 km - the Late Archean Abitibi Granite-Greenstone Belt



P-T Environment for Mesozonal Lode Gold

TEMPERATURE RANGE - 270-400° C

PRESSURE / DEPTH - 2-4 kbar?? ~ 7-14 km??

FLUID COMPOSITION - low salinity, H₂O-CO₂

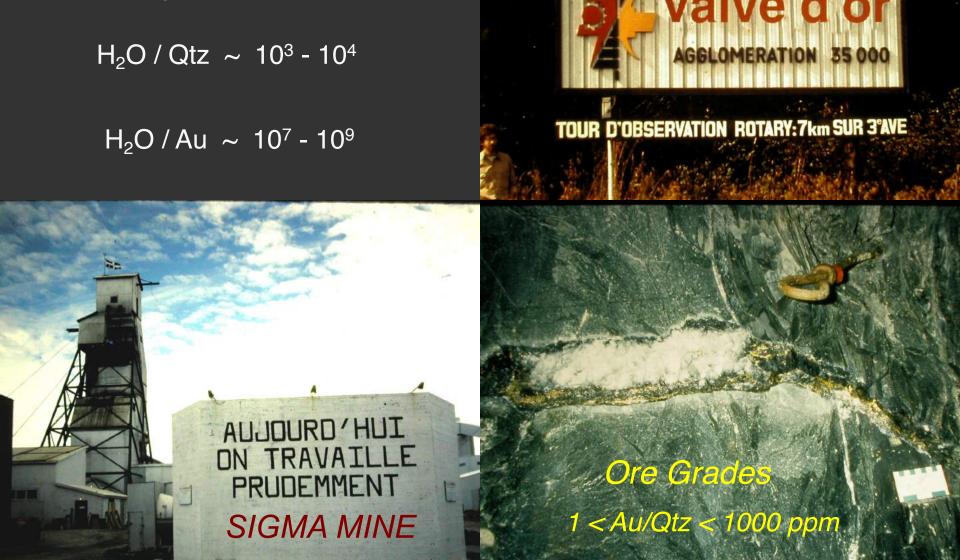
INCREMENTAL VEIN DEPOSITION – fluid inclusions - repeated episodes of fluid-pressure cycling and phase separation

METAMORPHIC ENVIRONMENT - low-mid-greenschist facies with carbonate alteration haloes around veins

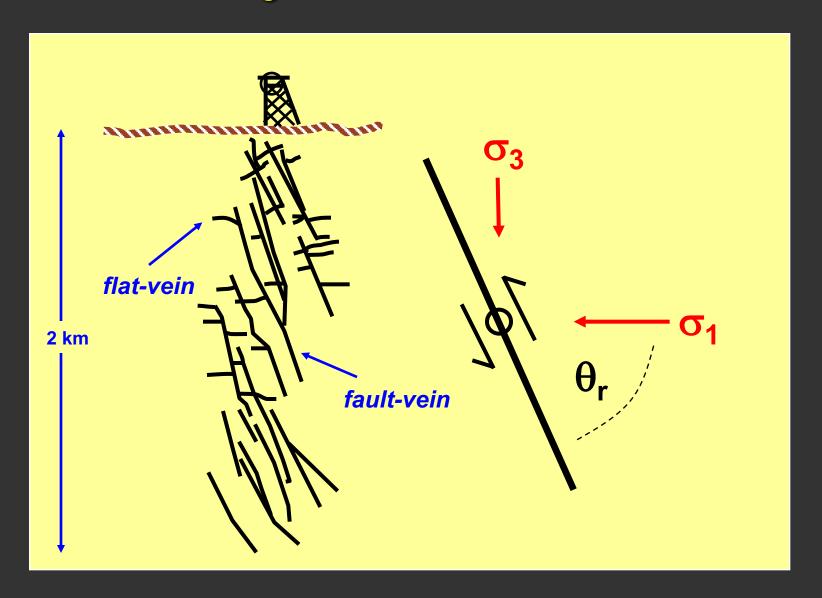
- DEFORMATION STYLE mixed brittle-ductile character (discrete shears and vein fractures as well as an L-S schistose shear zone fabric)
- vein systems have mostly developed on REVERSE FAULTS within the lower seismogenic zone in deforming continental crust

Val d'Or District

Transport Solubilities



Sigma Mine, Val d'Or

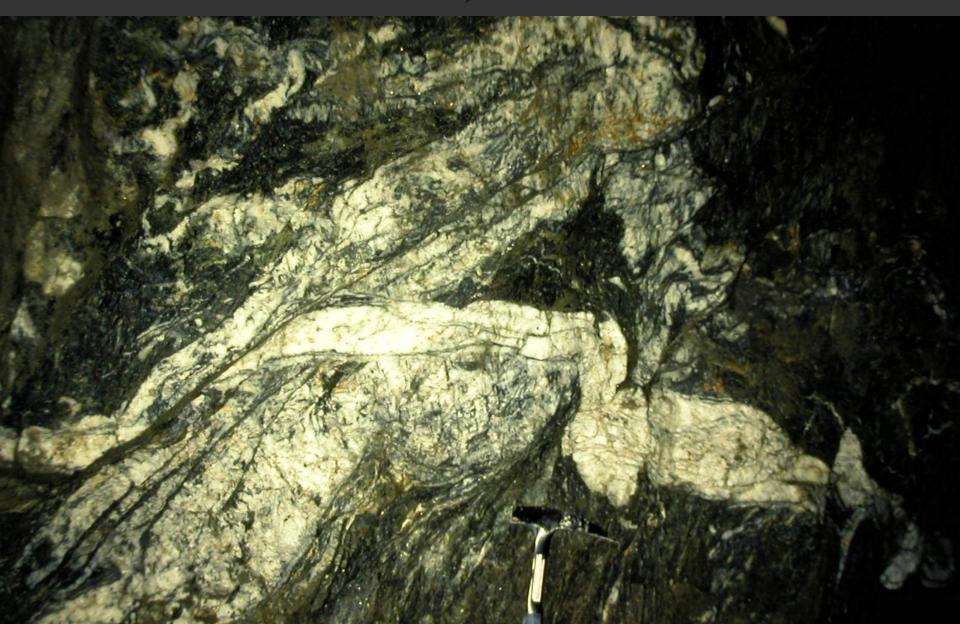


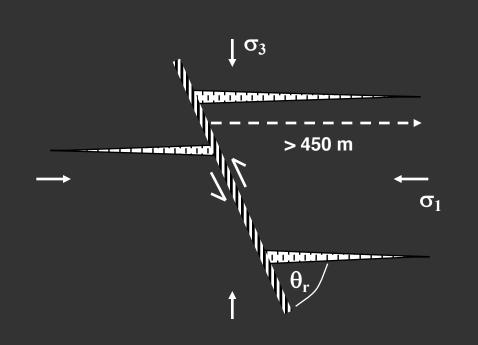


Sigma Mine – Au-Quartz Veins Hosted on Reverse Faults with Associated Flat-Lying Extension Veins



Mutually Cross-Cutting Flats & Fault-Veins, Giant Mine, Yellowknife

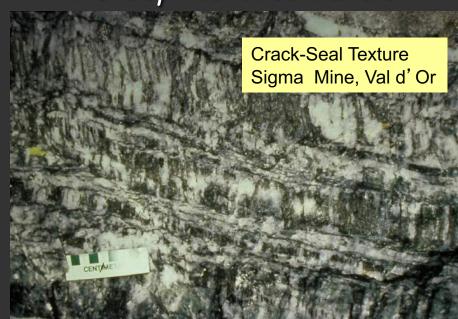






Flat Extension Veins Associated with Steep Reverse Faults





Mesozoic Orogenic Gold-Quartz, Mother Lode Belt, CA



Stress Ratio for Fault Reactivation (2D)

- for a cohesionless fault

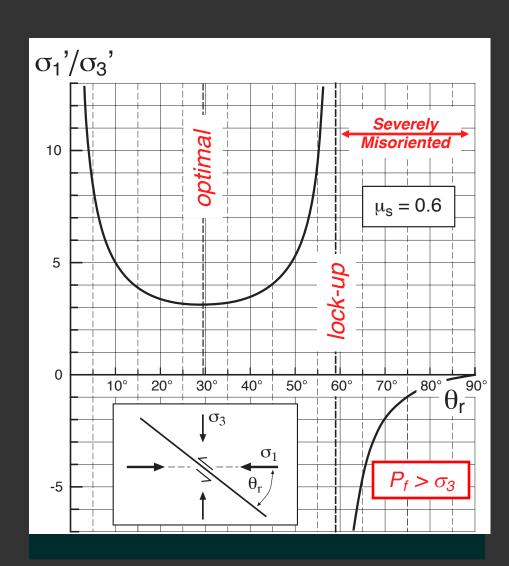
$$\tau = \mu_s \cdot \sigma_n' = \mu_s(\sigma_n - P_f)$$

$$\frac{\sigma_1'}{\sigma_3'} = \frac{(\sigma_1 - P_f)}{(\sigma_3 - P_f)} = \frac{(1 + \mu_s \cot \theta_r)}{(1 - \mu_s \tan \theta_r)}$$

