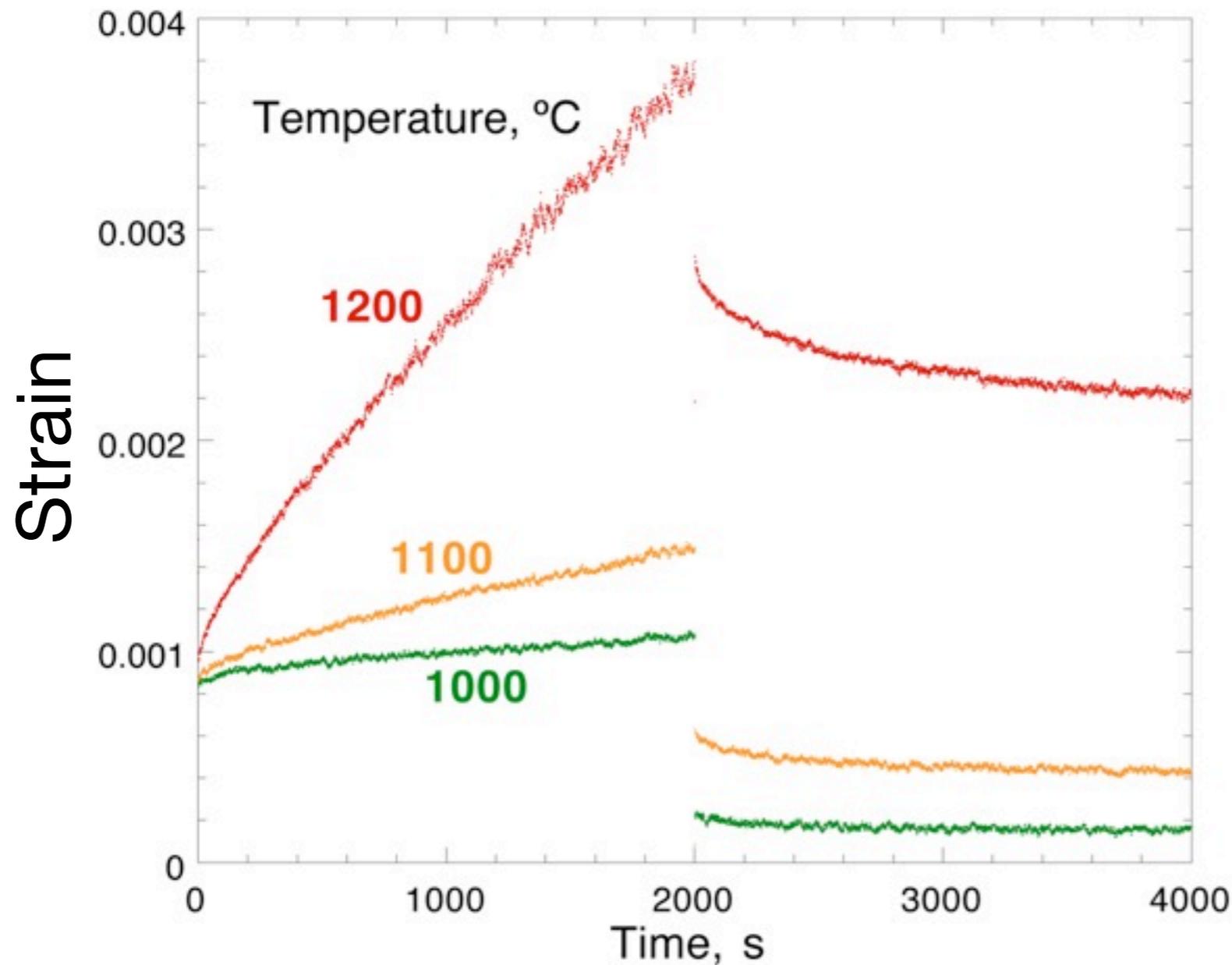


Experimental Observation of Transient Creep of Upper Mantle Rocks

Ulrich Faul

MIT

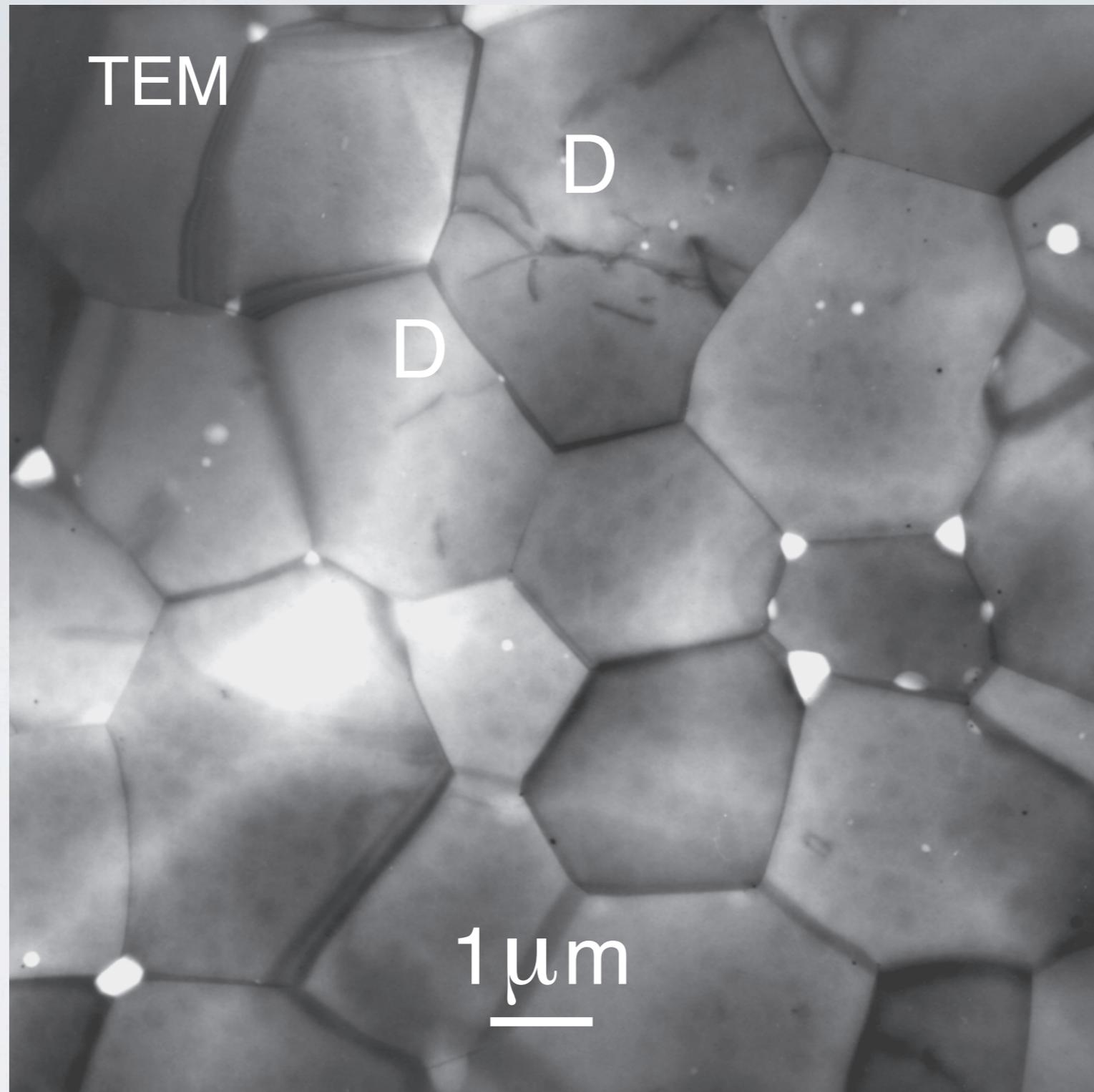
Microcreep in response to application of a step function stress



