

# Application and Validation of Simulated BBP & Cybershake Motions for Building Response Analyses

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# Background

**Broad objective:** Test and validate the use of **simulated ground motions from SCEC's Broadband Platform (BBP) & Cybershake** in nonlinear response history analysis and collapse assessment of tall buildings.

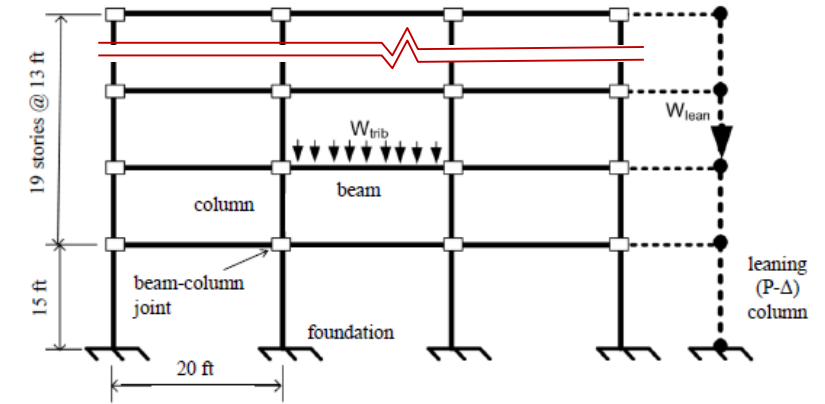
**Scope:** For two archetype buildings at three sites,

1. Select hazard-consistent ground motions for target hazard parameters ( $S_a$  response spectra intensity, shape and duration)
2. Analyzed structural responses under recorded and simulated motions, which are selected/scaled to the same target spectra
3. Contrast and evaluate building demand parameters
4. Identify the benefits and limitations of using simulated earthquake seismograms in engineering applications.

# Archetype Buildings

## 20-story RC frame

- **Archetype ID:** 1020 (FEMA P695)
- **Modeling:** Cyclic hinge model for beams and columns in the lateral frame + leaning system (gravity frame)
- **Period:**  $T_1 = 2.6$  sec,  $T_2 = 0.9$  sec



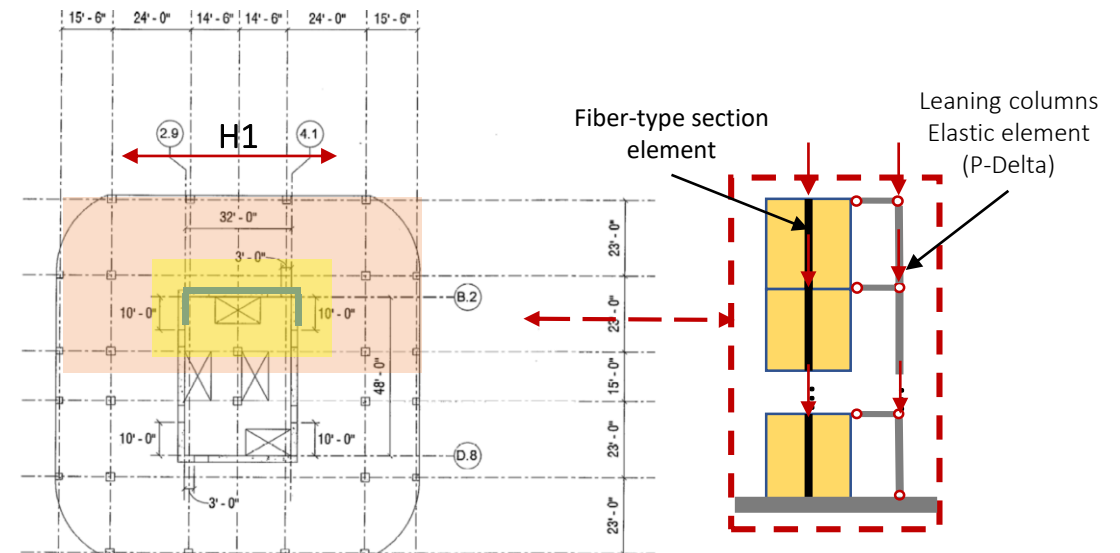
2D OpenSEES model: 20-story RC frame

## 42-story RC frame

- **Archetype ID:** simplified from TBI building 1C (H1 direction)
- **Modeling:** force-based fiber element for shear wall + leaning system (gravity frame)
- **Period:**  $T_1 = 4.2$  sec,  $T_2 = 1.0$  sec



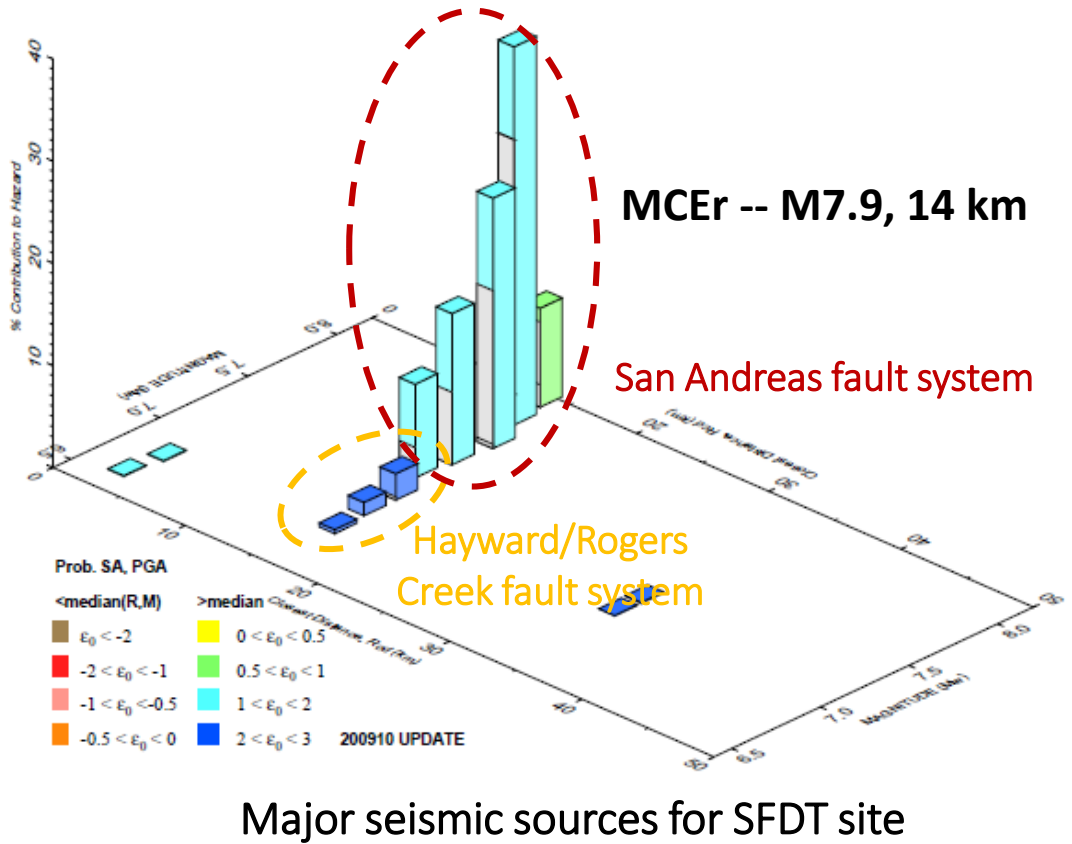
42-story shearwall building (PEER TBI)



2D OpenSEES model

# San Francisco Downtown, SFDT (8029-RIN)

*[1728 BBP Records]*



## Key Focus Areas

## GM selection

1. *Single-target IMs (Conditional Spectra + duration)*
2. *ASCE-7 MCER procedure*
3. *Simulated BBP is more consistent with governing hazard (requiring less scaling)*

## Structural response & collapse

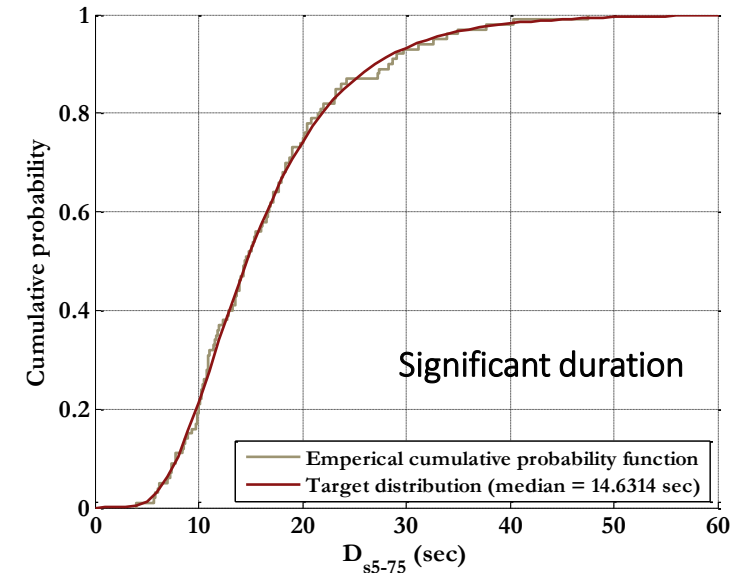
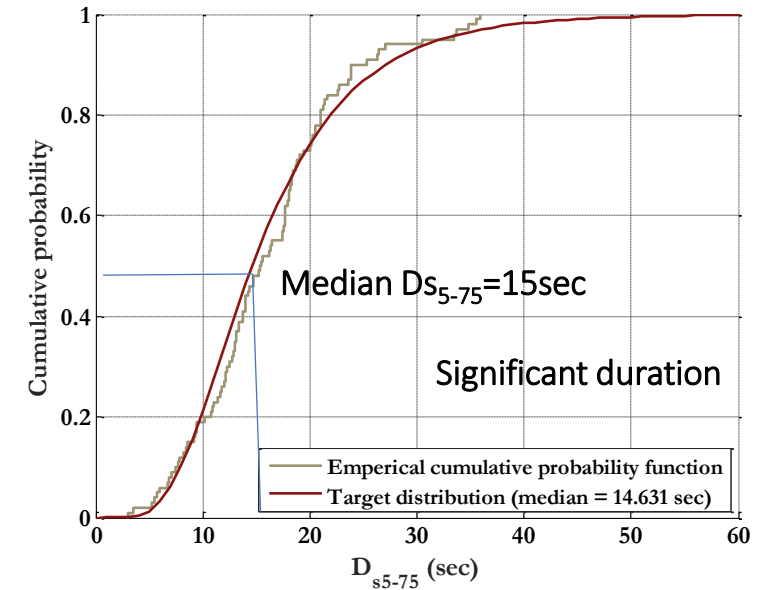
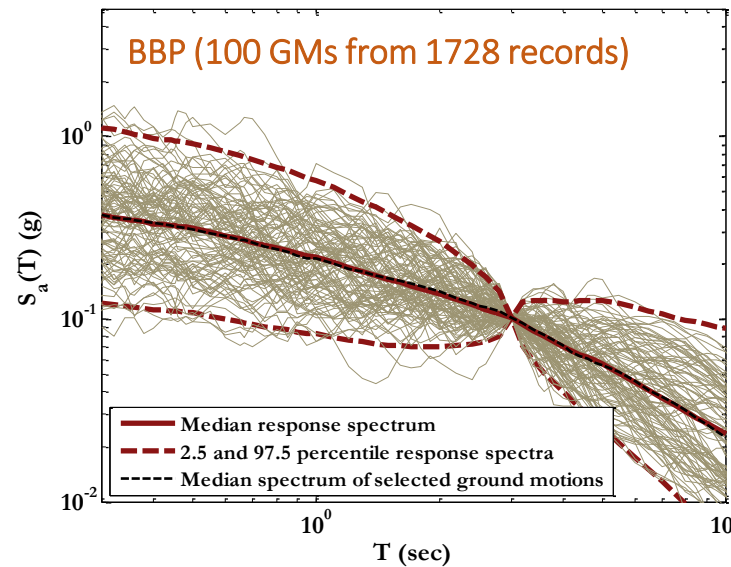
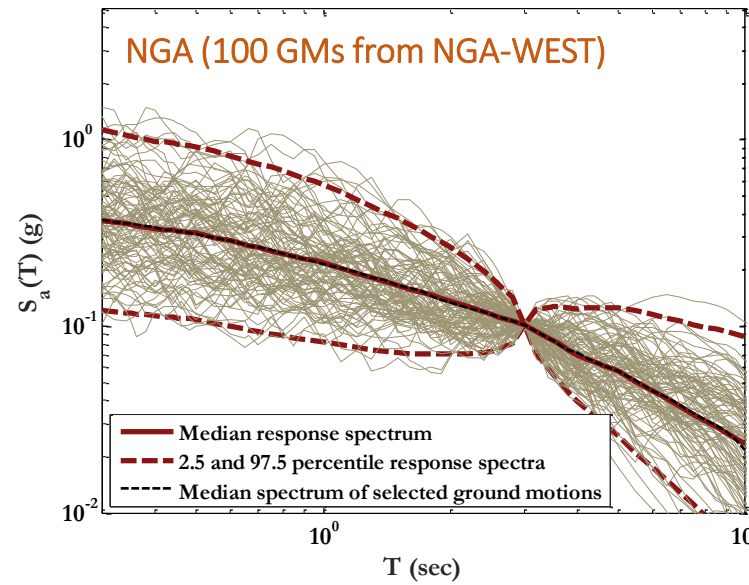
1. *Ability to match targets*
2. *Sensitivity of response to GMs*
3. *Contrasting CS versus UHS*