OPTIMAL -
$$\theta_r^* = 0.5 tan^{-1} (1/\mu_s)$$

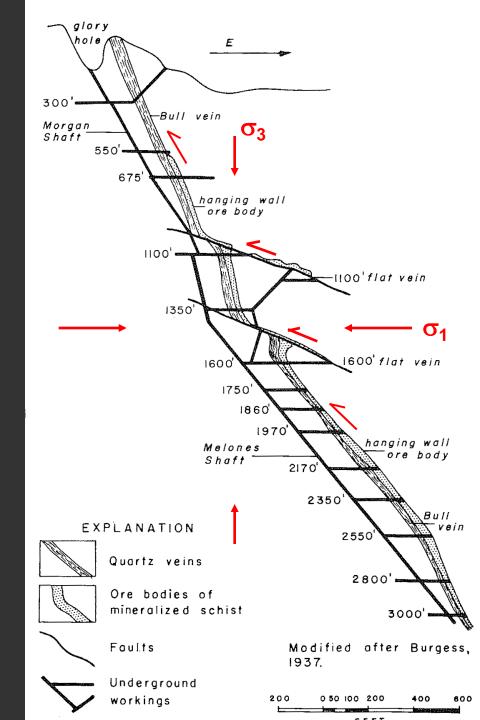
LOCK-UP - $\theta_r = 2\theta_r^* = tan^{-1} (1/\mu_s)$

$$\sigma_1'/\sigma_3' \to \infty$$
 if $\sigma_1 >>> \sigma_3$ or if $\sigma_3' \to 0$ i.e. $P_f \to \sigma_3$

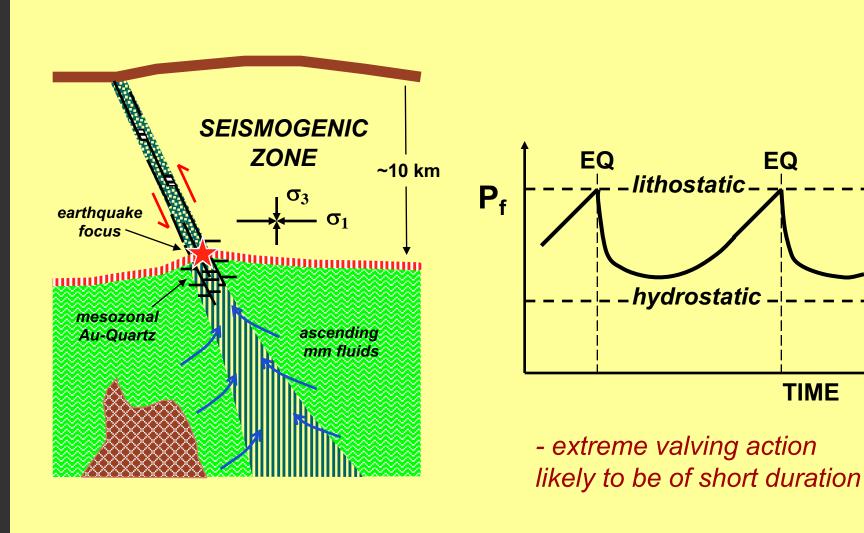


Carson Hill Mine, Mother Lode belt, California

COMPETITION!



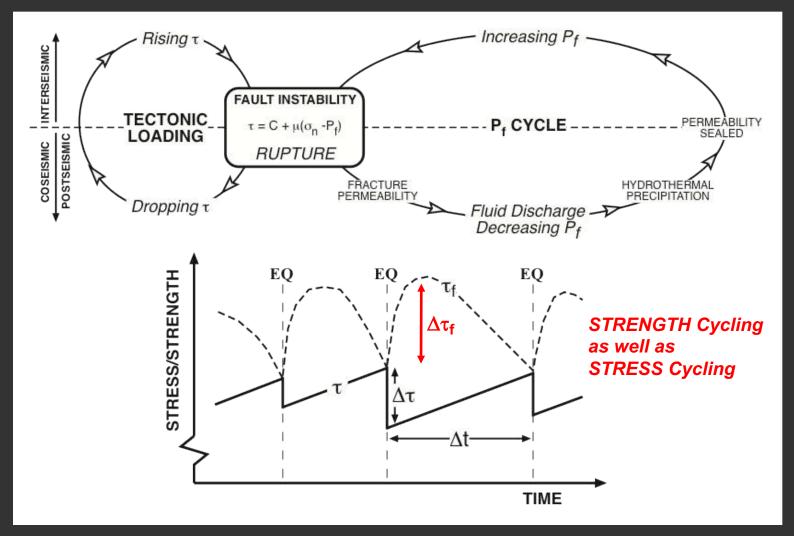
Extreme Fault-Valve Action on a Steep Reverse Fault



What is Fault-Valve Action?

- A fault may behave as a fluid-pressure activated 'valve' because of the dramatic postfailure increase in fault zone permeability
- Valving occurs when an earthquake rupture transects steep fluid-pressure gradients at the boundaries of overpressured portions of the crust
- Extreme valve-action (involving episodic discharge of large fluid volumes) commonly associated with steep reverse faults in the lower seismogenic zone

Fault-Valve Action Affecting Earthquake Nucleation and Recurrence

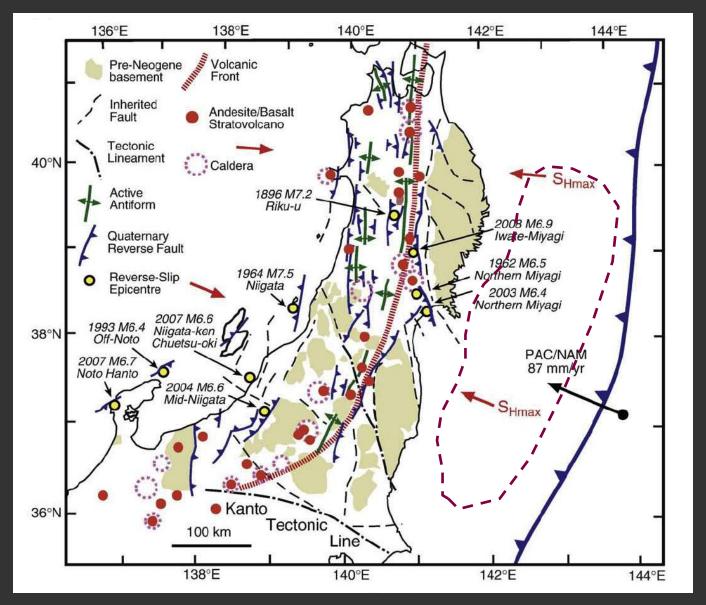


How Faults Get Loded - Are Rupture Nucleation Sites Special??

- Mesozonal vein systems develop towards base of the seismogenic zone (270° < T < 400° C; 7 < z < 14 km)
- Vein systems demonstrate that the P_f conditions for reactivation of misoriented faults were <u>locally</u> satisfied
- Typical dimensions < 2 km along strike and down-dip
- ? NUCLEATION SITES ? for reverse-slip ruptures ?
- Can rupture nucleation sites be identified on nonmisoriented faults?

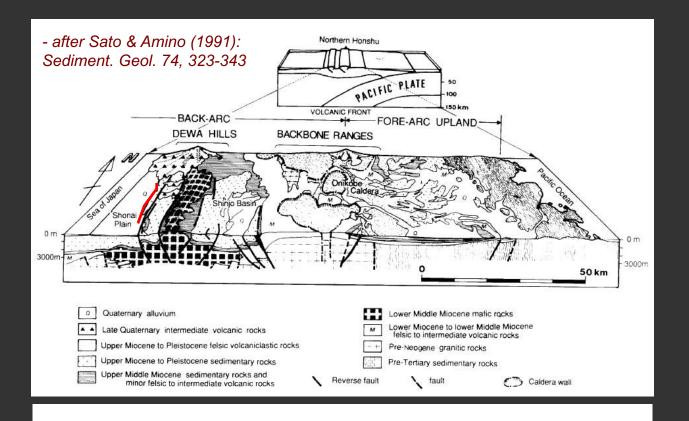
5. WHERE MAY 'FAULT-VALVE' ACTION BE OCCURRING TODAY?

NE Honshu – a Magmatic Arc under Compression



- after H. Sato, 1994: J. Geophys. Res. 99, 22,261-22,274

Active Compressional Inversion in NE Honshu



- IV. COMPRESSIONAL INVERSION < Late Pliocene < 3-4 Ma to Present
- III. PRE-INVERSION PHASE Late Miocene to Pliocene
- II. POST-RIFT PHASE Middle to Late Miocene
- I. RIFT PHASE Early to Middle Miocene (22-15 Ma) (opening of Japan Sea)

March 25, 2007, M6.7 Noto Hanto Reverse Slip Rupture - 058° /60° SE

High proportion of 'Inland Earthquakes' in northern Honshu result from ongoing compressional inversion

Recent Compressional Inversion Earthquakes in NE Honshu



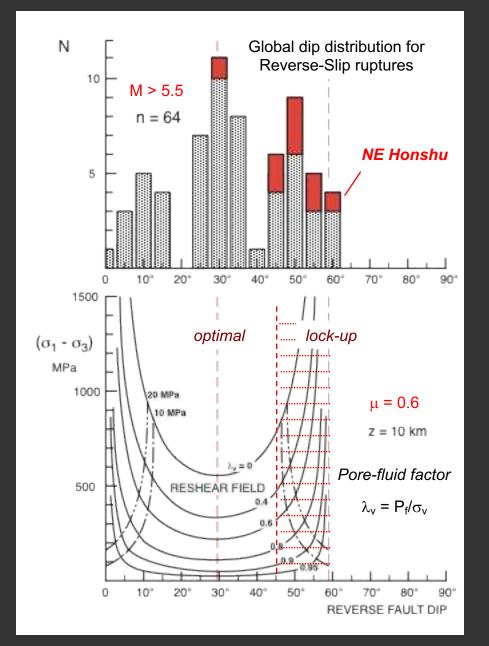
Dip Distribution of Reverse Fault Ruptures