Jackson et al., 2002

response: elastic + transient + viscous

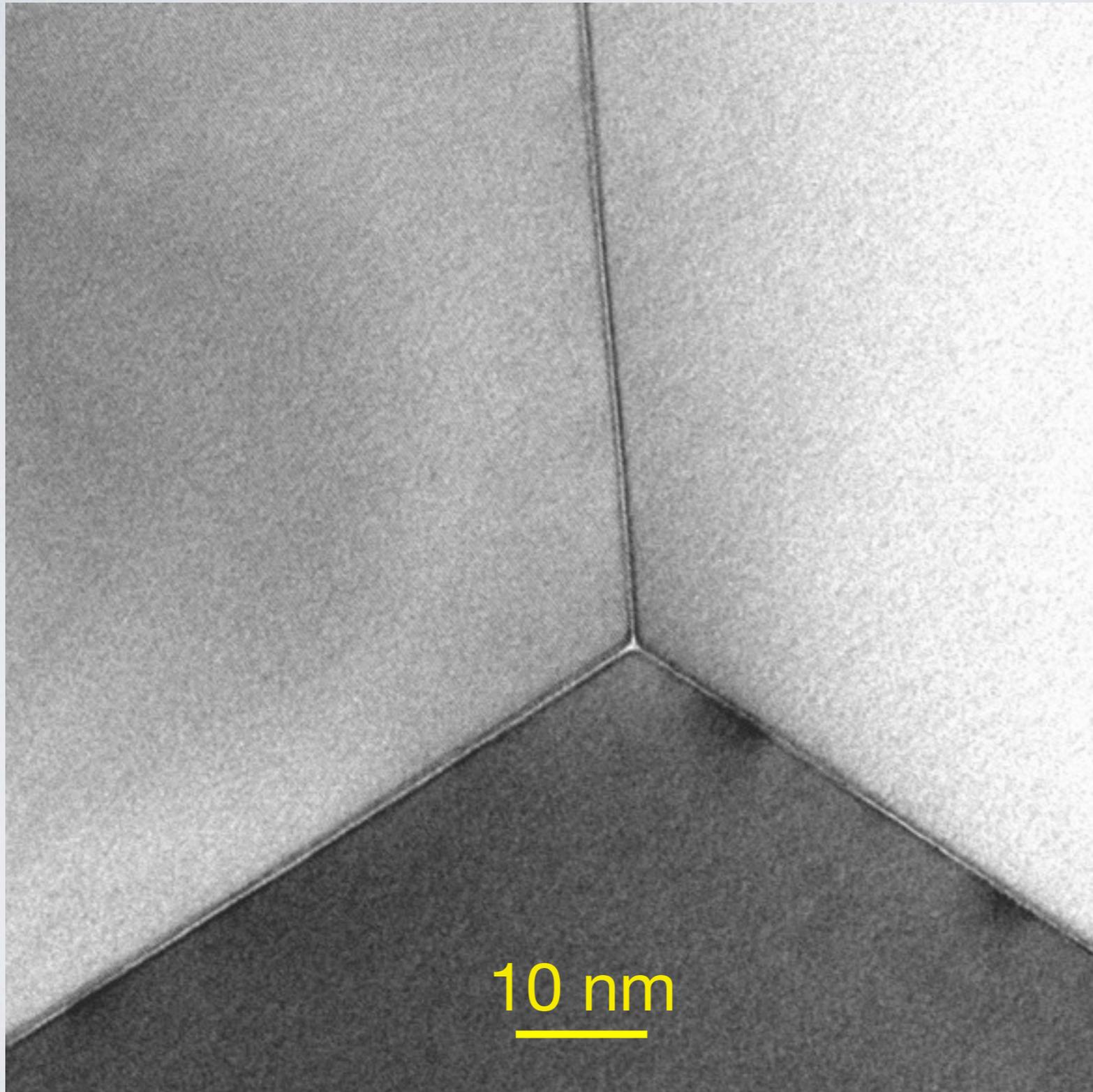
Microstructure: melt-free polycrystalline olivine



Jackson et al.,
2002

defects: grain boundaries, dislocations

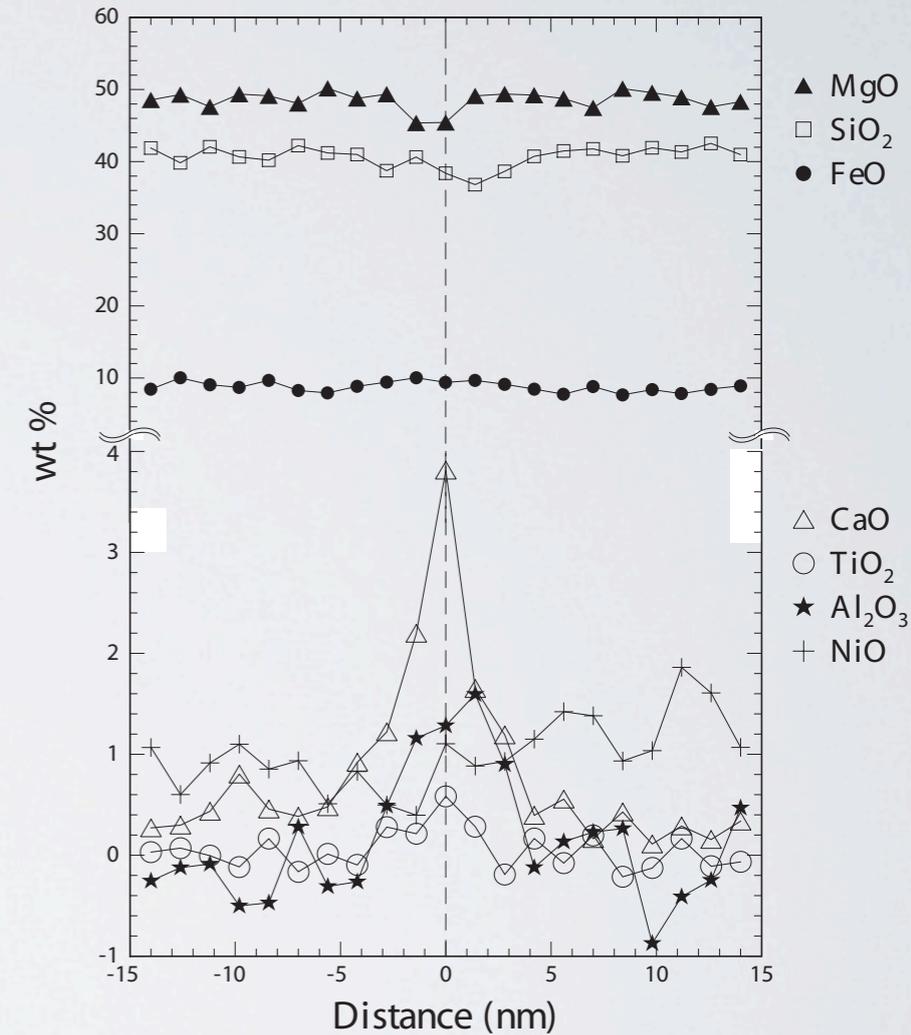
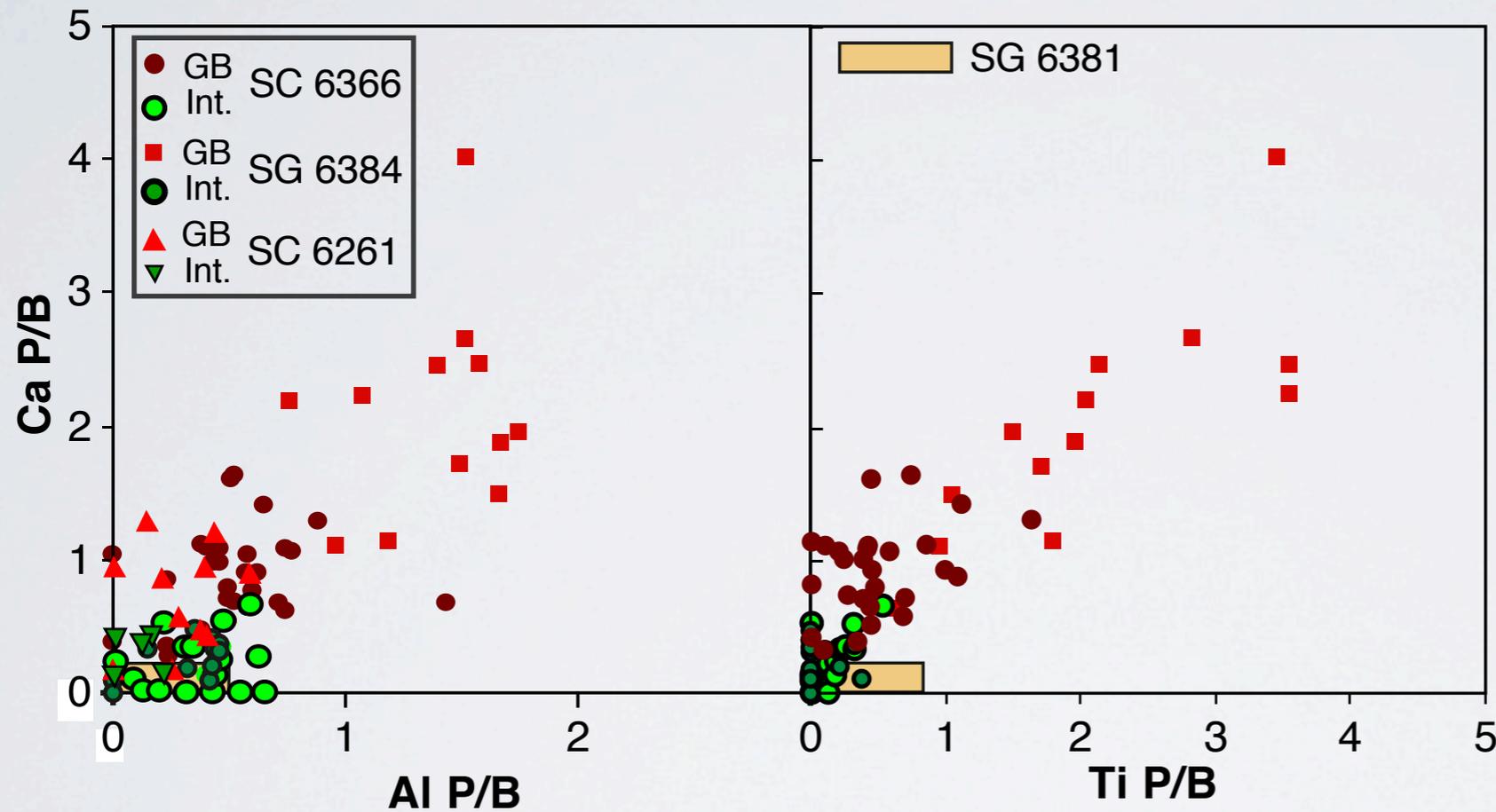
A closer look at grain boundaries:



TEM image of triple junction of melt-free olivine. Grain boundaries oriented parallel to the beam.

Faul et al., 2004

TEM-EDS analyses of high angle grain boundaries

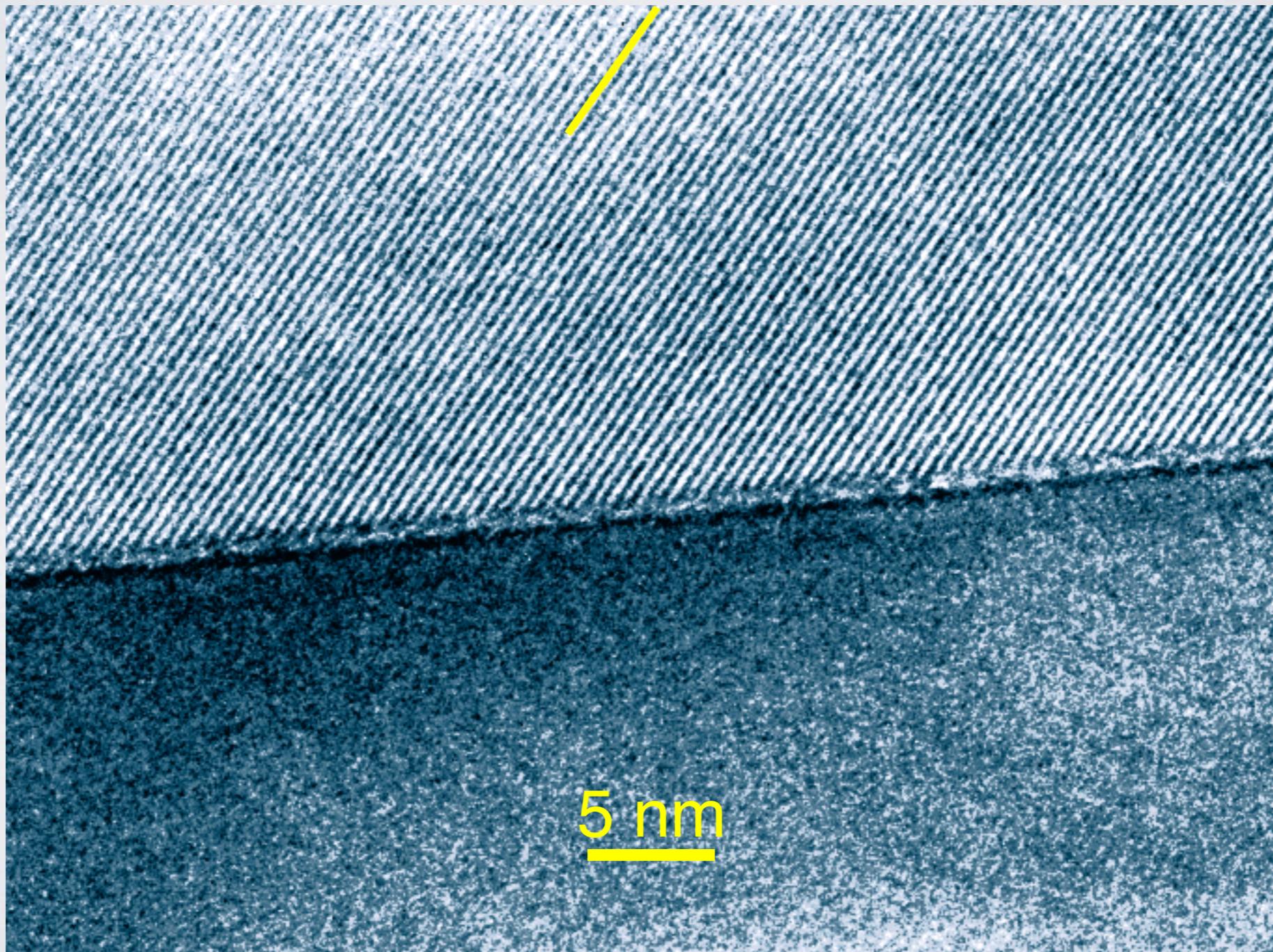


Hiraga et al., 2003

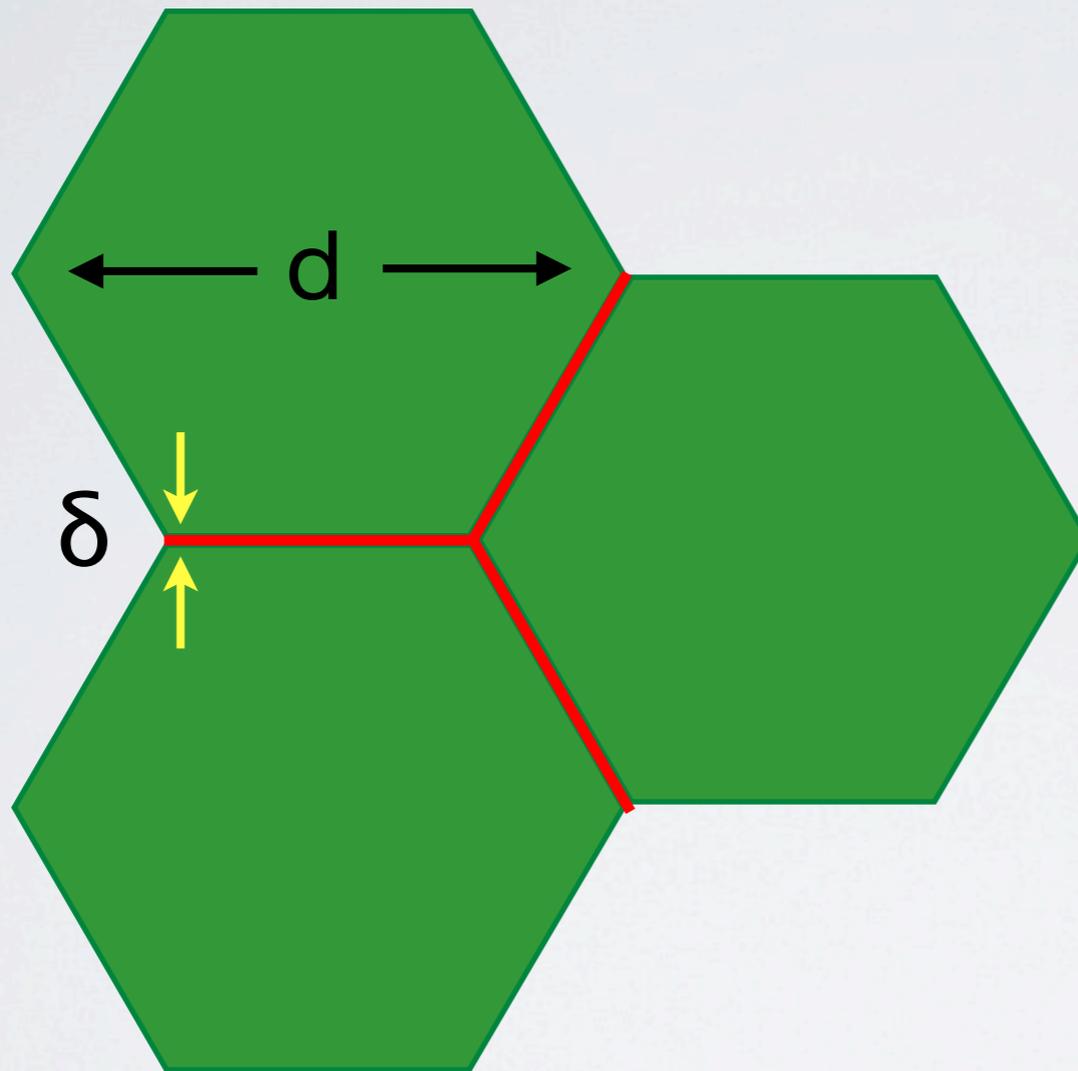
Grain boundaries are trace element enriched relative to grain interiors