## Intensity Measures (IMs)

- **Target:** Conditional Spectra (**CS**)<sup>[1]</sup> and significant duration,  **$Ds_{5-75}$** <sup>[2]</sup>
- Prediction equations for spectral acceleration,  $S_a$ <sup>[3]</sup> and duration<sup>[4]</sup> with correlations to construct Generalized Conditional Intensity Measure (**GCIM**)<sup>[5]</sup>:  $CS + Ds_{5-75}$

## Ground motion selection

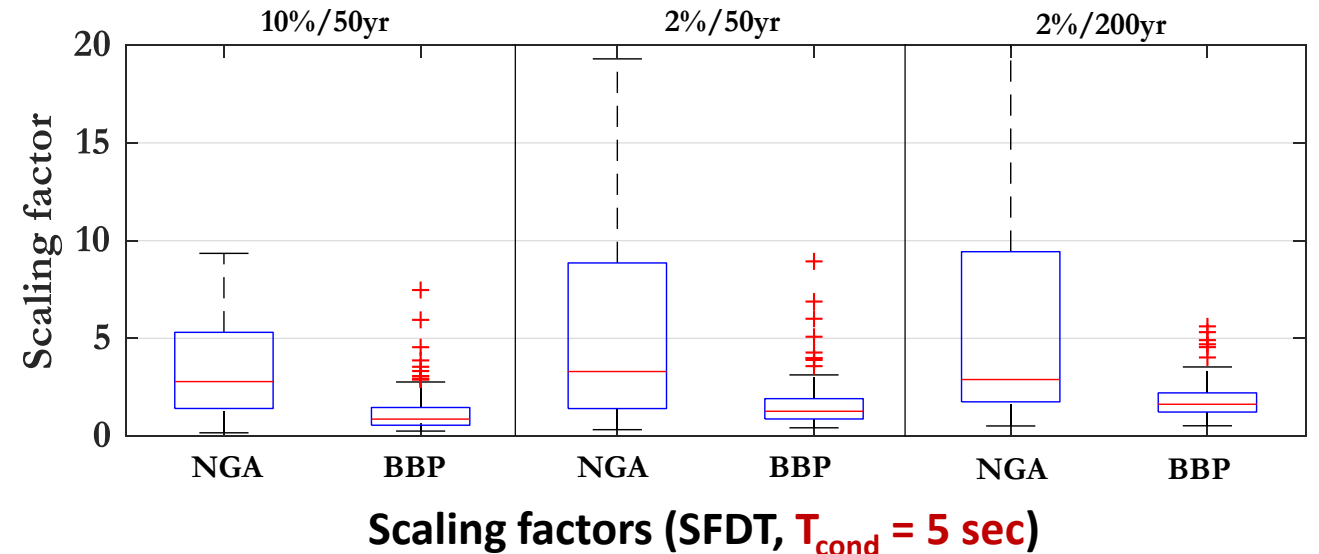
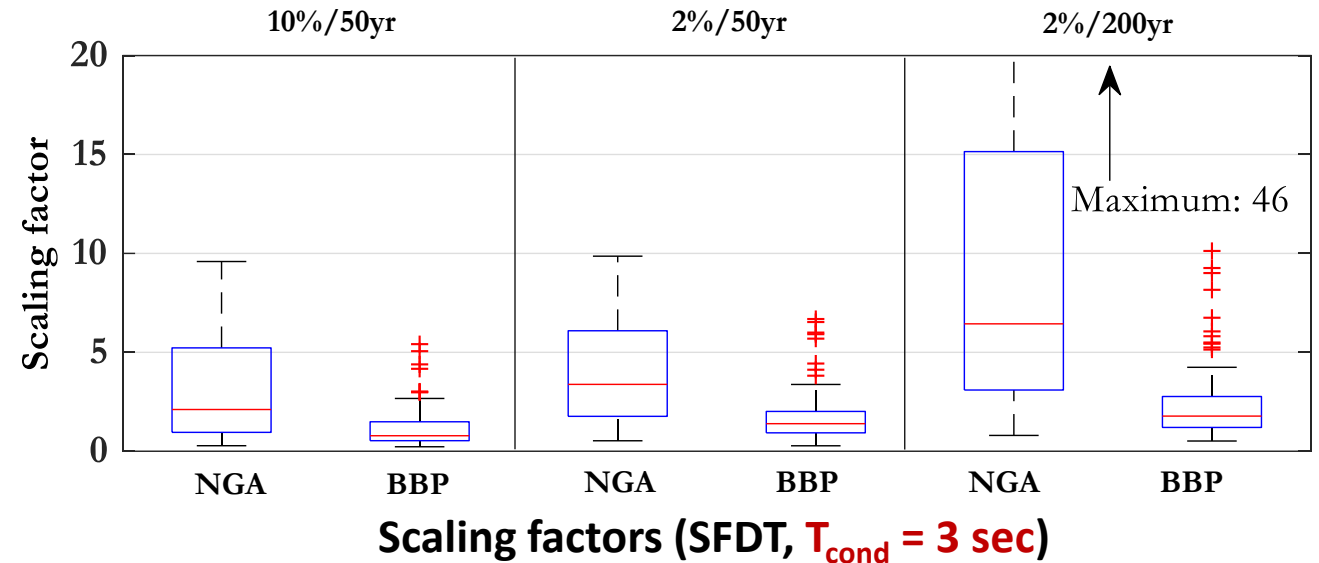
- Expanded selection algorithm<sup>[6]</sup> with different weights to CS and duration<sup>[7]</sup> to optimize selection
- **Results (10%/50yr & 2%/50yr):** Recorded **NGA** and simulated **BBP** motions **match target IMs well**



**Ground motion selection ( $T_{\text{cond}} = 3 \text{ s}$ , SFDT, 10%/50yr)**

## Scaling factor

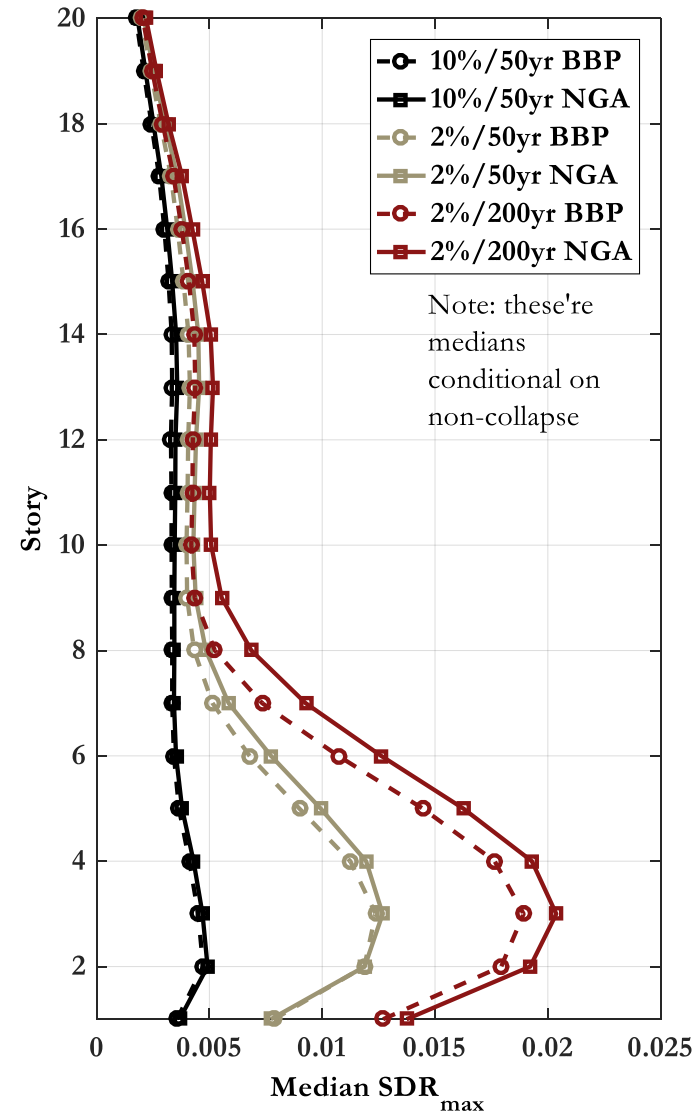
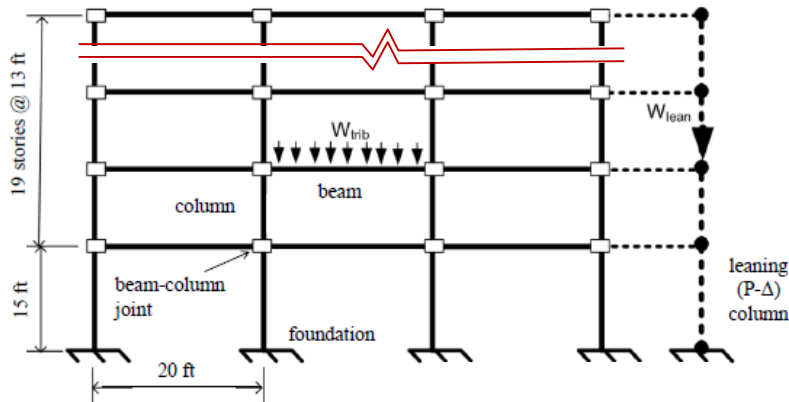
- Since **BBP** (v17.3, Part C) records are simulated from large events, they generally need much **smaller scaling factors** compared to NGA records
- The benefit of BBP (and simulations such as CyberShake) to avoid large scaling factors is apparent at high intensity levels
- Constrained by the number of simulation runs