Peak at $\delta \sim 30^\circ$ and apparent 'lock-up' at $\delta \sim 60^\circ$ consistent with $\mu =$

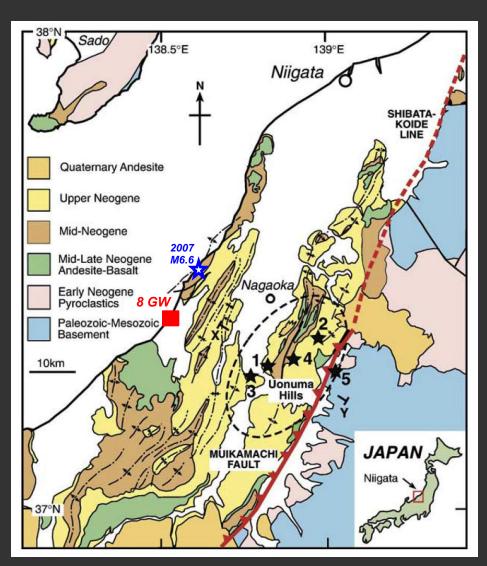
0.6

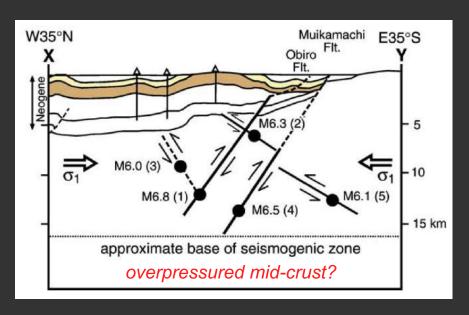
Differential stress needed for reverse fault reshear at 10 km depth as a function of fault-dip and the state of fluid overpressure $(\sigma_1 \text{ assumed horizontal})$

Near-lithostatic fluid overpressures needed for reshear of steep reverse faults in preference to formation of new optimally oriented thrusts



2004 Mid-Niigata Earthquake Sequence





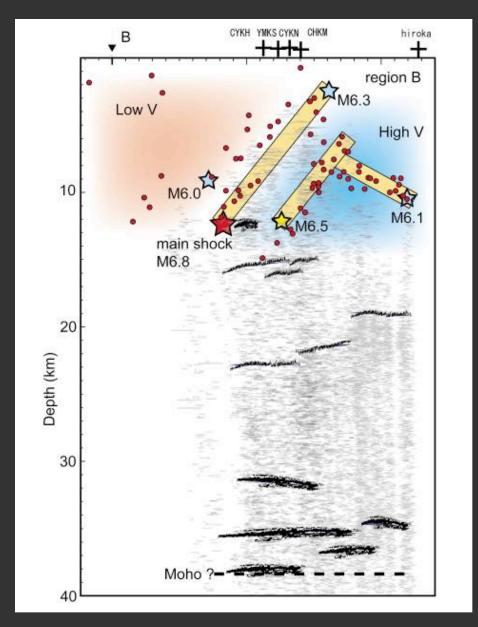
COMPETITION!

2004 Mid-Niigata Earthquake Sequence

EQ	Date- Time	<u>Strike</u>	Dip	Rake (dev.)	<u>Depth</u>	M _{JMA}	M _W	M _o (x 10 ¹⁷ Nm)
1.	Oct. 23 17.56	216°	53° N W	93° (+3°)	9 km	6.8	6.6	88
2.	Oct. 23 18.03	020°	34° SE	73° (-17°)	7 km	6.3	5.9	8.5
3.	Oct. 23 18.11	020°	58° SE	70° (-20°)	9 km	6.0	5.7	4.1
4.	Oct. 23 18.34	216°	55° N W	94° (+4°)	12 km	6.5	6.3	32
5.	Oct. 27 10.40	039°	29° SE	73° (-17°)	11.5 km	6.1	5.9	7.5

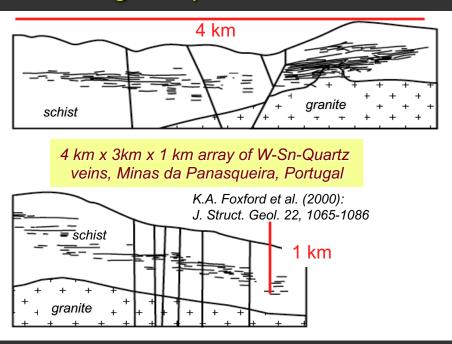
- from Hikima & Koketsu (2005) & Shibutani et al. (2005)

Bright-Spots Associated with 2004 Mid-Niigata Sequence



S. Matsumoto et al. (2005): Earth, Planets, Space 57, 557-561

Fluid-Filled Arrays of Flat-Lying Hydrofractures as Bright-Spot Reflectors



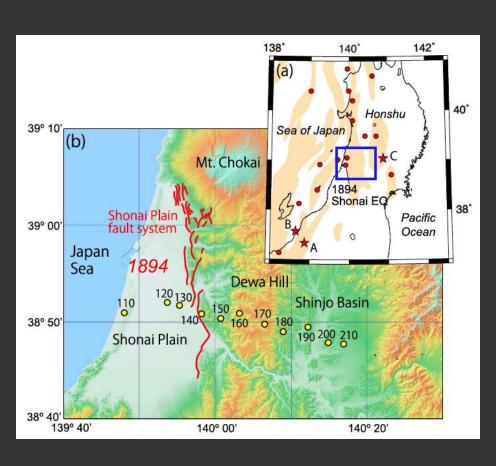
Hydrofracture Condition

$$P_f = \sigma_3 + T$$
with
$$(\sigma_1 - \sigma_3) < 4T$$

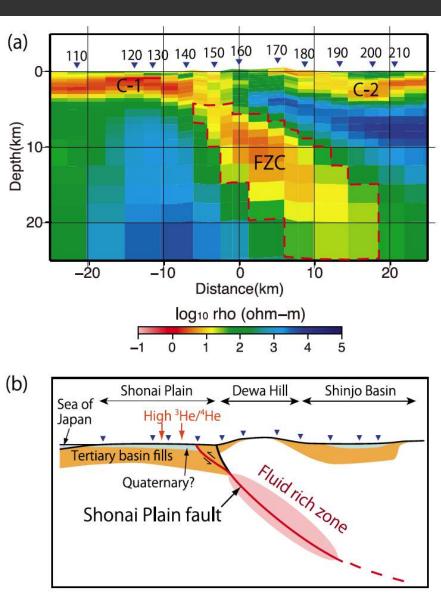
=> *lithostatic* P_f if $\sigma_v = \sigma_3$



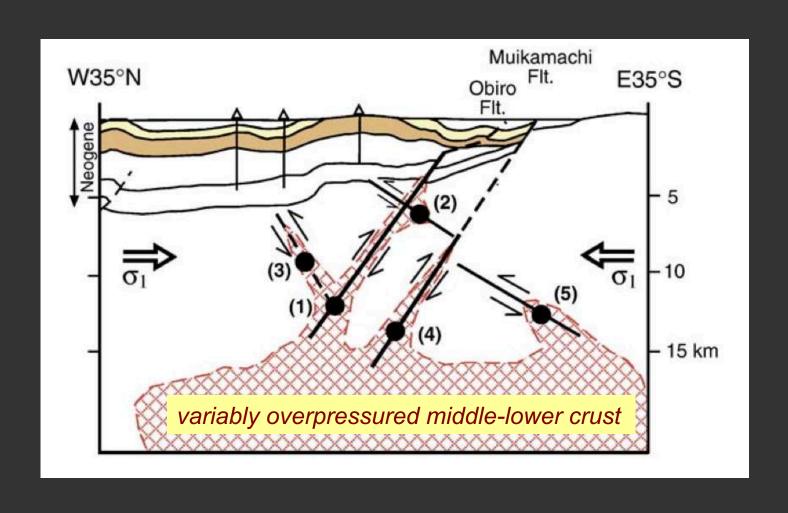
Shonai Plain Reverse Fault System



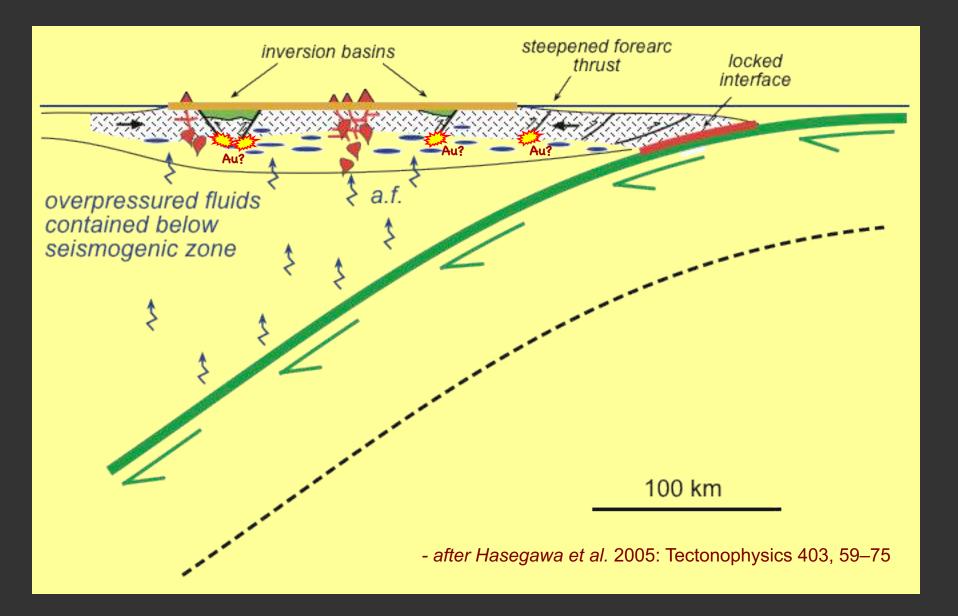
- Ichihara et al. 2011: Geophys. Res. Lett. 39, L09301, doi:10.1029/2011GL047382



Localised vs. Distributed Overpressuring?