High angle (general) grain boundaries in olivine:
smooth (no evidence of steps or dislocation structures),
structurally distinct, ~ 1nm wide, chemically enriched

(010)



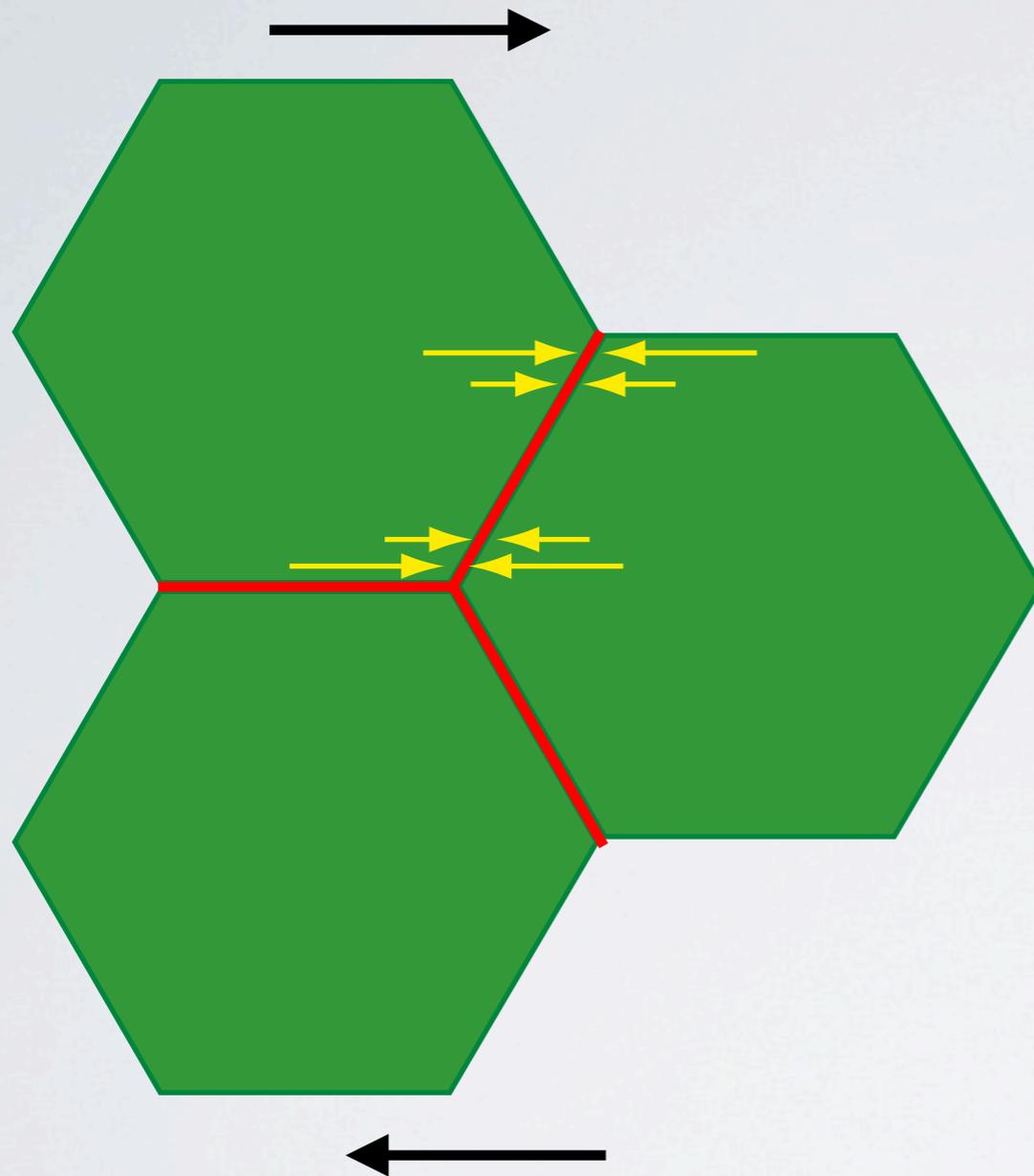
Grain boundary sliding due to shear stress



d grain size, grain
 δ boundary width
 η_{gb} grain boundary
viscosity
 D_{gb} grain boundary
diffusivity

results in three distinct processes:

1. Elastically accommodated sliding



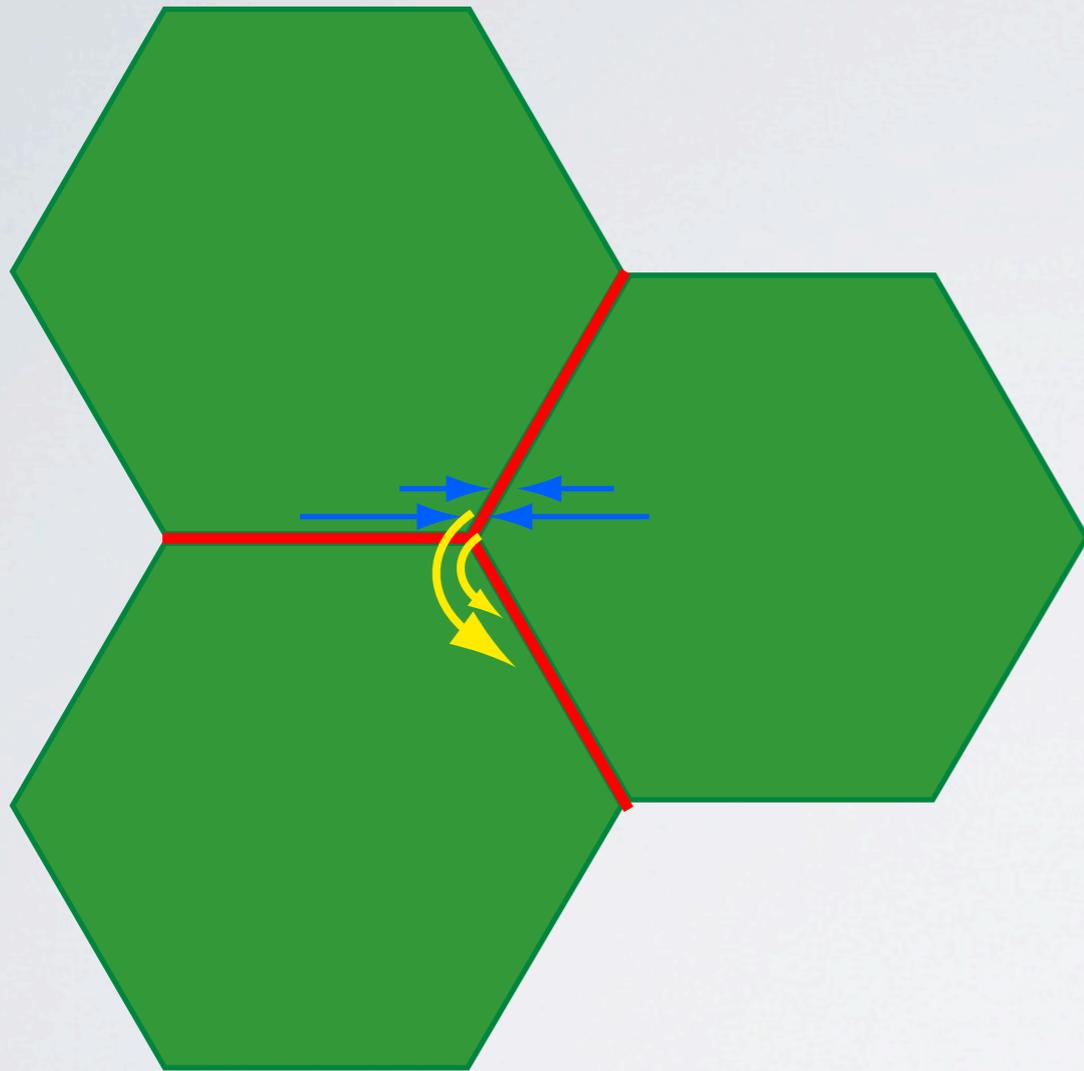
viscous sliding of grain boundaries
leads to elastic stress
concentrations at grain corners