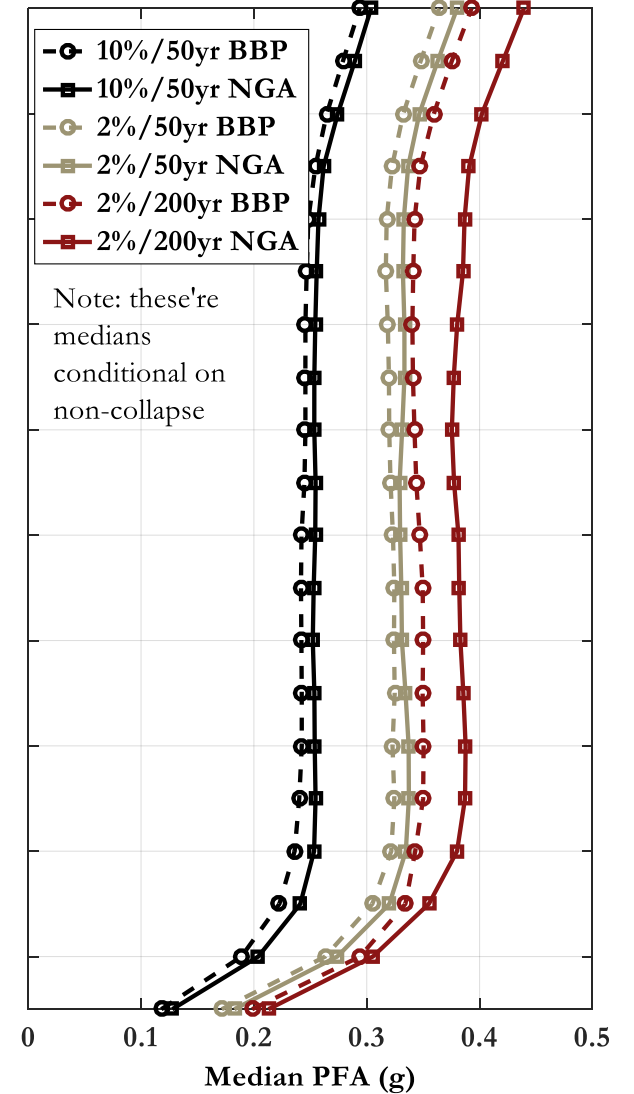
# Multi-Stripe Analysis (MSA)

## 20-Story Frame Response

- *Maximum Story Drift Ratio ( $SDR_{max}$ )*
  - *Comparable up to 2%/50yr*
  - *<10% difference under 2%/200yr*
- *Peak Floor Acceleration (PFA)*
  - *Comparable up to 2%/50yr*
  - *~10% difference under 2%/200yr*



Maximum Story Drift Ratio

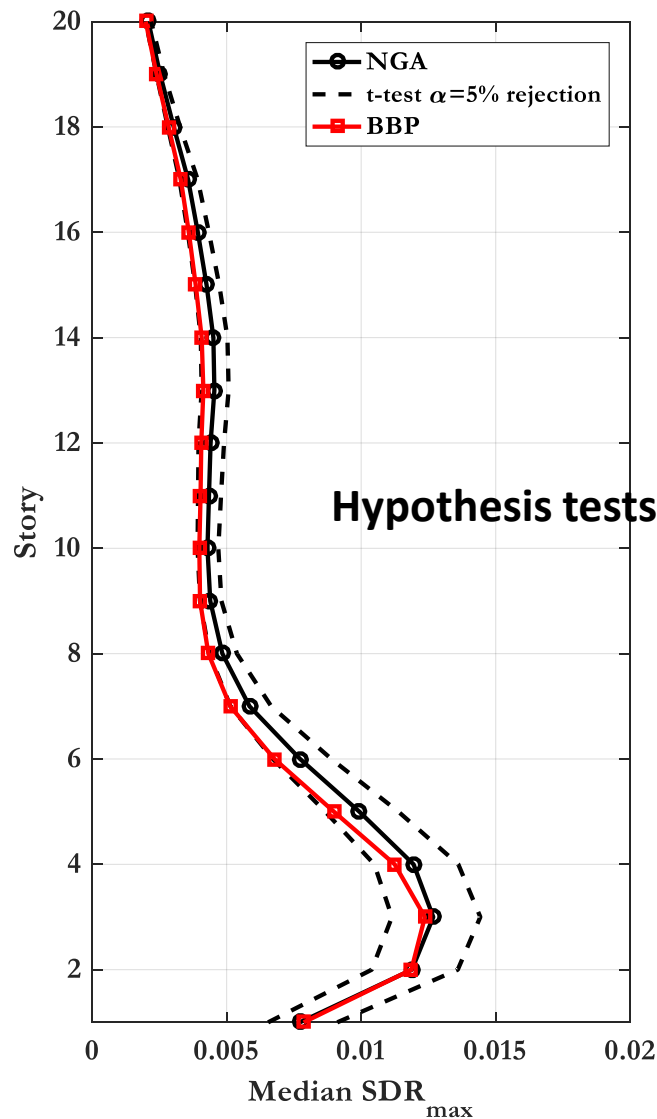
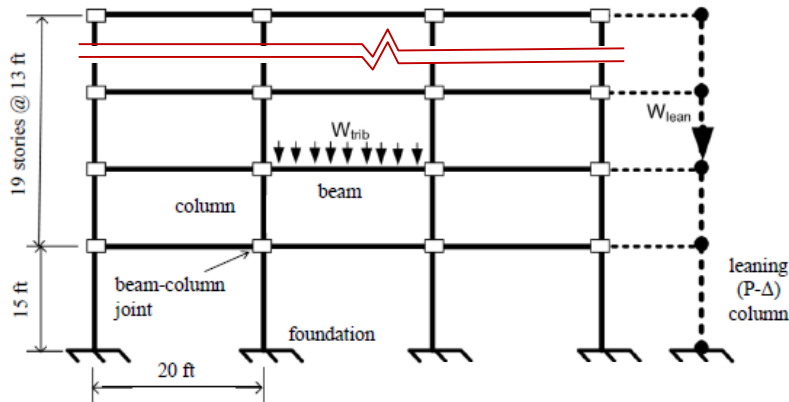


Peak Floor Acceleration

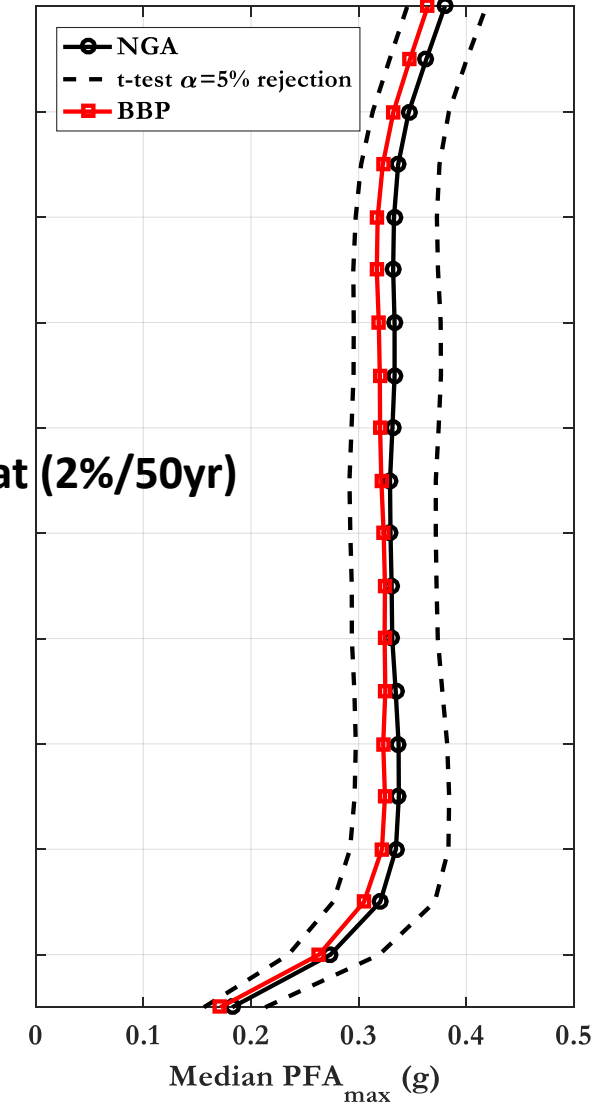
# Multi-Stripe Analysis (MSA)