Magmatic Arc Under Compression

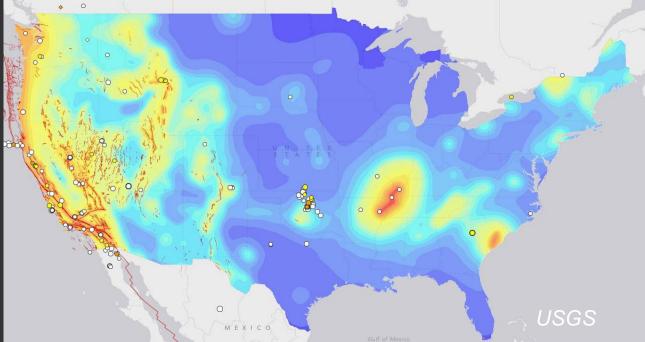


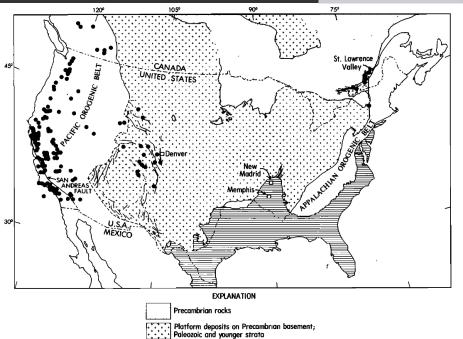
Conditions of Seismogenesis - NE Honshu

- Compressional regime ($\sigma_v = \sigma_3$) with horizontal σ_1 orthogonal to magmatic arc
- Larger ruptures nucleate in lower half of crustal seismogenic zone (commonly, 7 < z < 15 km)
- Dominance of steep reverse faults ($50^{\circ} < \delta < 60^{\circ}$) over 'Andersonian' thrusts ($\delta \sim 25-35^{\circ}$) suggests near-lithostatic overpressure in rupture nucleation sites
- Lower seismogenic zone with 150° < T < 350° C is <u>hydrothermally active</u> - electrical and tomographic studies support presence of <u>overpressured fluid in</u> <u>interconnected pore space</u> around the active faults
- $(\sigma_1 \sigma_3) < 40$ -80 MPa if bright spot reflectors are fluidfilled hydrofracture arrays with $P_f > \sigma_v = \sigma_3$

How many EQs are are wholly or partly fluid-driven?

- Anthropogenic vs. Natural?





Platform deposits; Mesozoic and Cenozoic strata

CO₂ locality

Seismicity and CO2 rich springs

Irwin & Barnes, 1980: J. Geophys. Res. 85, 3115-3121

Intraplate EQs along the Atlantic Seaboard

- 1982 Miramachi, New Brunswick, sequence m_b 5.7,
 5.1, 5.4, 5.0 at c. 7 km depth predominantly reverse-slip ruptures on NNE-SSW striking conjugate planes dipping 50-65° (Wetmiller et al. 1984)
- 1983 Goodnow, NY m_b 5.7 7-8 km depth, close-to-pure reverse slip on a plane striking NNW-SSE, dipping 60-70° WSW
- 2011 Mineral, Virginia EQ M_w 5.7 6-8 km depth close-to-pure reverse slip mainshock rupture 033° /51° SE (Wu et al. 2015)
- 2012 Waterboro, Maine M_w 4.0 6.6 km depth closeto-pure reverse slip – dip c. 33° SW? or 57° NE?
- 1886 Charleston, S. Carolina c. M_w7.0 ????

What Drives Fault Failure?

TWO drivers to failure - $\Delta(\sigma_1 - \sigma_3)$ and ΔP_f

Increasing Stress
$$(\sigma_1 - \sigma_3)$$
, τ at constant P_f

Increasing P_f at constant $(\sigma_1 - \sigma_3)$, τ

Failure from INCREASING DIFFERENTIAL STRESS

Failure from DECREASING FAULT STRENGTH

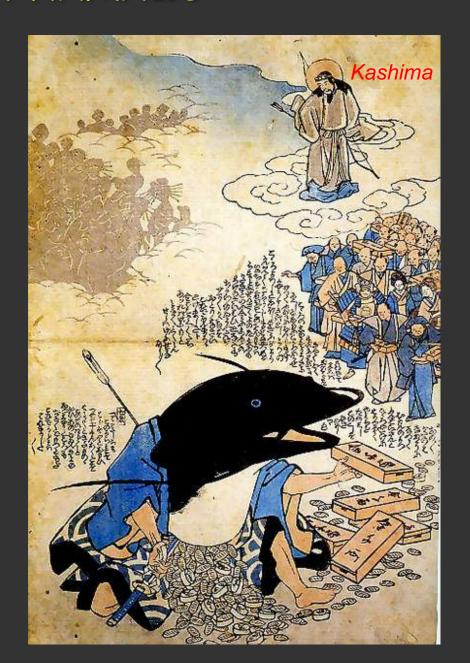
WHAT FLUIDS? - H_2O and/or CO_2 ??

CONCLUSIONS

- 1. Dip distribution of reverse fault ruptures supports $\mu_s \sim 0.6$
- 2. Compressional Inversion is widespread and accounts for a high proportion of active steep reverse faults (e.g. N. Honshu)
- 3. Reactivation mechanics suggest ~lithostatic fluid overpressures needed for rupture nucleation on steep reverse faults
- 4. Such high overpressures are supported by hydrothermal vein systems developed around steep reverse faults exhumed from the lower seismogenic zone
- 5. High fluid overpressures in the lower seismogenic zone of areas undergoing active compressional inversion also supported by observations of bright-spot reflectors, anomalously high V_ρ/V_s, and high electrical conductivity
- 6. Cycling of fluid-overpressure through 'fault-valve' action changes frictional fault strength, affecting EQ nucleation and recurrence
- 7. Fault Failure that is at least partly FLUID-DRIVEN may be more widespread than is generally supposed.