$$\text{time scale: } \tau_E = \eta_{gb} d/G \delta$$

recoverable strain, anelastic process

After Raj and Ashby, 1971; Raj, 1975

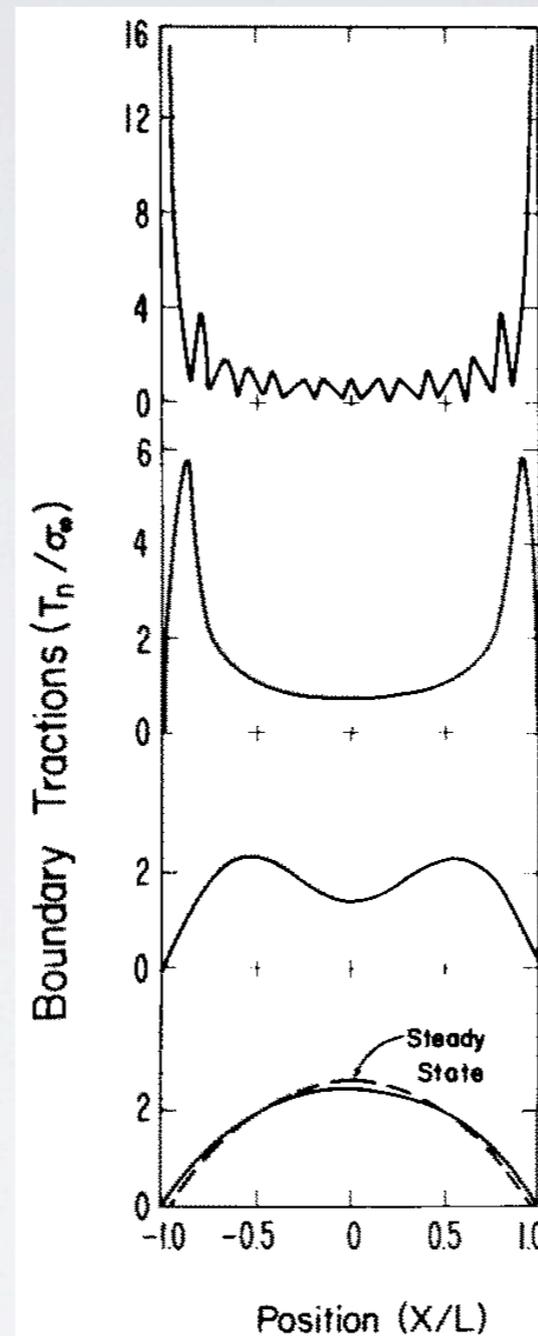
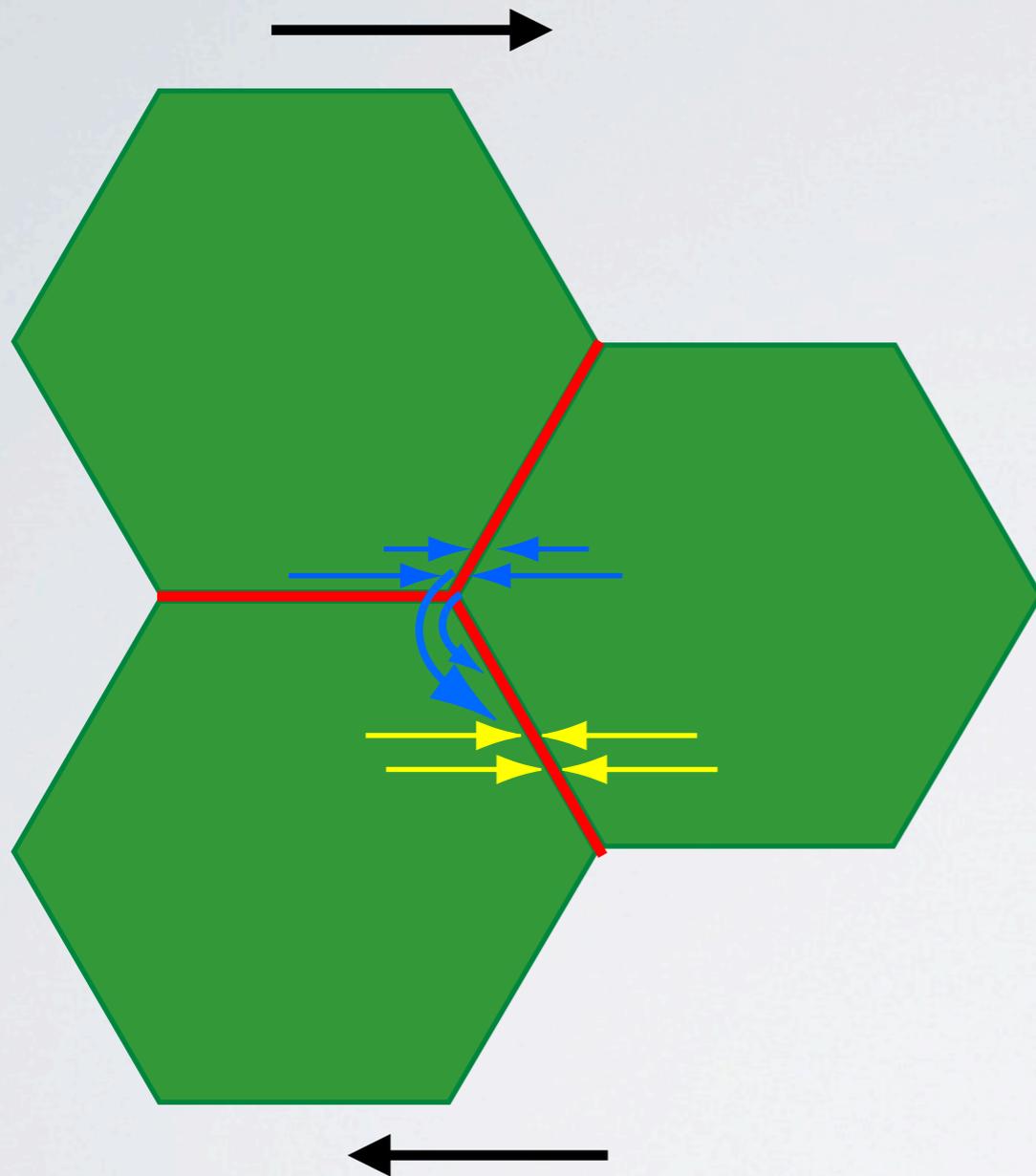
2. Diffusionally assisted sliding