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Maximum Story Drift Ratio

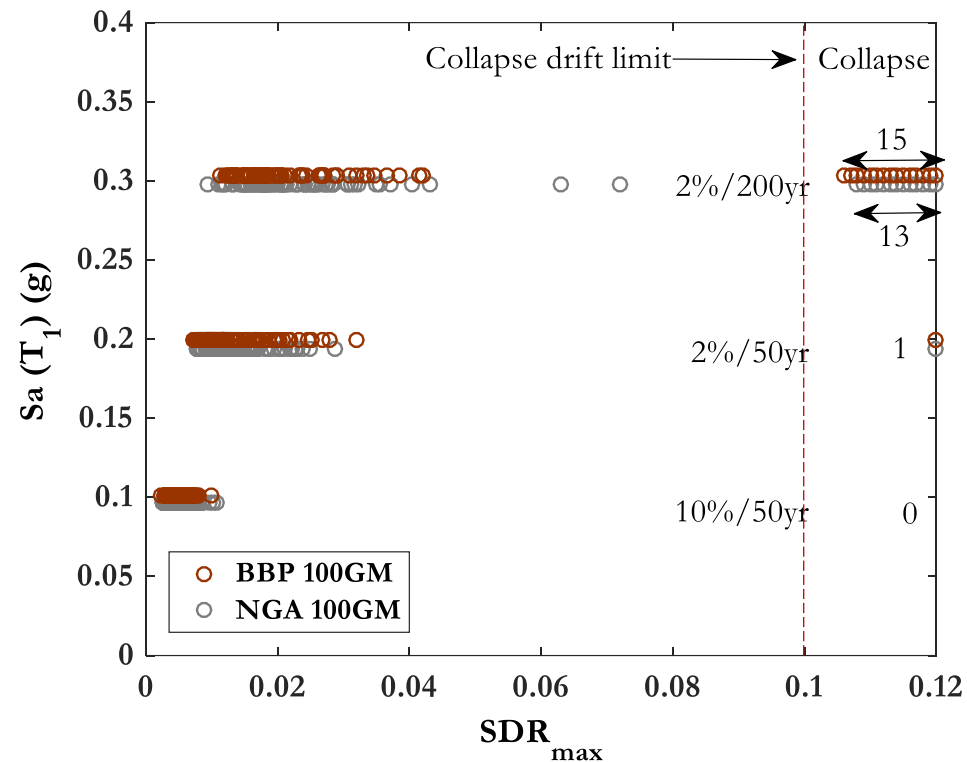


Peak Floor Acceleration

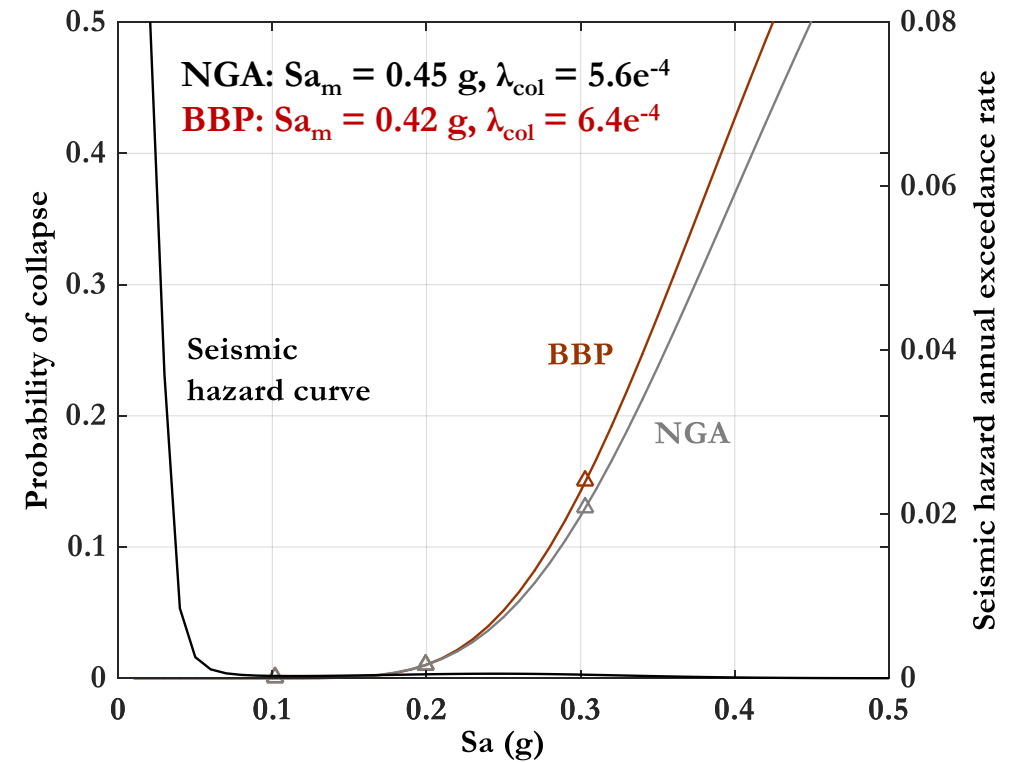


## Collapse risk (20-story RC frame)

- NGA and BBP motions yield the same number of collapses at 10%/50yr and 2%/50yr levels
- Collapse (2%/200yr): BBP 15 vs. 13 NGA
- About 7% difference in median collapse intensity and about 15% difference in mean annual frequency (MAF) of collapse



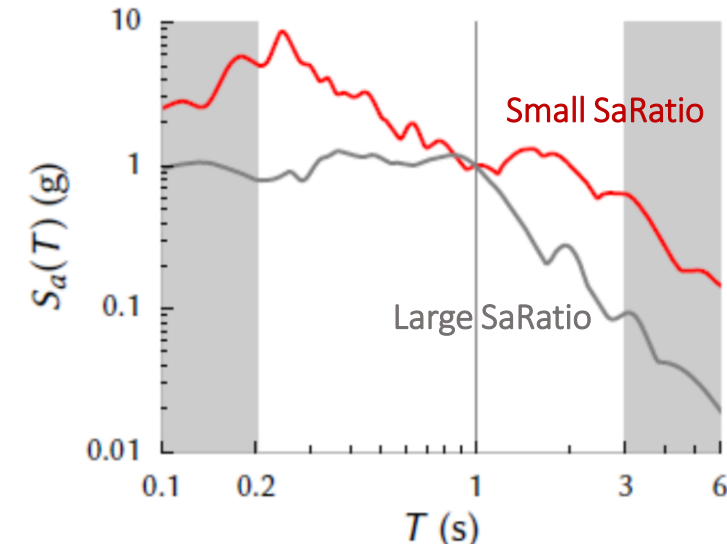
Stripe Analysis - Story Drift Ratios



Collapse Fragilities

## Collapse deaggregation (20-story RC frame)

Although both selected GM sets fit the target Conditional Spectra, the BBP set has more records with smaller SaRatio's. This contributes to a slightly higher estimated collapse probability at 2%/200yr.

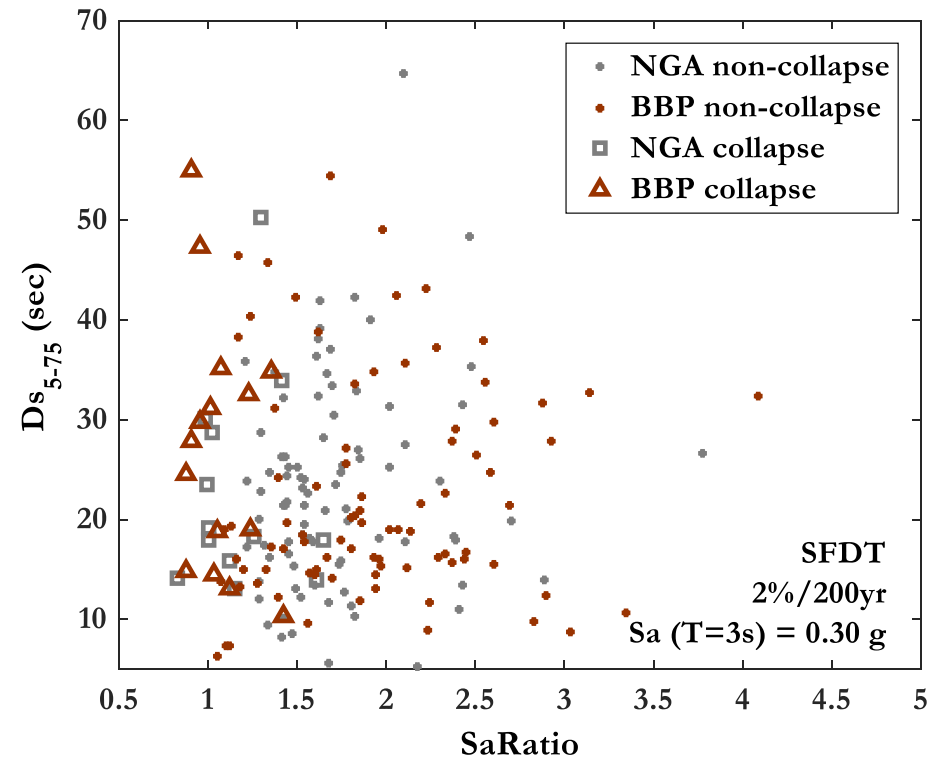


$$Sa,avg(T_0, T_2) = \exp \left[ \frac{\int_{T_0}^{T_2} \ln Sa(\tau) d\tau}{T_2 - T_0} \right]$$

$$SaRatio(T_0, T_1, T_2) = \frac{Sa(T_1)}{Sa,avg(T_0, T_2)}$$

## Sa,average & SaRatio

- $Sa,avg$ : average PSA values over a period range
- $SaRatio$ : the ratio between  $Sa(T_1)$  and  $Sa,avg$ , which describes the period-dependent spectral shape

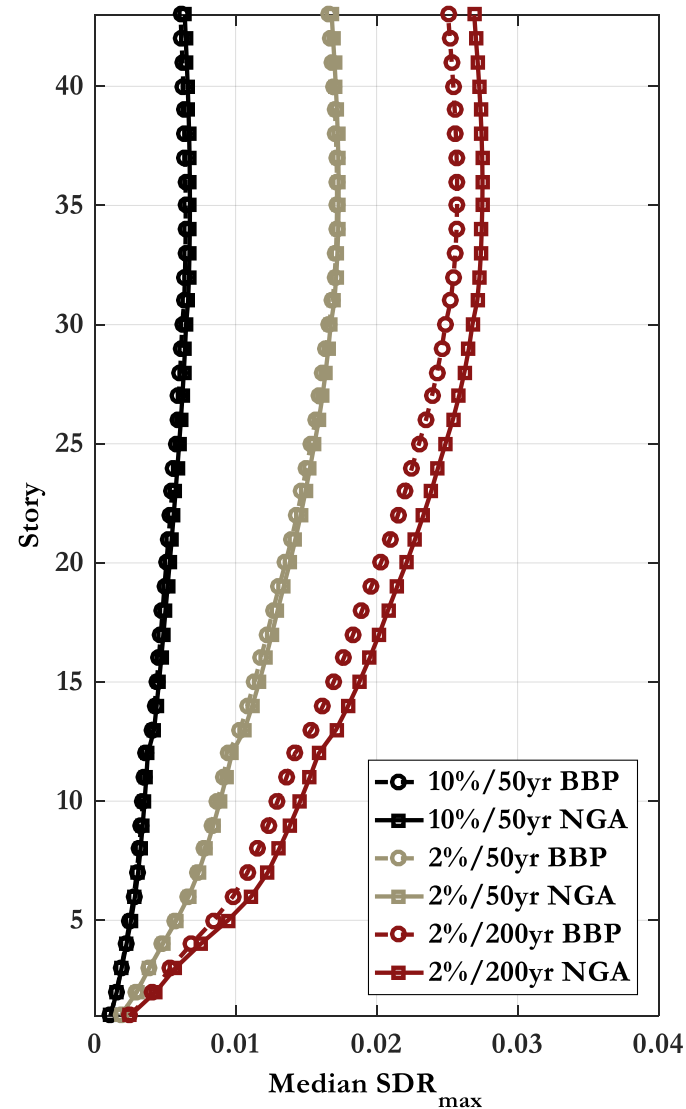


## Collapse deaggregation (100 GMs)

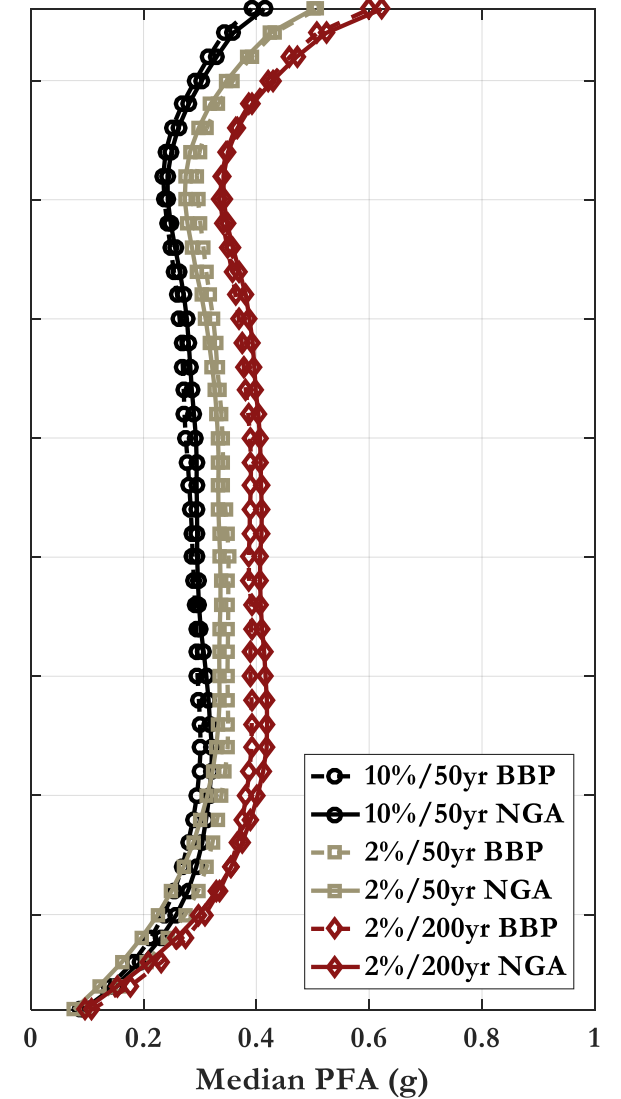
# Multi-Stripe Analysis (MSA)