THE GOLDEN NAMAZU

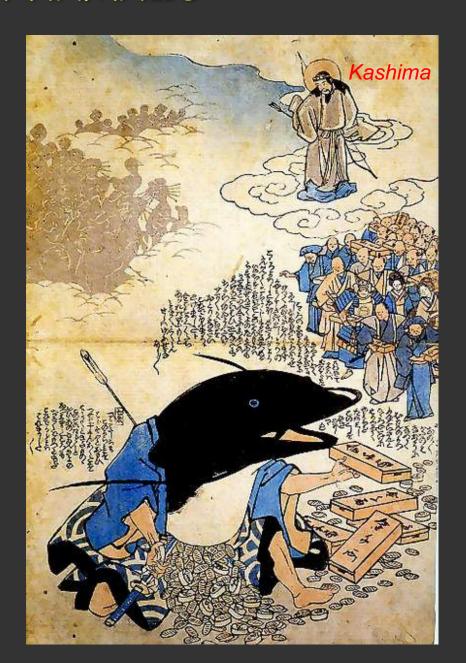


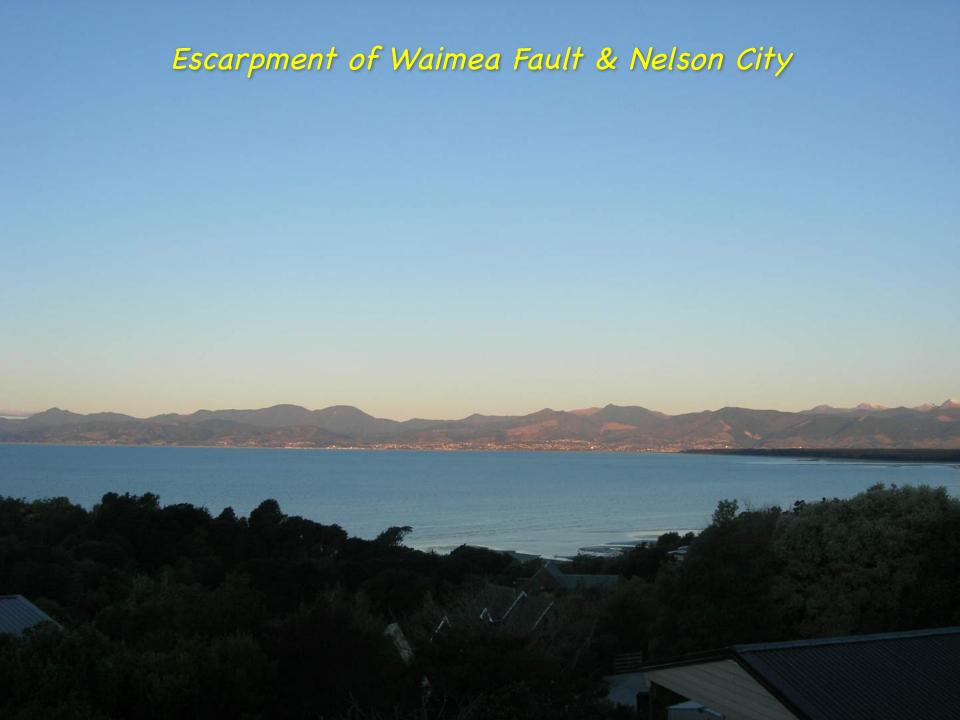


THE GOLDEN NAMAZU









Mathematical Complexity

X

Geological Complexity

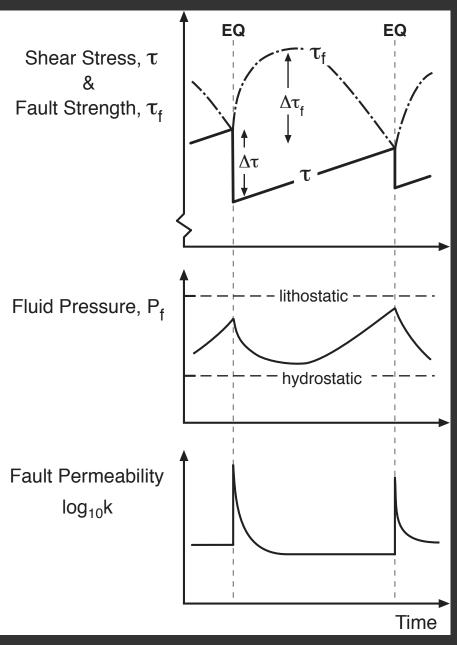
•



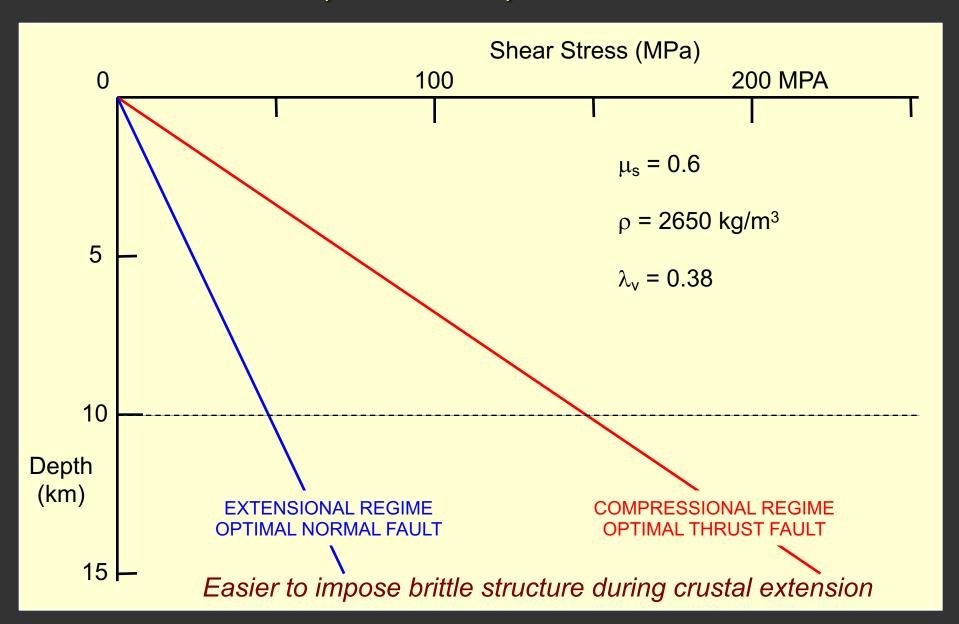
INFERRED FAULT-VALVE CYCLE



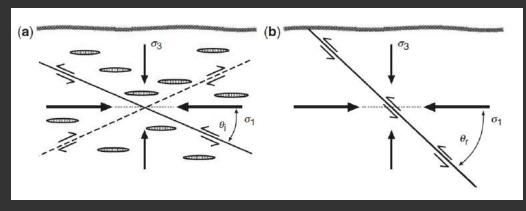
- intense competition between creation and destruction of fracture permeability

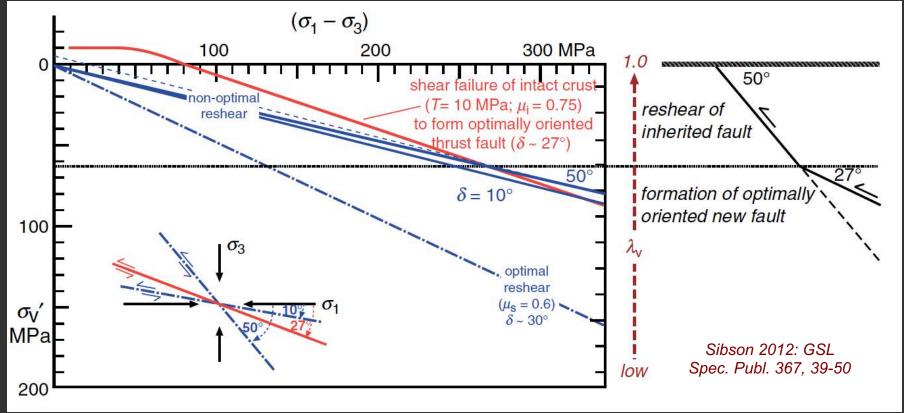


Frictional Strength of Optimally Oriented Faults under Hydrostatic-Byerlee Conditions

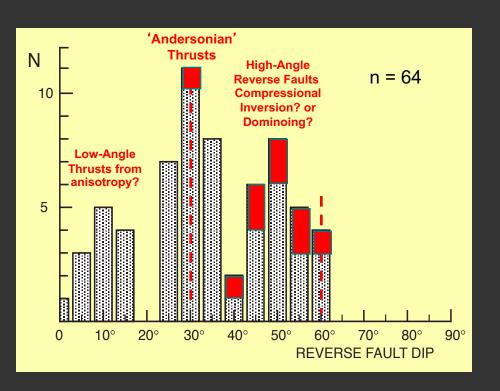


Non-Optimal Reshear vs. Formation of New Fault





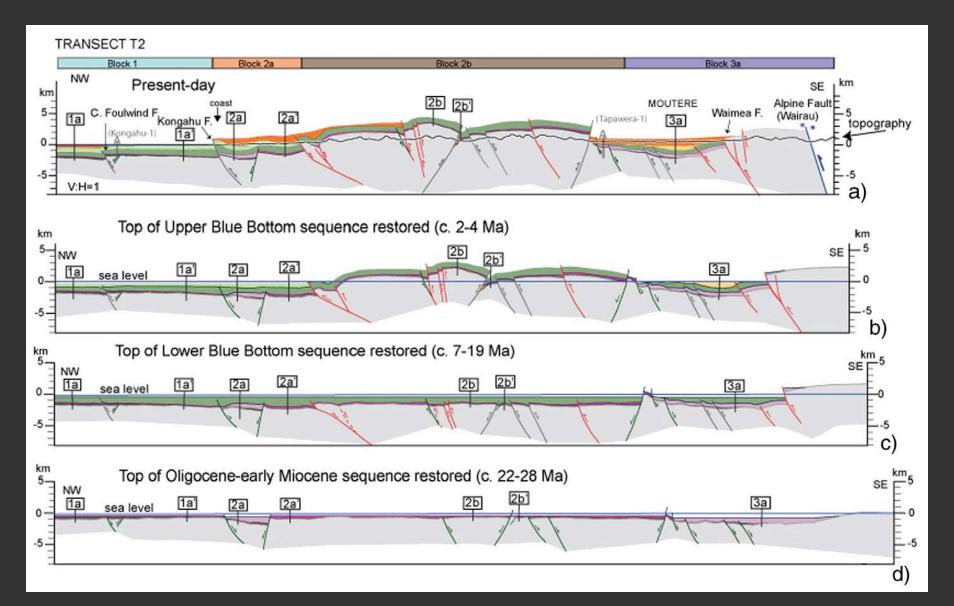
Interpreted Dip Distribution for Reverse Fault Ruptures



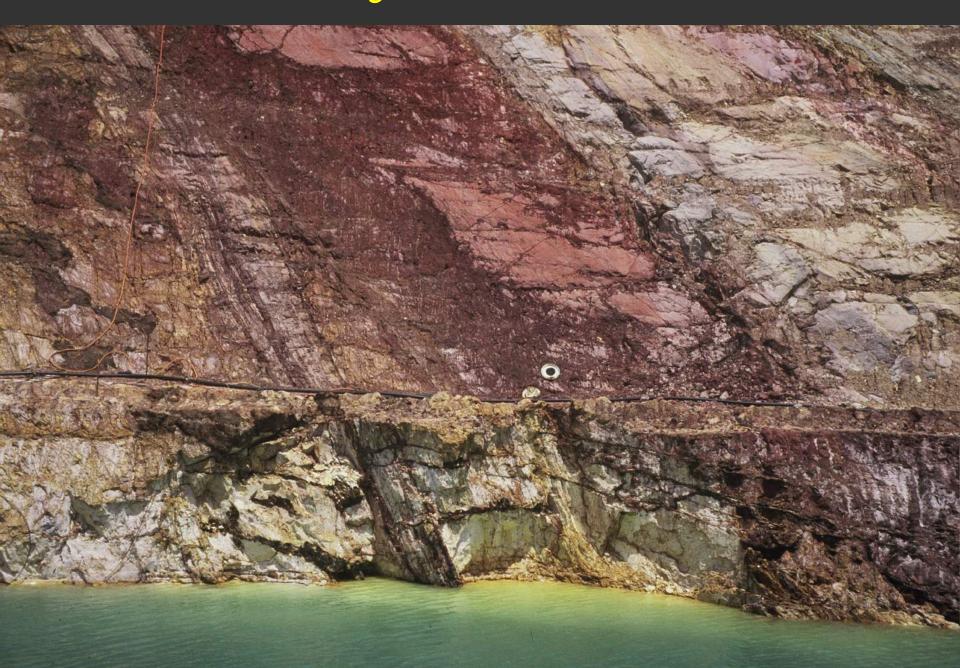
On the assumption of horizontal σ_1

- $30\pm5^{\circ}$ dip cluster may reflect optimal 'Andersonian' orientation for reactivation when $\mu_s \approx 0.6$
- Lack of rupture dips >60° may reflect frictional 'lock-up' at $\theta_r \approx 60^\circ$, also consistent with $\mu_s \approx 0.6$
- Dip clusters at 10±5° and 50±5° represent unfavourably oriented reverse faults