- stress concentrations cause diffusion away from corners
- transient phase is characterised by diffusion over increasing length scales

transient but 'viscous' process

3. Diffusionally accommodated sliding (steady state)

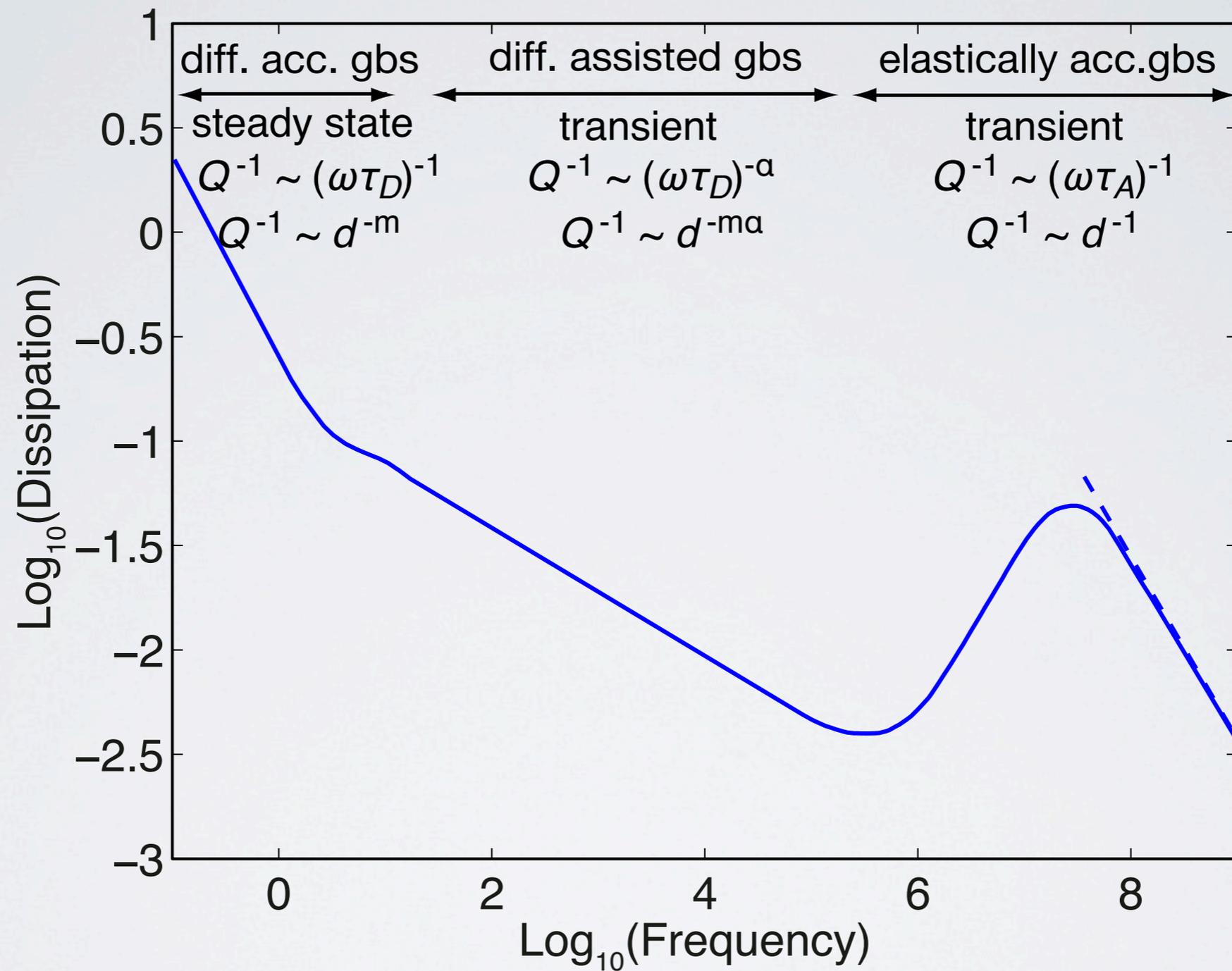


Raj 1975,
Gribb &
Cooper, 1998

time scale: $\tau_D \sim T d^3 / G \delta D_{gb}$

gb normal stresses are highest in center between grain corners (steady state diffusion creep)

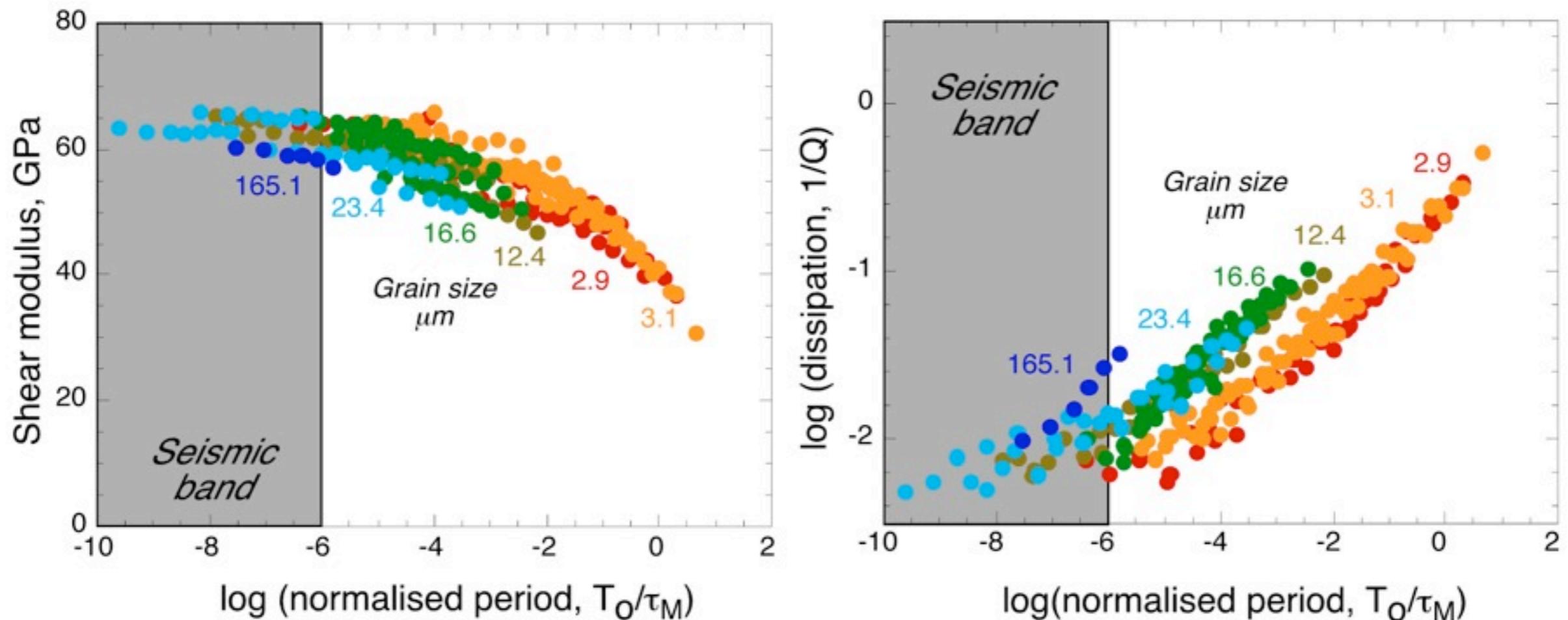
Frequency domain model (Morris and Jackson, 2009, Lee et al., 2011)



grain size dependence changes from
 \sim linear (transient) to cubic (steady state)

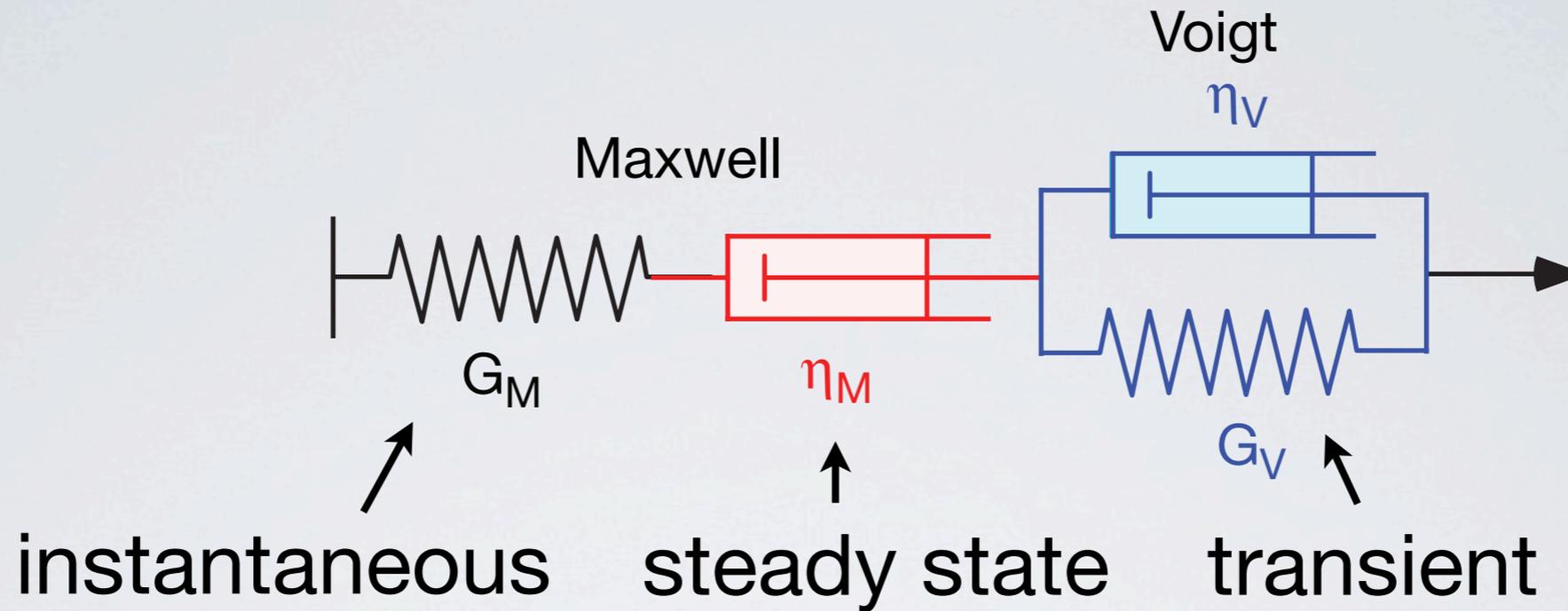
DEPARTURES FROM THE MASTER CURVE

ANU essentially melt-free olivine, $800 < T(C) < 1200$, $1 < T_o(s) < 1000$, $\eta_{ss} \sim d^3$