## 42-story shearwall

- *Maximum Story Drift Ratio ( $SDR_{max}$ )*  
*Comparable up to 2%/50yr*  
*<10% difference under 2%/200yr*
- *Peak Floor Acceleration (PFA)*  
*Comparable up to 2%/50yr*  
*<10% difference under 2%/200yr*



Maximum Story Drift Ratio



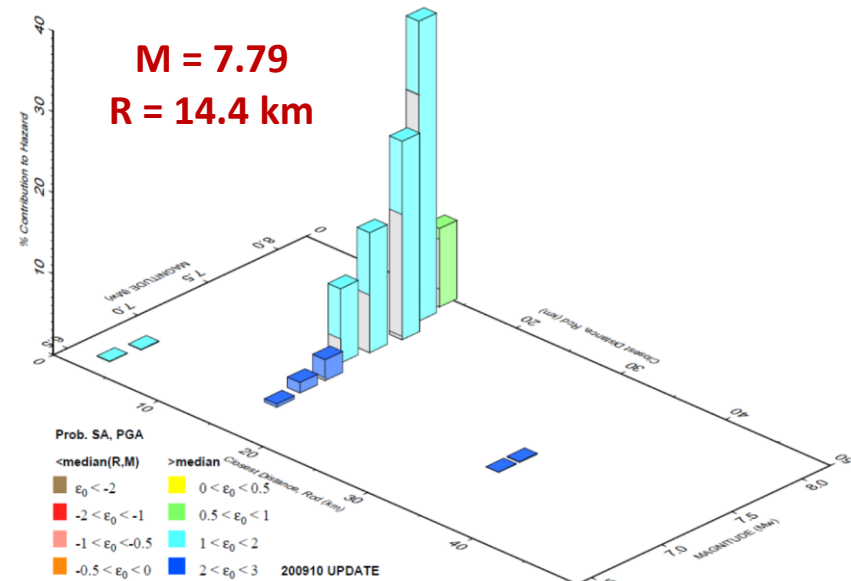
Peak Floor Acceleration

# ASCE 7-16 Procedure

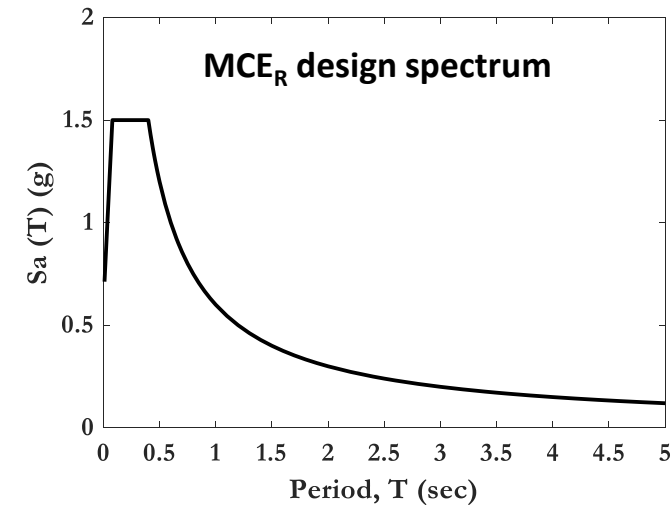
## Ground motion selection

- *Site information:*
  - *Site class: B*
  - $S_s = 1.5 g$
  - $S_1 = 0.6 g$
- *Target: ASCE 7-16  $MCE_R$ /DBE spectrum*
- *Record number: 11*
- *Criteria:*
  - *Consistent  $M$ ,  $R$ , and mechanism*
  - *Close site condition*
  - *Mean  $S_a \geq$  target over  $(0.2T_1 \sim 1.5 T_1)$*

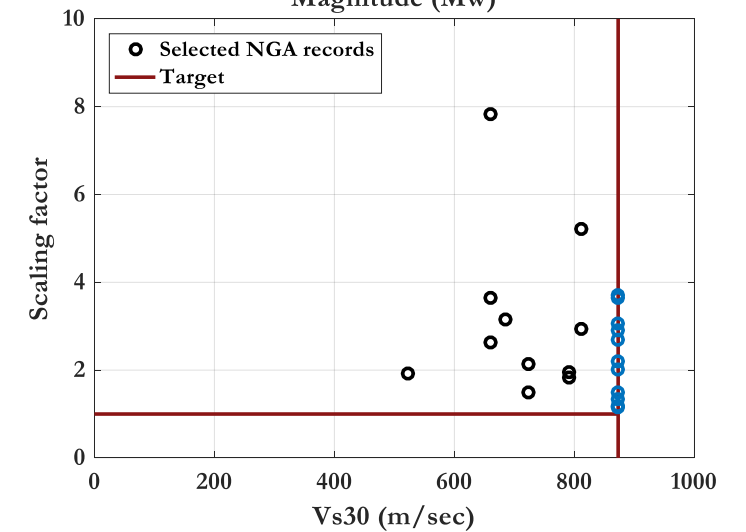
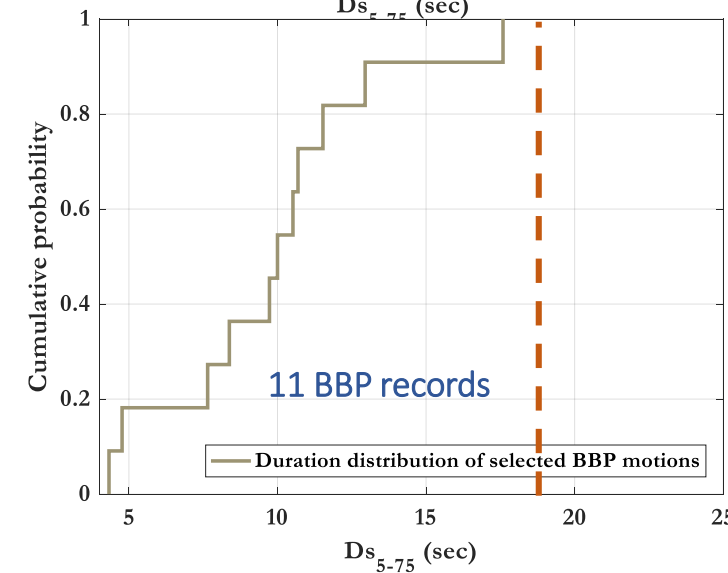
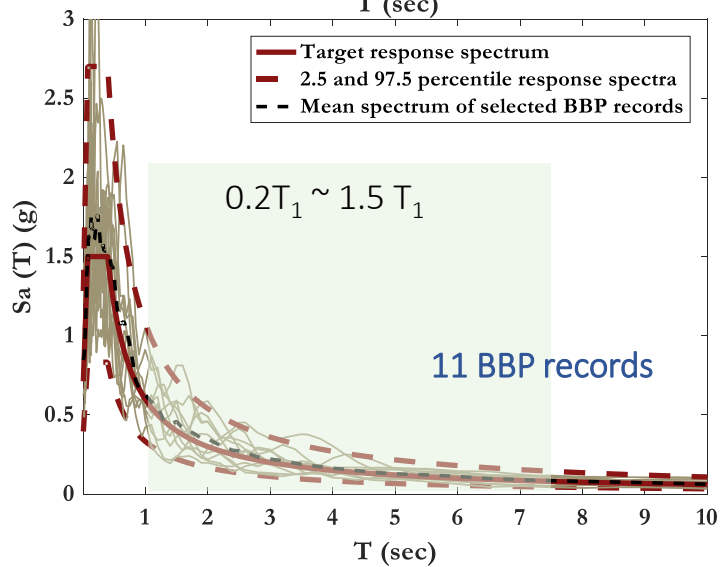
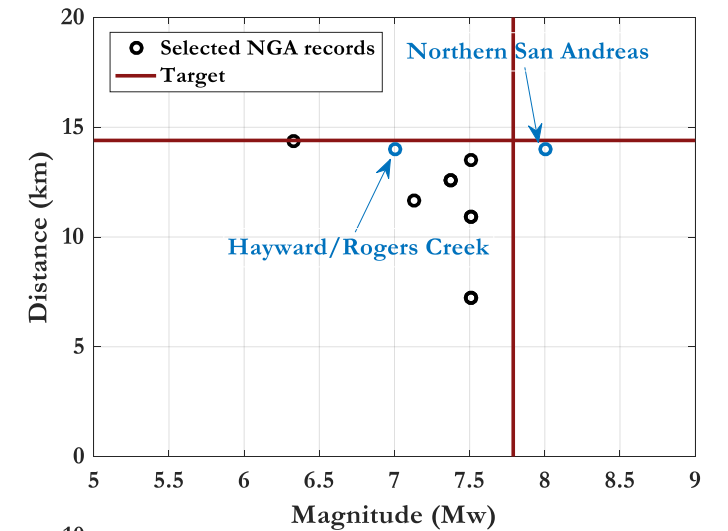
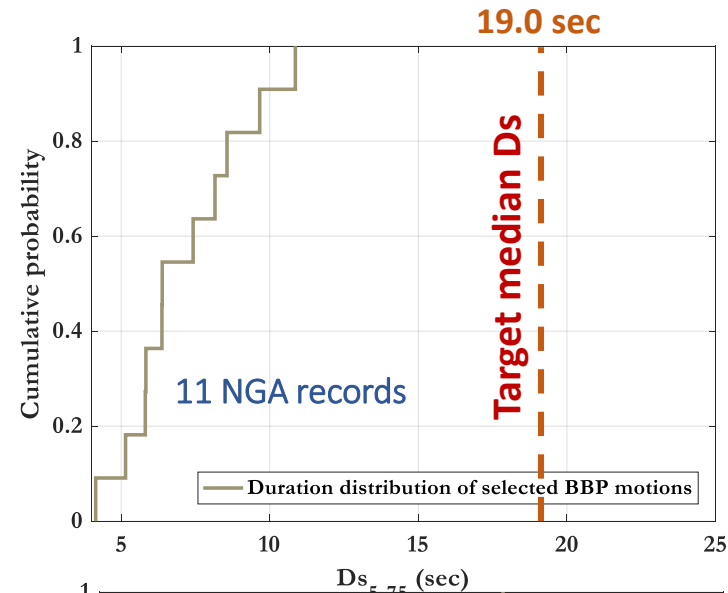
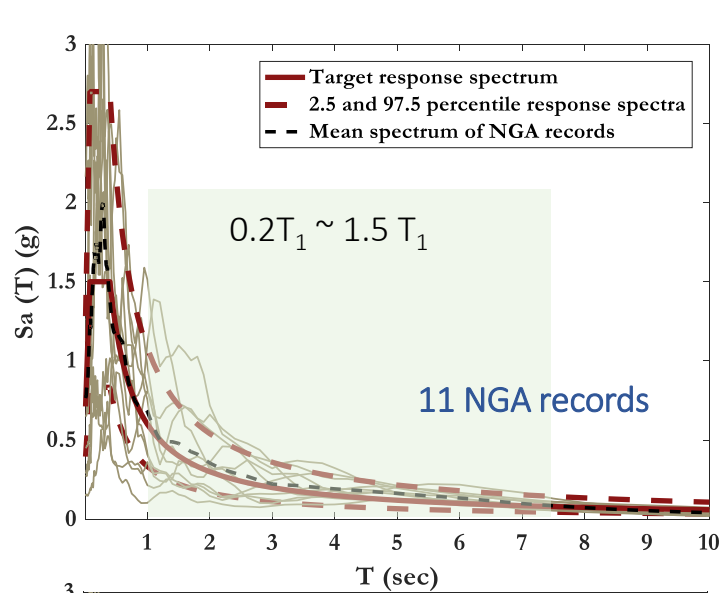
$MCE_R$  and design response spectrum from ASCE-7 (after USGS design tool)