Progressively Restored NW-SE Cross-Sections, NW South Island

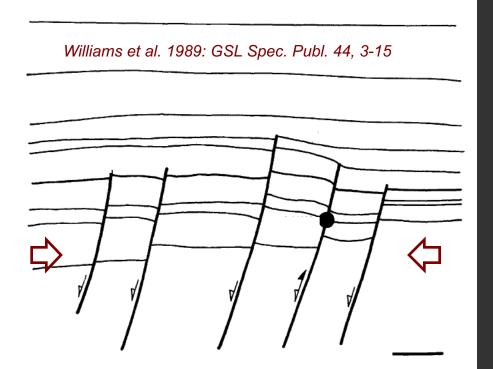


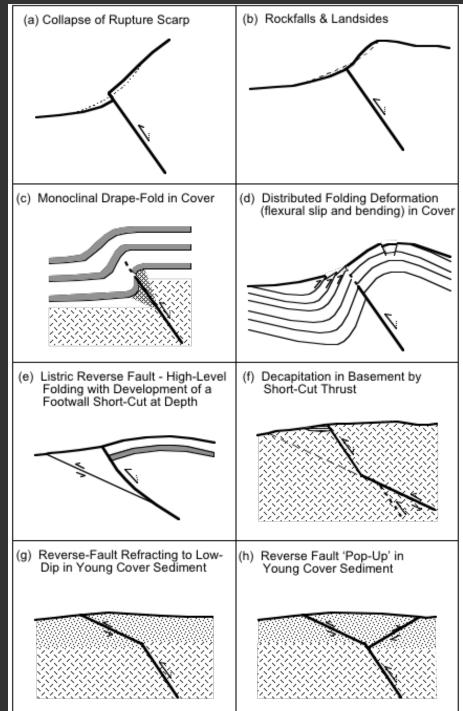
Paddington North Pit, W.A.



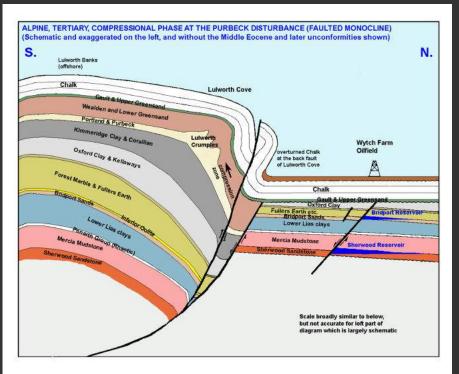
Near-Surface Structural Complications

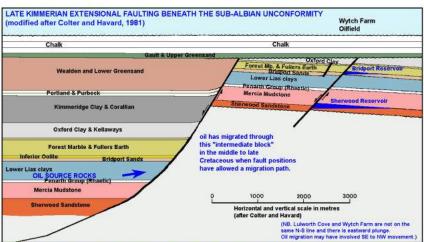
Incipient Inversion – seismogenic structures lurking below sediment cover along margins of former extensional basins



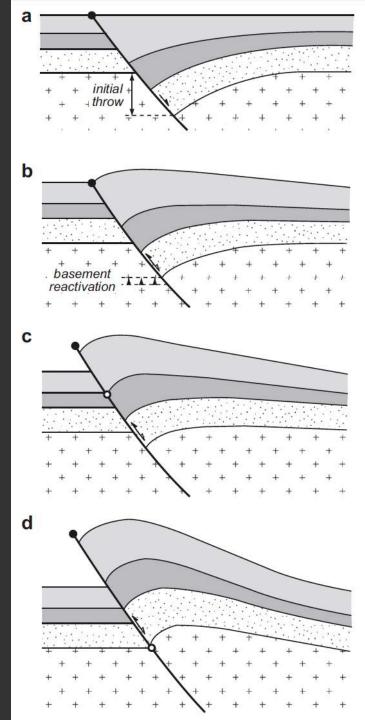


Progressive Inversion



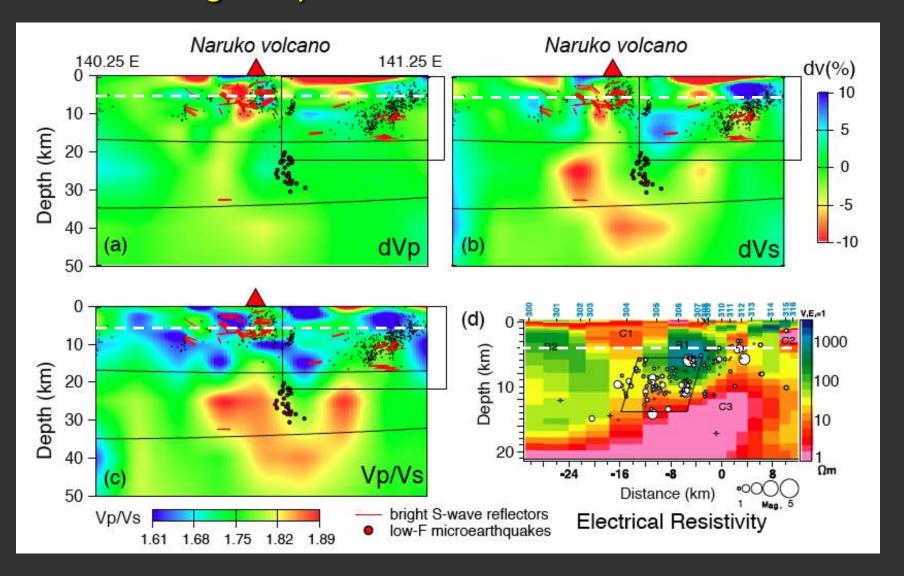


EXPLANATION OF STRUCTURES AT LULWORTH COVE AND WYTCH FARM, DORSET (MARGIN OF CHANNEL INVERSION). This is schematic and simplified, and is based on Colter and Havard (1981), House (1993), and observations on the analogous inversion margin at Bincombe (Weymouth Relief Road). It is hypothetical above cliff level at Lulworth Cove and it omits Tertiary unconformities. See also Underhill and Stoneley (1998) for more information. lan West (c) 2010.



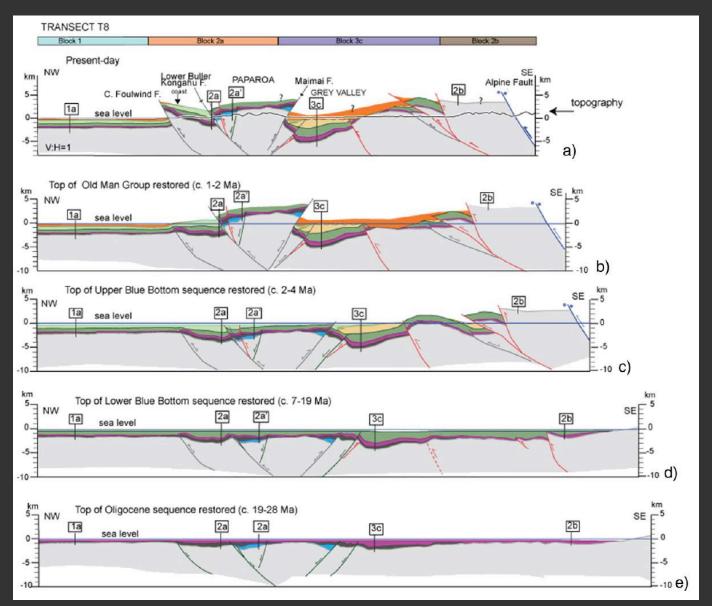


Bright-Spot Reflectors, NE Honshu



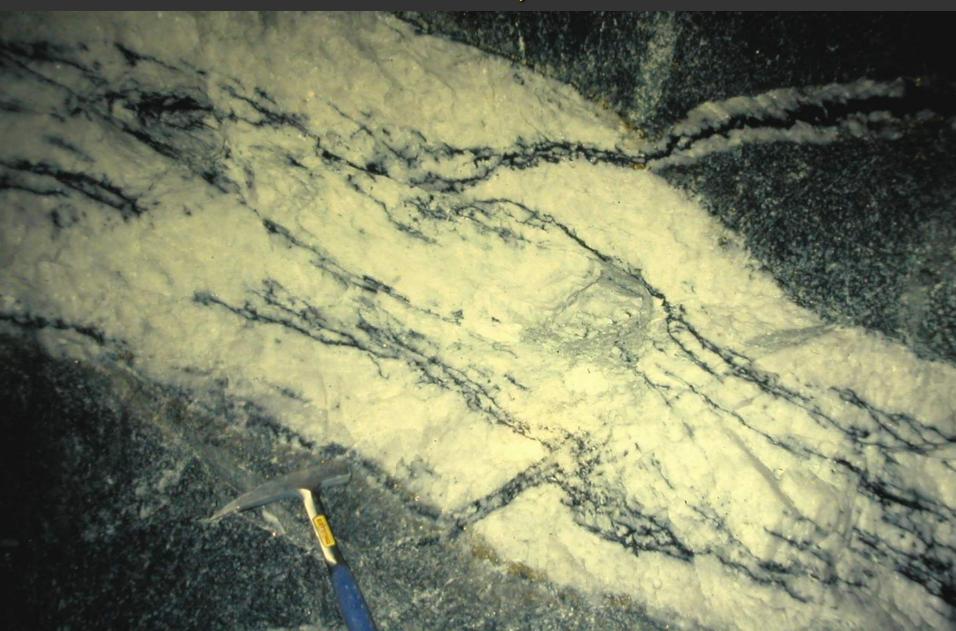
A. Hasegawa et al. (2005): Tectonophysics 403, 59-75