Q^{-1} is more mildly grain-size sensitive than expected from scaling with the Maxwell time $\tau_M = \eta_{ss}/G_U \sim d^3 \exp(E/RT)$ for Coble creep
 -> transient close to linear in grain size dependence

Data fitting: (extended) Burgers model



Time domain: strain as a function of time (creep function)

$$J(t) = J_M + t/\tau_M + J_V (1 - \exp(-t/\tau_V))$$

$$J_M = 1/G_M; \tau_{M,V} \text{ relaxation times}$$

Frequency domain:

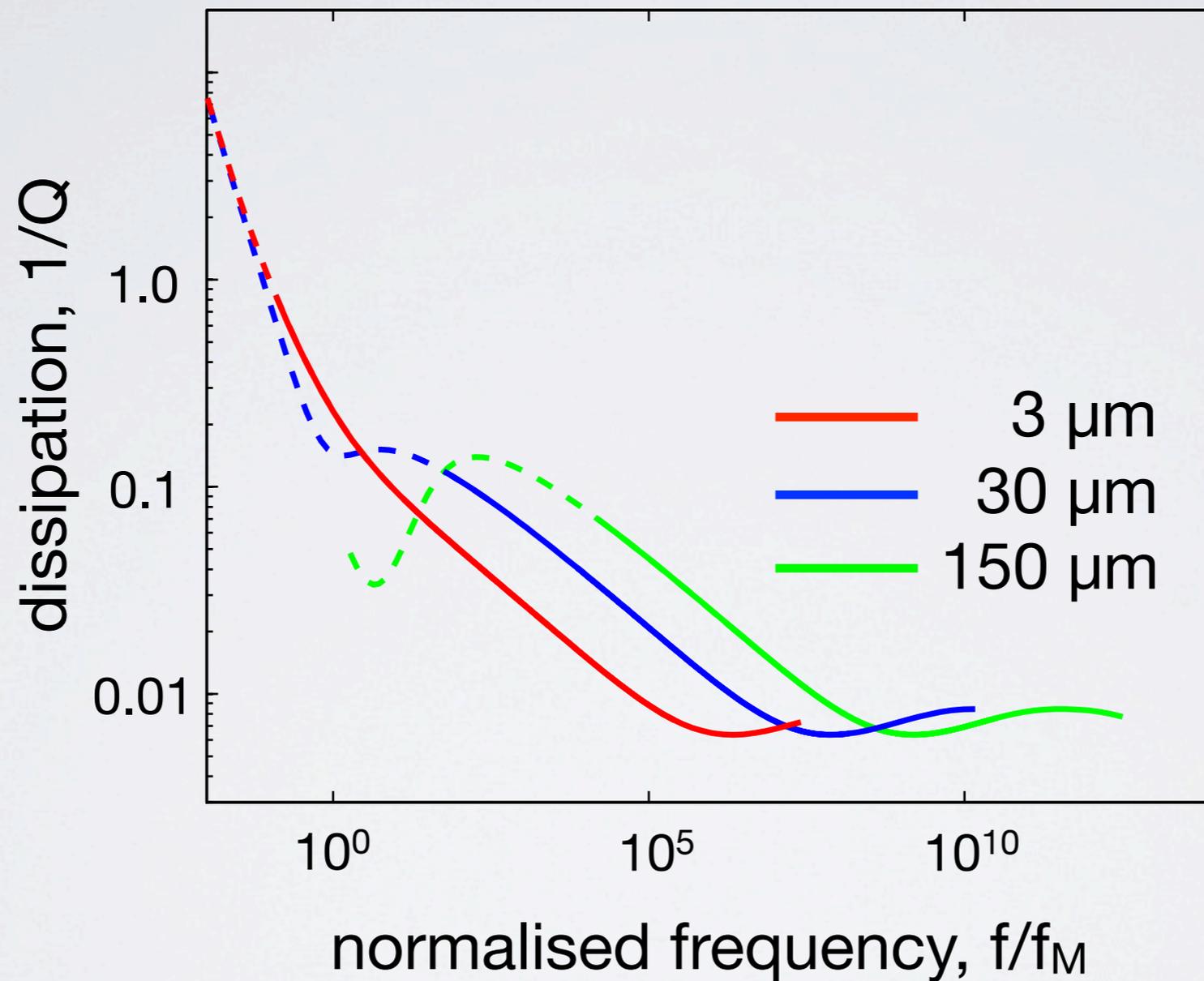
$$J_1(\omega) = J_M + J_V / (1 + \omega^2 \tau_V^2),$$

$$J^*(\omega) = J_1(\omega) + i J_2(\omega)$$

$$J_2(\omega) = J_V \omega \tau_V / (1 + \omega^2 \tau_V^2) + 1/\omega \tau_M$$

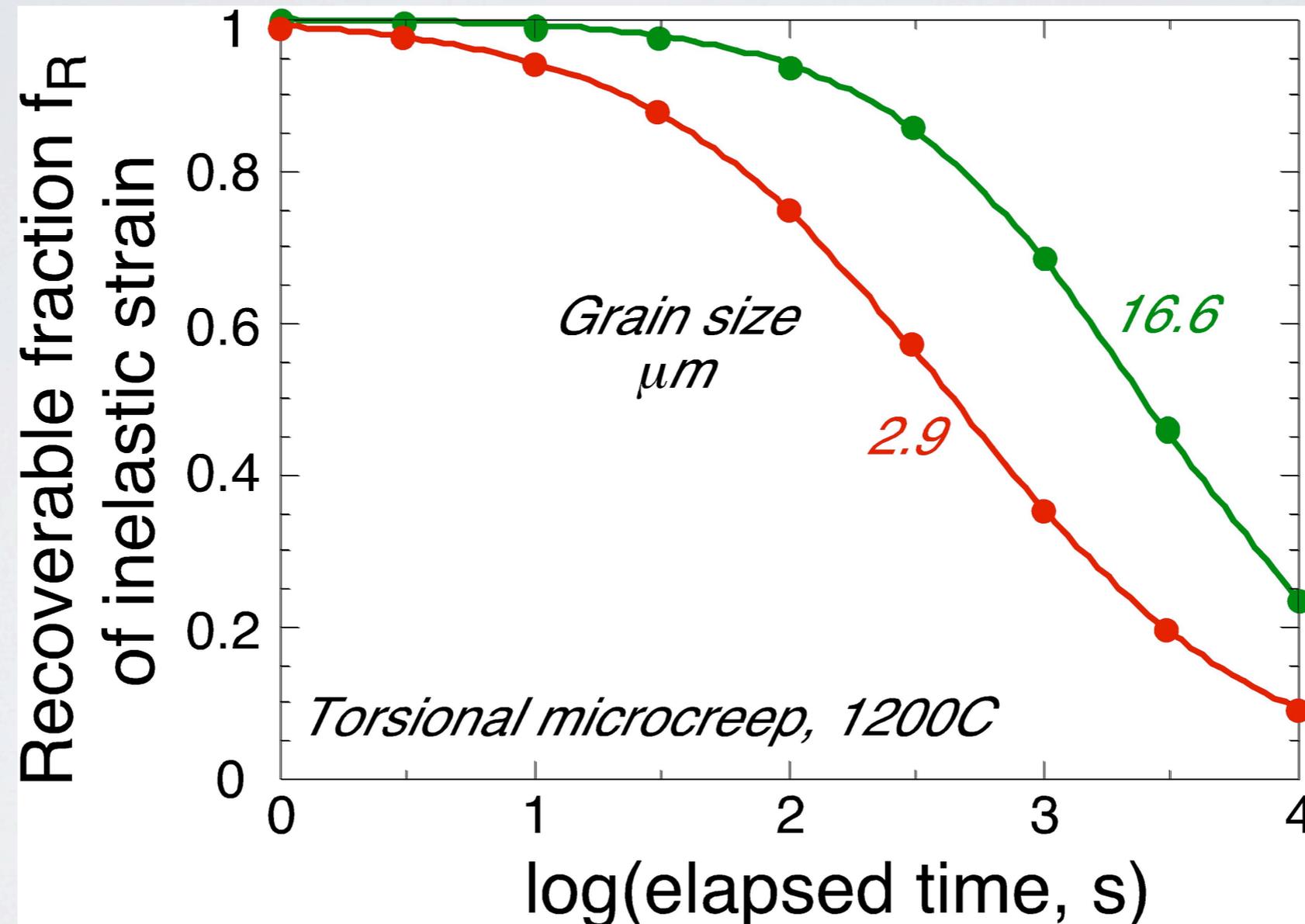
$$G(\omega) = [J_1^2(\omega) + J_2^2(\omega)]^{-1/2} \quad Q(\omega) = J_1(\omega)/J_2(\omega)$$