Seismic hazard deaggregation at 2% in 50 years intensity for 8029-RIN (after USGS)



## MCEr, T = 5 sec: selected NGA vs. BBP records

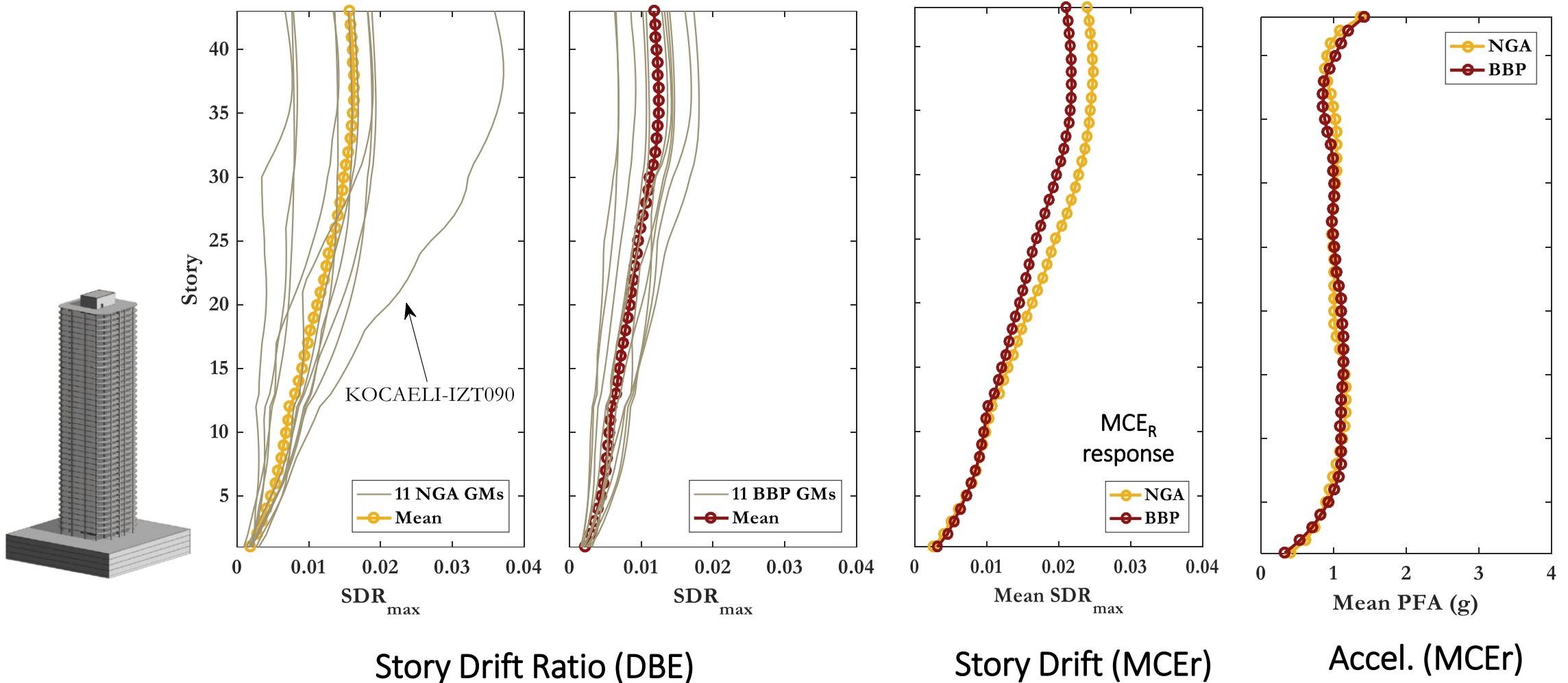


Comparison between selected 11 NGA and BBP records ( $S_a$  and duration)

Causal comparison ( $M$ ,  $R$ ,  $V_{s30}$ , and scaling)

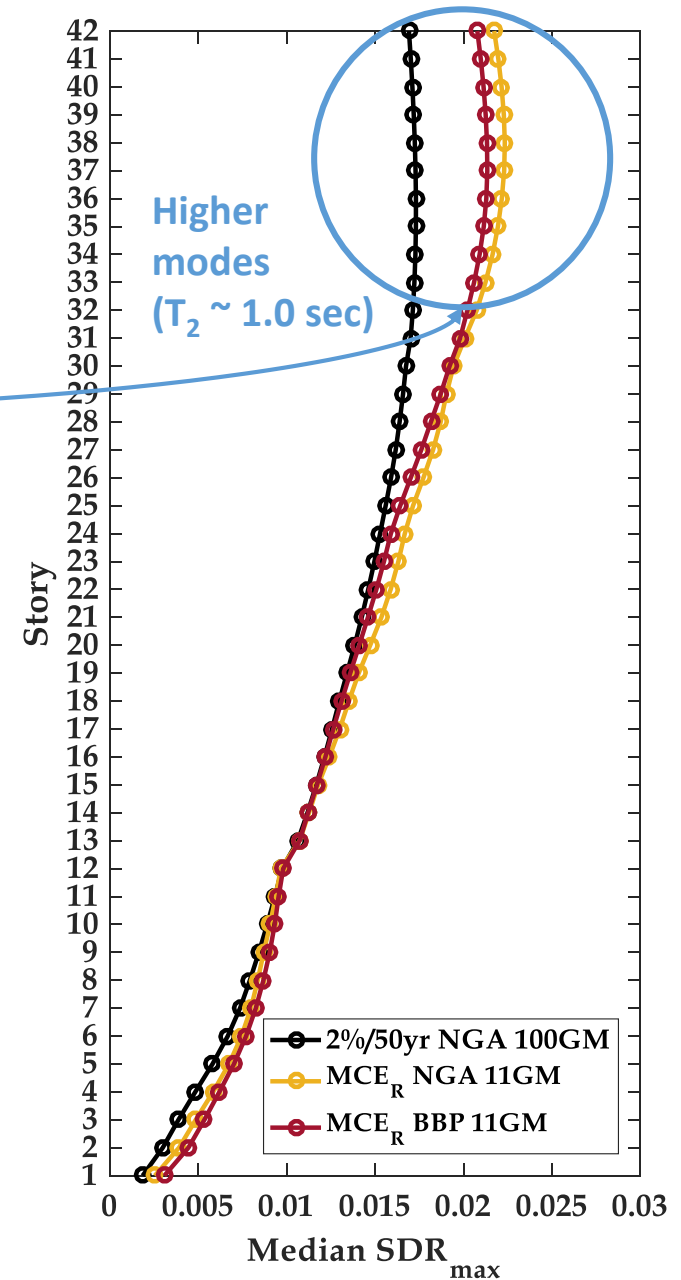
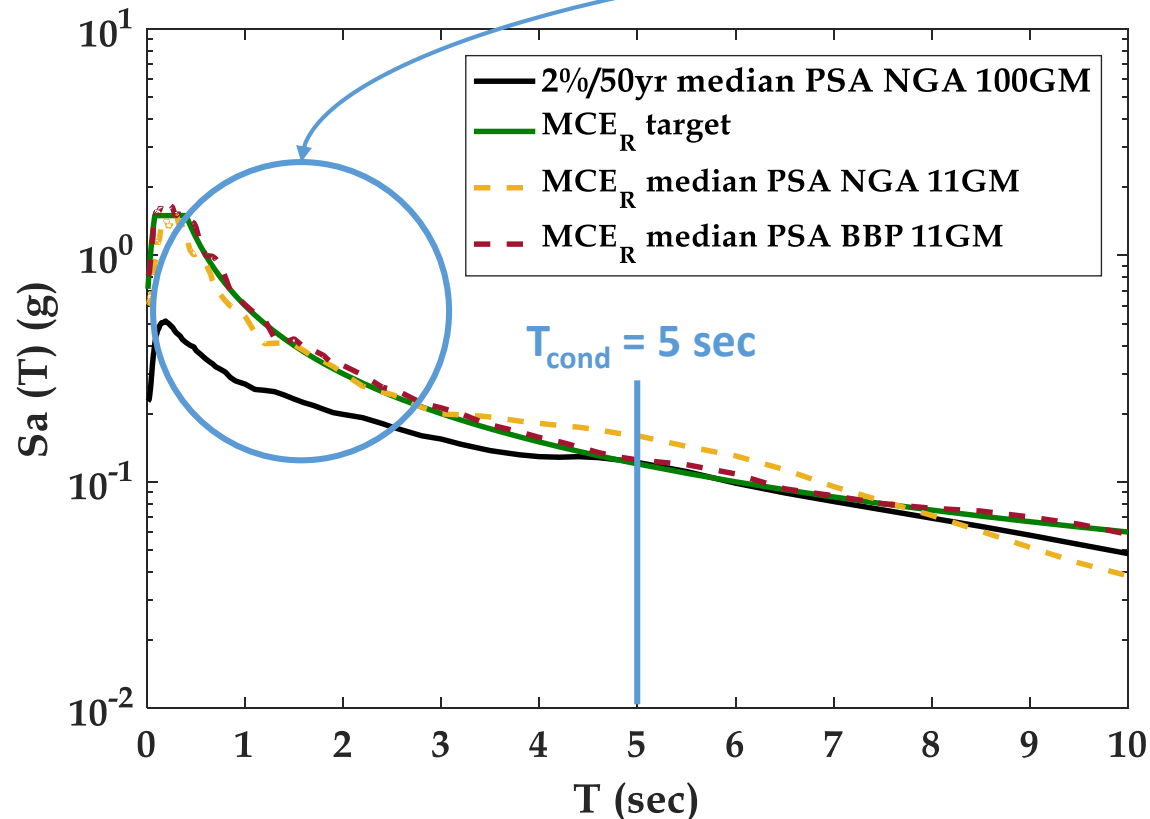
## 42-Story Shear Wall Response

- Effects from longer duration is insignificant (drift is modest)
- NGA: drifts ~10% larger
- BBP: smaller variation in response



## MCE<sub>R</sub> (UHS) vs. 2%/50yr CS Target

- Median PSA of 11 GM under MCER is generally higher than the median PSA of 100 GM under 2%/50yr, especially in the high-frequency range
- Median responses under 11 GM are slightly larger than the median responses under 100 GM



# Summary (San Francisco Site)

1. Simulated (BBP) motions can be selected/scaled to match the PSHA target IMs ( $CS+D_{s5-75}$ ) with *much smaller scaling than existing recorded motions*.
2. When ground motions are selected/scaled to comparable target IMs, there are no statistically significant differences in *calculated structural responses and collapse risks between recorded and simulated motions*.
3. Strictly following ASCE-7 guidelines (matching magnitude, mechanism and soil conditions), BBP simulations:
  - a) provide a better fit to the response spectra target (e.g.,  $MCE_R$ ) with *less dispersion and closer match to expected durations*,
  - b) can *avoid “unrealistic” spectral shapes* in selected records, thus offering more reliable response prediction from a limited number of ground motions.