Progressively Restored NW-SE Cross-Sections, NW South Island

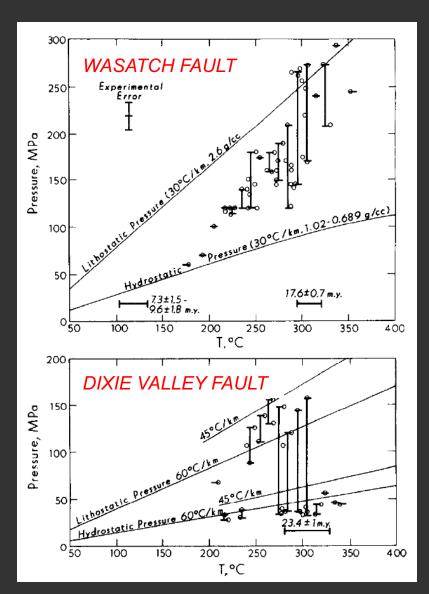


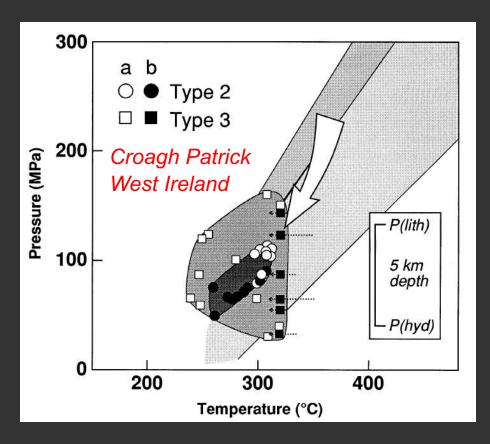
Ghisetti, Sibson & Hamling 2016: Tectonophysics

Cross-Cutting Flats & Fault-Veins, Pascal Nord Mine, Abitibi Belt



Fluid Inclusion Records of Pressure Cycling

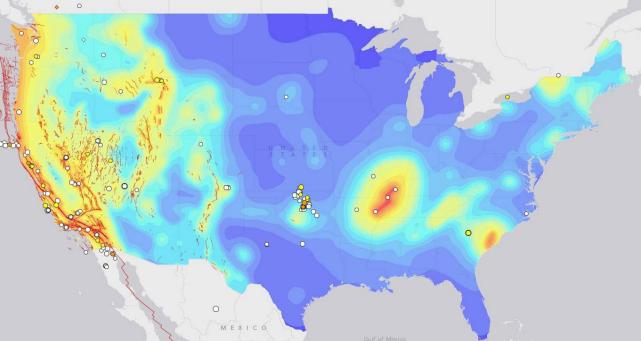


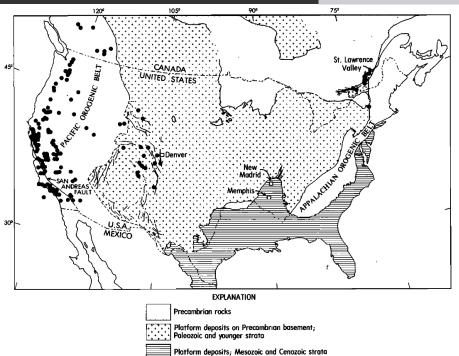


- Wilkinson and Johnston, 1996: Geology 24, 395-398

- Parry and Bruhn, 1990: Tectonophysics 170, 335-344

Seismicity and CO2 rich springs

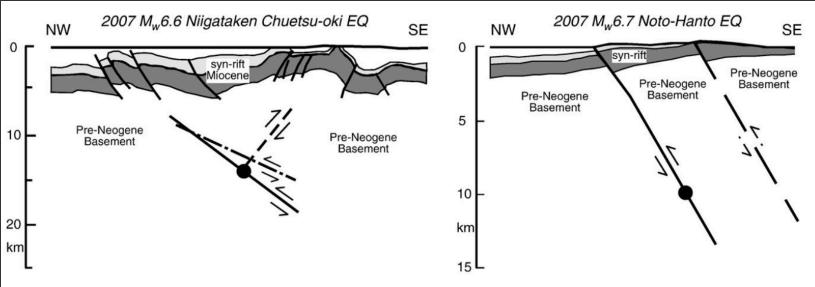




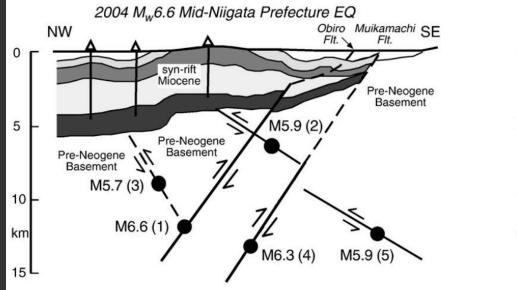
CO₂ locality

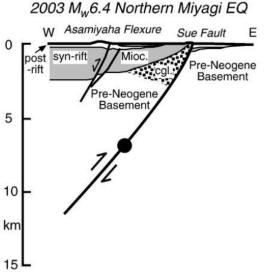
Irwin & Barnes, 1980: J. Geophys. Res. 85, 3115-3121