Extended Burgers model fit to forced oscillation data for olivine



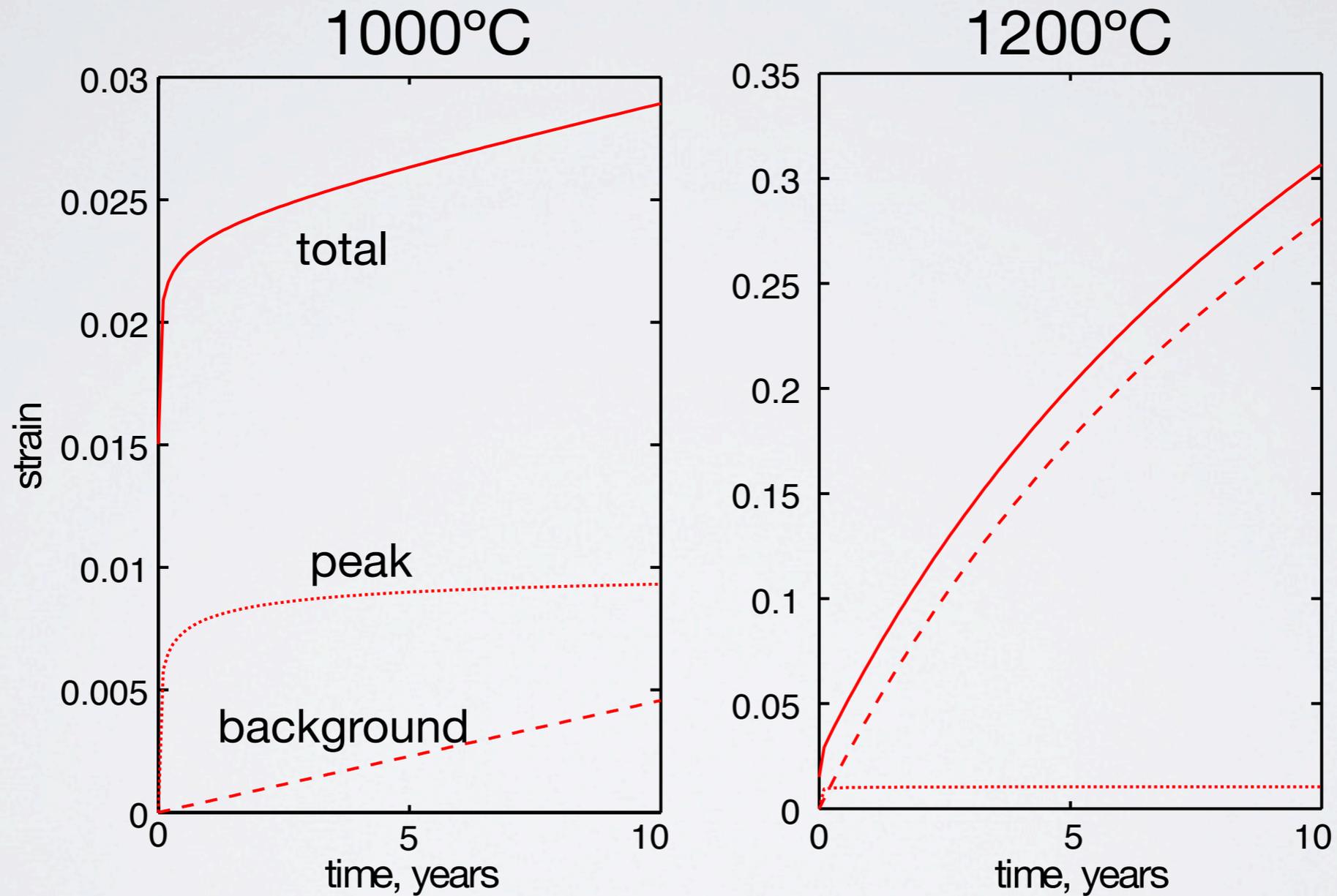
curves 'collapse' in Maxwell regime ($f < f_M$); spread due to linear grain size dependence in transient regime

Microcreep records: Recoverable (elastic + anelastic) portion of strain decreases with time



transient is (near linearly) grain size dependent

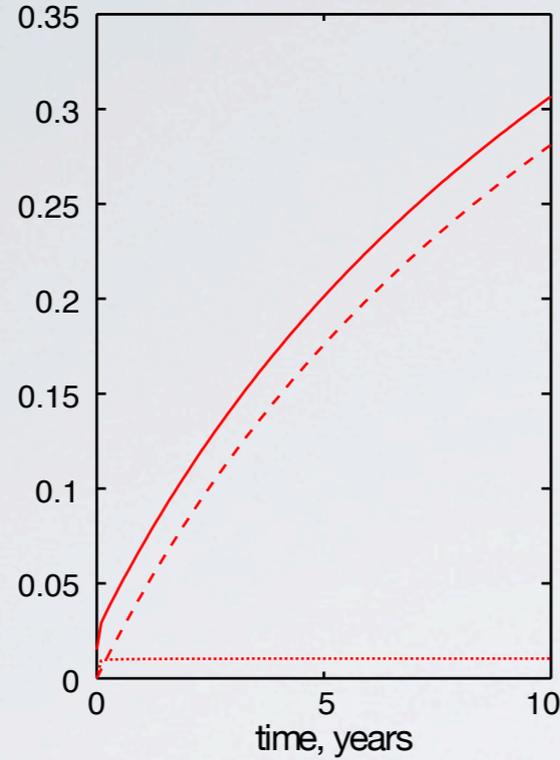
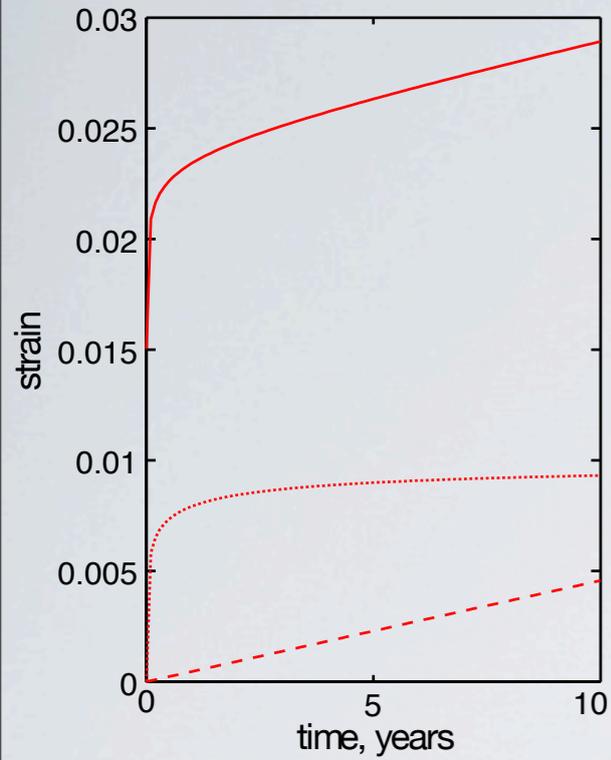
Extended Burgers model calculation of transient strain, extrapolated to 1 cm grain size



1000°C

1200°C

Comparison with creep observed by GPS in Southern California applicable at small strains (far field)



Freed et al., 2010

solid lines: observations
dashed: steady state creep models