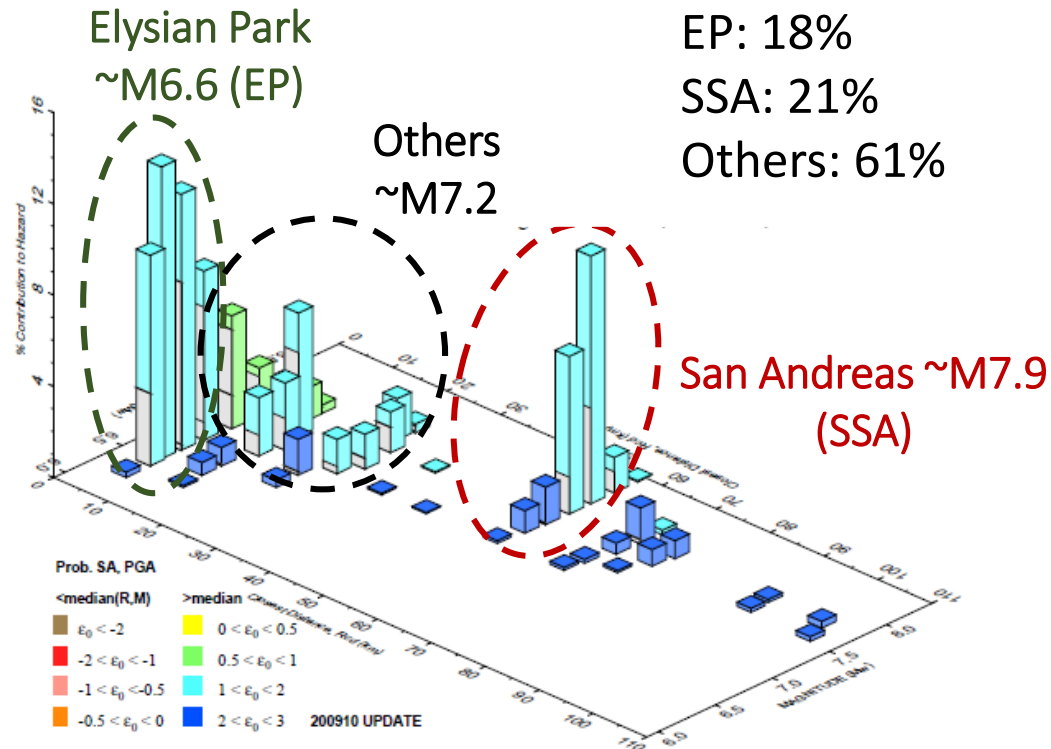
# Los Angeles Downtown (LADT)

MCEr (T=5s):

EP: 18%

SSA: 21%

Others: 61%



Major seismic sources for LADT site

## Key Focus Areas

### GM selection

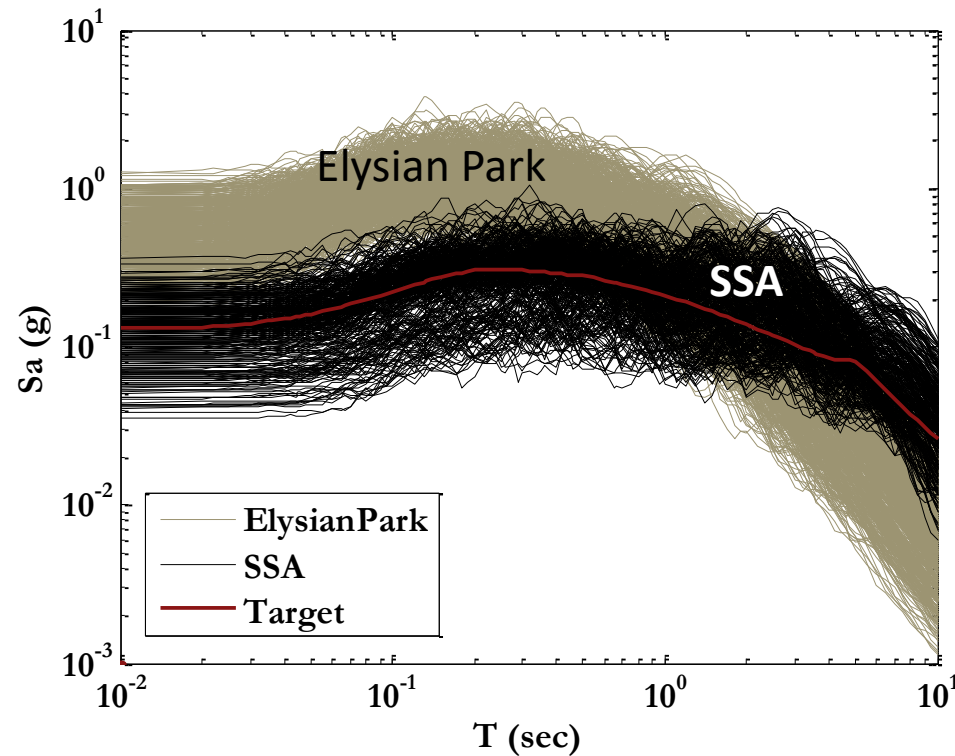
1. Multi-target IM's
2. Spectral shape of Elysian Park records

### Structural response & collapse

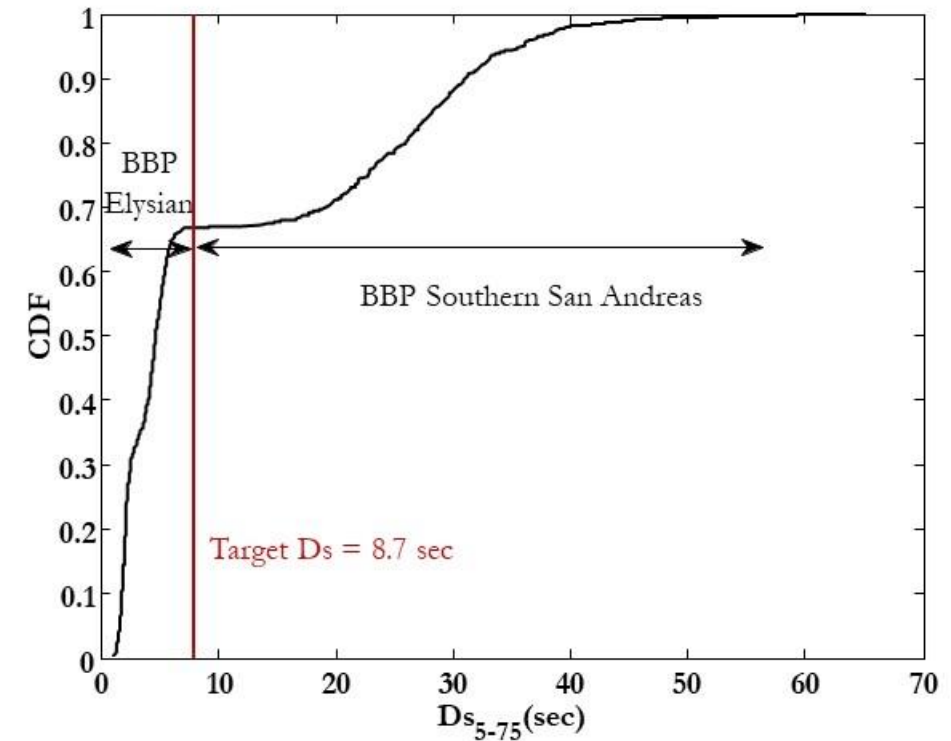
1. Investigate sensitivity to different GMPE
2. Investigate sensitivity to records with different causal parameters

## Multi-target selection (LADT)

1. Competing seismic sources: (1) South San Andreas, (2) Elysian Park, and (3) others (e.g., Puente Hills) whose **mechanisms and GM characteristics are very different**
2. Select ground motions **for each major source target** based on their relative contributions to the total hazard (dependent on  $T_1$  and return period)



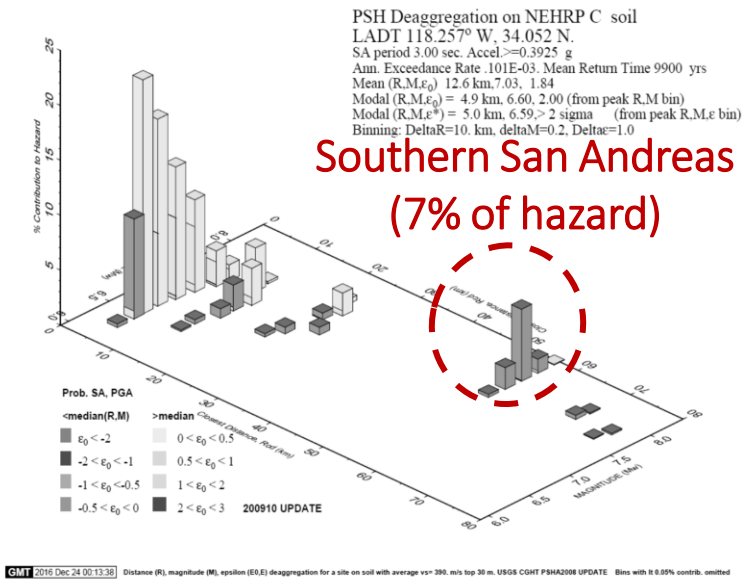
Target Spectrum vs. EP & SSA simulations  
(LADT, 10%/50yr,  $T_{\text{cond}} = 5$  sec)



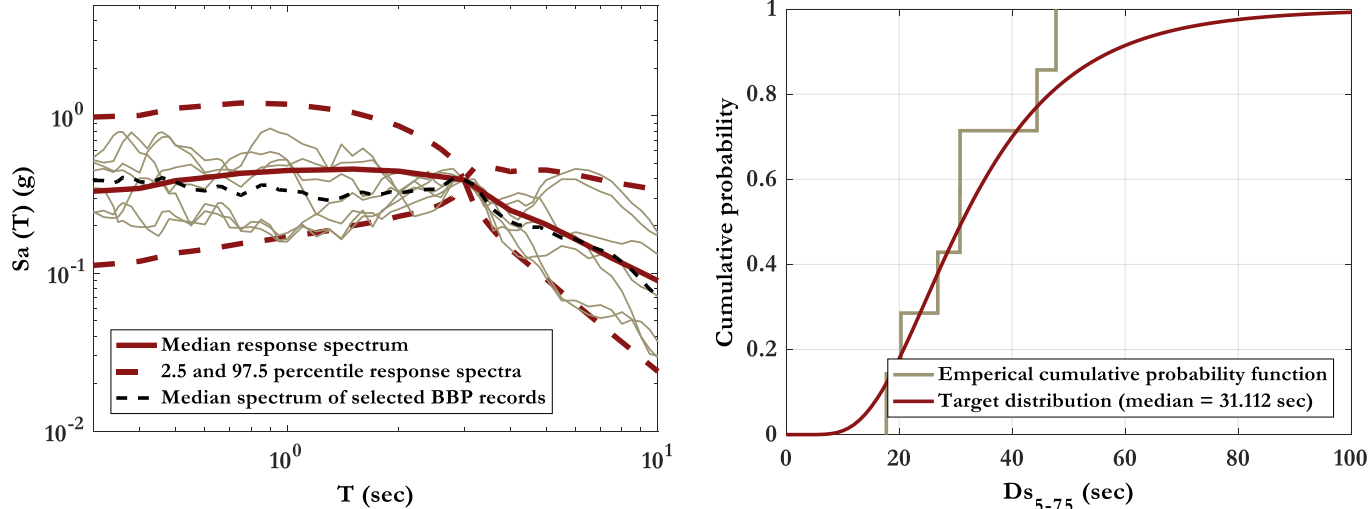
Target Duration vs. EP & SSA simulations  
(LADT, 10%/50yr,  $T_{\text{cond}} = 5$  sec)