Northern Honshu Inversion Earthquakes

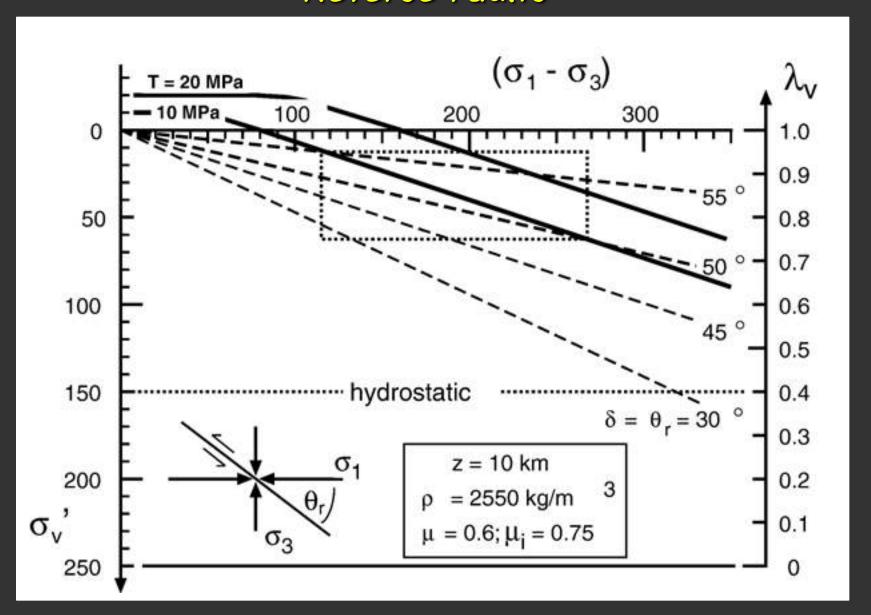


- Sibson, 2009: Tectonophysics 473, 404-416

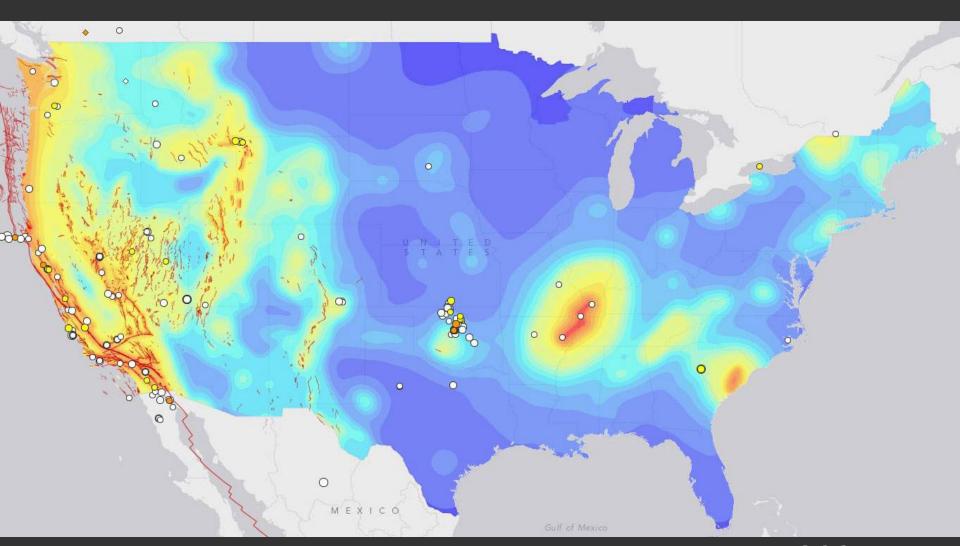




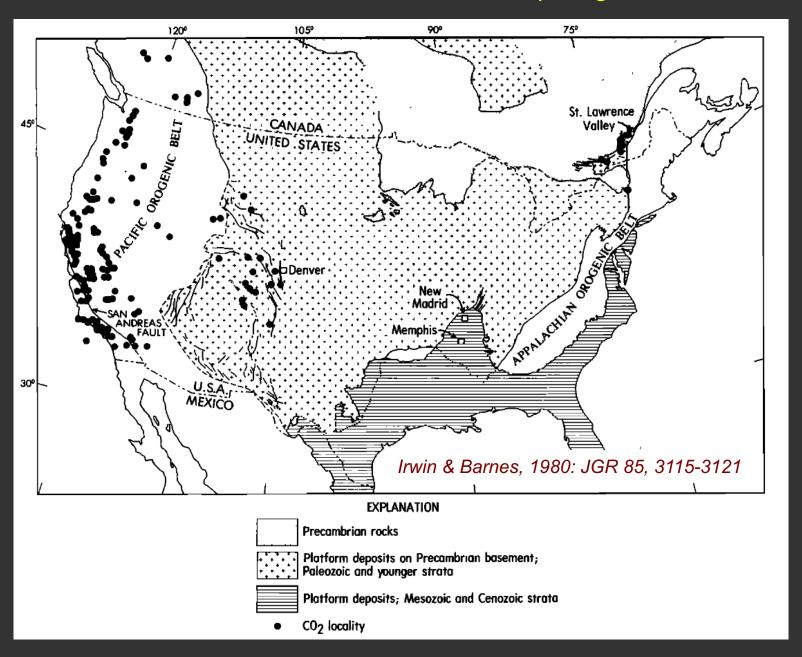
Competition between Inherited and New-Forming Reverse Faults



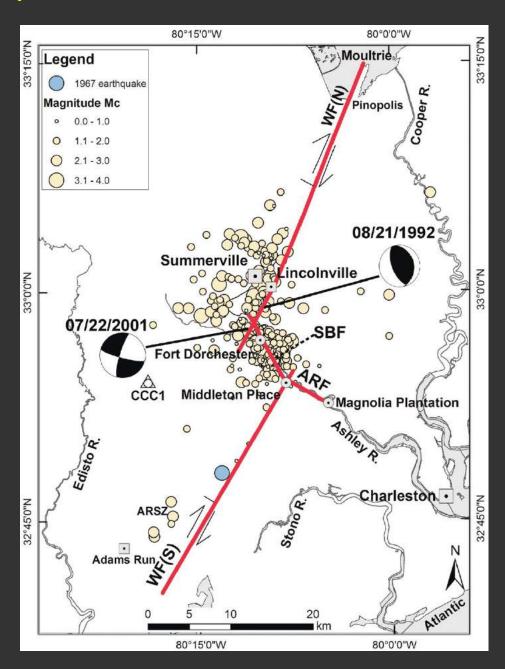
How many EQs are fluid-driven? - Anthropogenic vs. Natural?



Seismicity and CO₂ rich springs

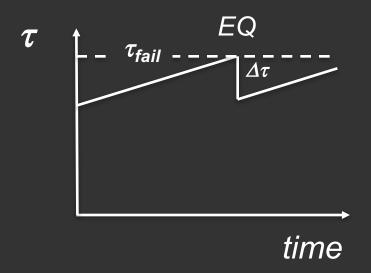


1886 Charleston EQ Source Mechanisms



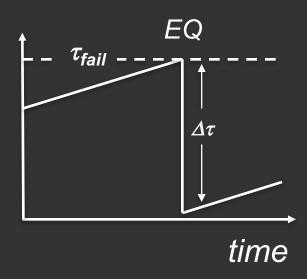
Dura-Gomez & Talwani, 2009

Partial vs. Near-Total Stress Relief



$$\Delta \tau / \tau_{fail} \rightarrow 10\%$$

hydrostatically pressured faults?



$$\Delta \tau / \tau_{fail} \rightarrow 1$$

approaching lithostatic overpressures?

$$\Delta \tau / \tau_{fail}$$
 -> 1 implies

$$\Delta \tau \approx \tau_{fail}$$
requiring either

$$\mu_{\rm s}$$
 < 0.1

or

$$P_f \rightarrow \sigma_n$$
 (i.e. $\lambda_v \rightarrow 1.0$)

EQs with Near-Total Shear Stress Drop

1952 M7.7 Kern County EQ Steep Reverse Castillo & Zoback,

1995

1989 M6.9 Loma Prieta EQ Dextral > Zoback & Beroza,

Reverse 1993

2002 M7.9 Denali EQ Dextral SS Wesson & Boyd, 2007

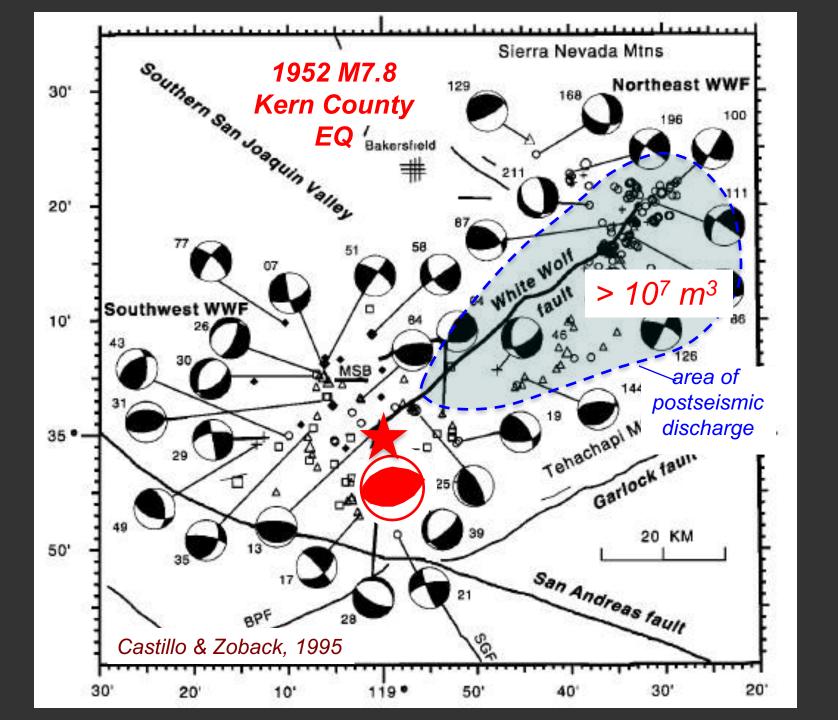
2008 M7.2 Iwate-Miyagi- Reverse Yoshida et al., 2014

Nairiku EQ

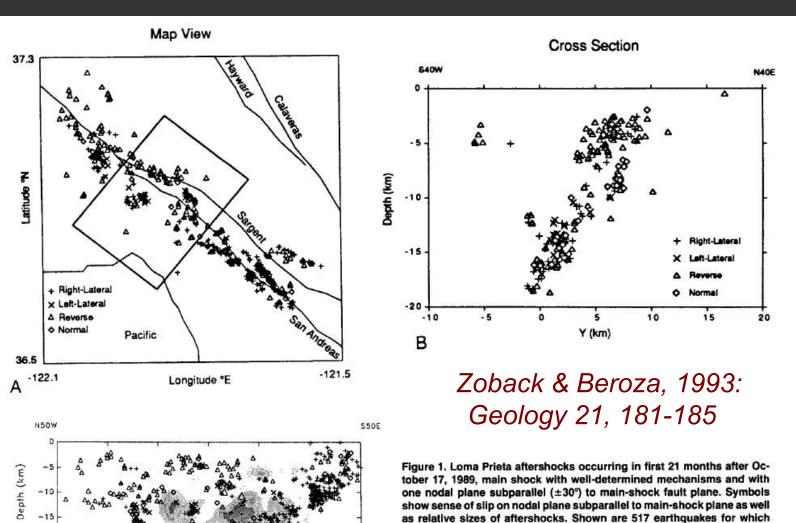
2011 M6.6 Fukushima- Normal Yoshida et al., 2015

Hamadori EQ

2011 M9.0 Tohoku-Oki EQ Megathrust Hasegawa et al., 2012



1989 M6.9 Loma Prieta EQ



Right-Lateral

Left-Lateral

Reverse

Normal

C

Distance (km)

Slip Amplitude (cm)

300

Figure 1. Loma Prieta aftershocks occurring in first 21 months after October 17, 1989, main shock with well-determined mechanisms and with one nodal plane subparallel (±30°) to main-shock fault plane. Symbols show sense of slip on nodal plane subparallel to main-shock plane as well as relative sizes of aftershocks. Shown are 517 earthquakes for which focal mechanisms are determined within ~30° at 90% confidence (D. Oppenheimer, 1991, personal commun.). A: Map view of events located within 30 km of main-shock hypocenter (along strike) and within 10 km of fault plane. B: Cross-section view of aftershocks that occurred within 10 km along strike of hypocenter projected onto N50°W. Limits of this projection are shown in A. C: Longitudinal view of fault zone as viewed from southwest and centered laterally on main-shock hypocenter. Gray shading indicates amount of slip in main shock (after Beroza, 1991). Main-shock hypocenter occurred at depth of 18 km.