# Southern San Andreas (T=3s, 2%/200yr)

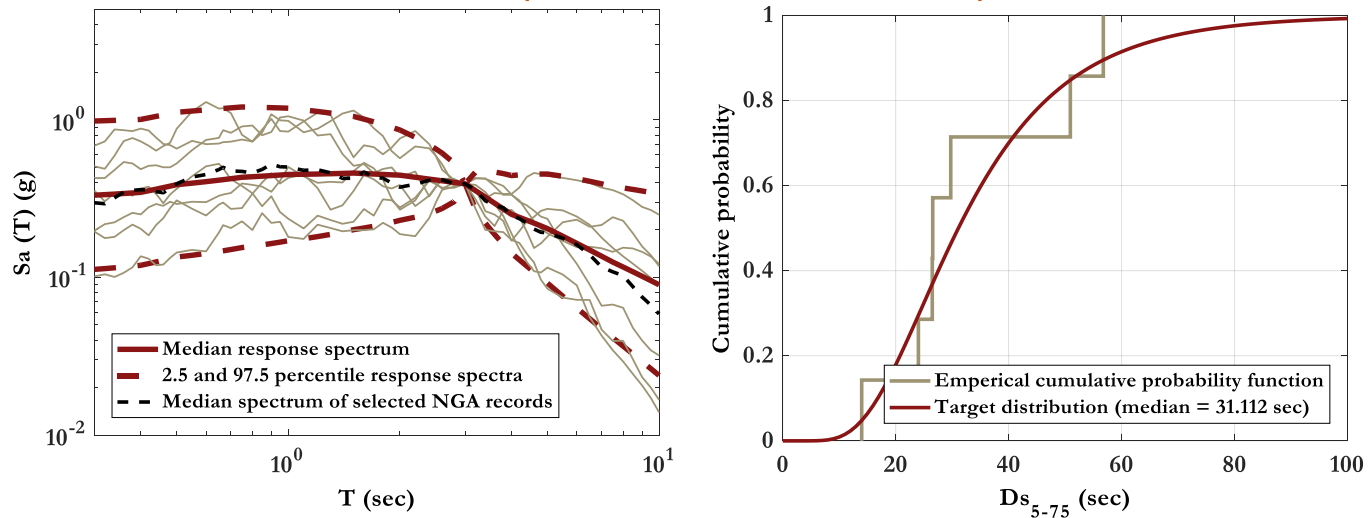
Reasonable match to the targets for both  
BBP and NGA motions at all 3 intensities.



BBP (7 GMs from 352 Southern San Andreas)



NGA (7 GMs from NGA-WEST)

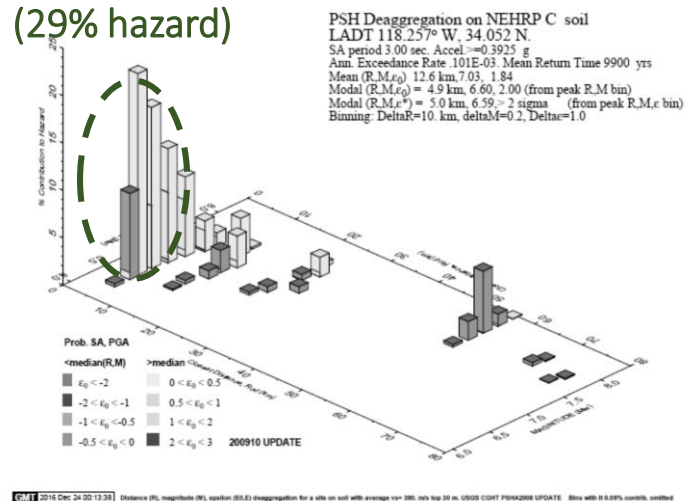


Ground motion selection (T<sub>cond</sub> = 3 s, LADT, 2% in 200 years)

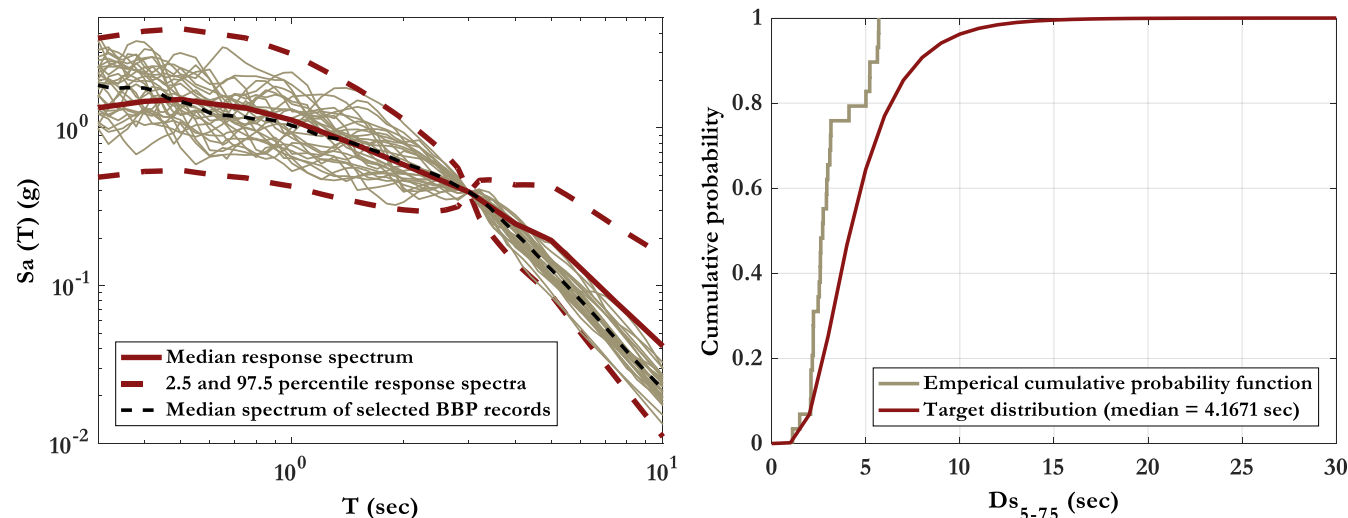
# Elysian Park (T=3s, 2%/200yr)

- Good agreement between selected records and target up to 2%/50yr level
- **Discrepancy in BBP motions for 2%/200yr hazard**

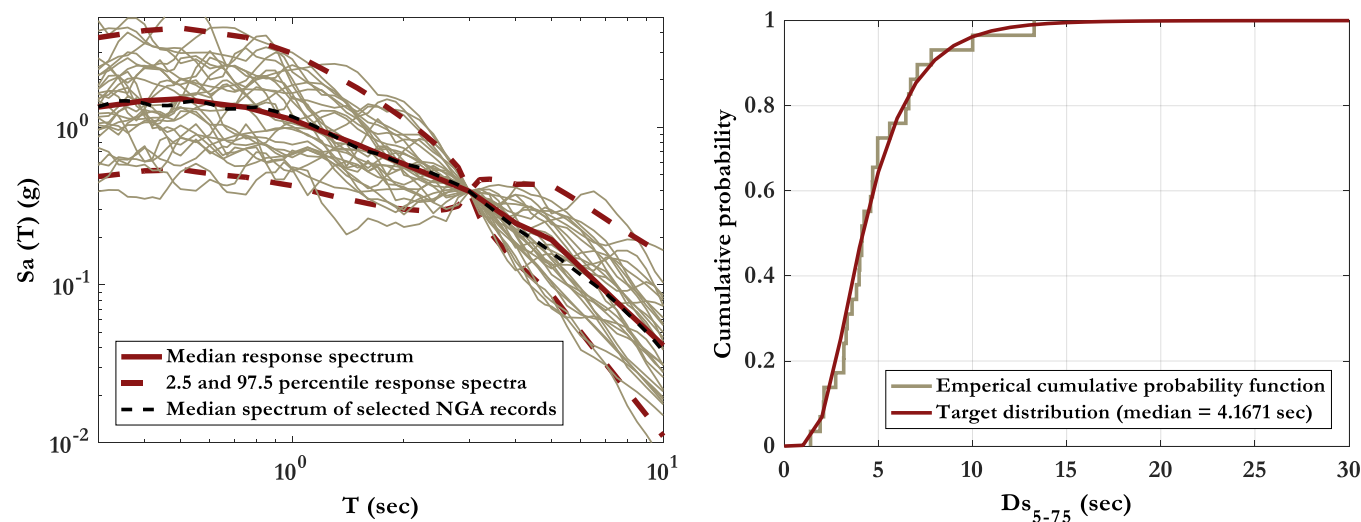
## Elysian Park (29% hazard)



## BBP (29 GMs from 704 Elysian Park)



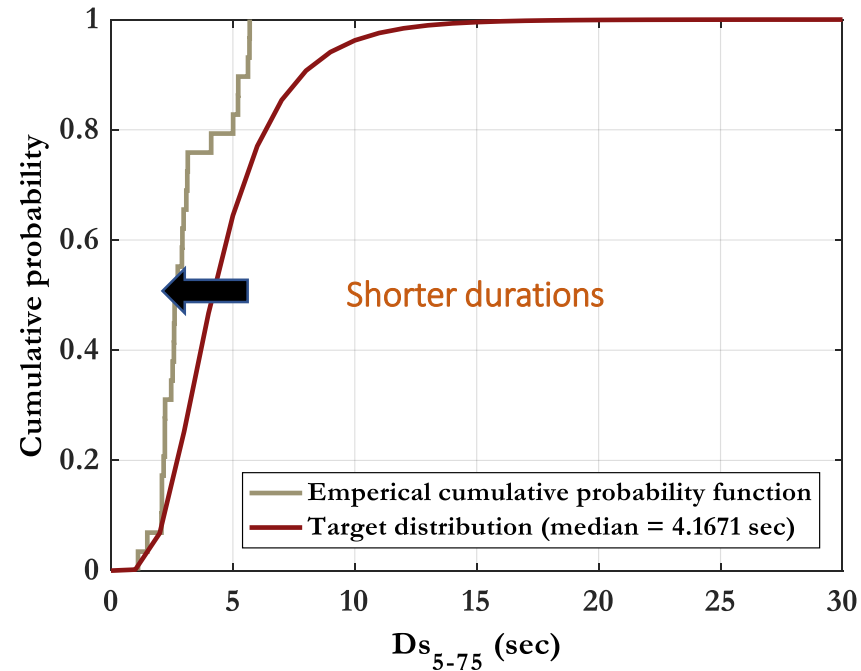
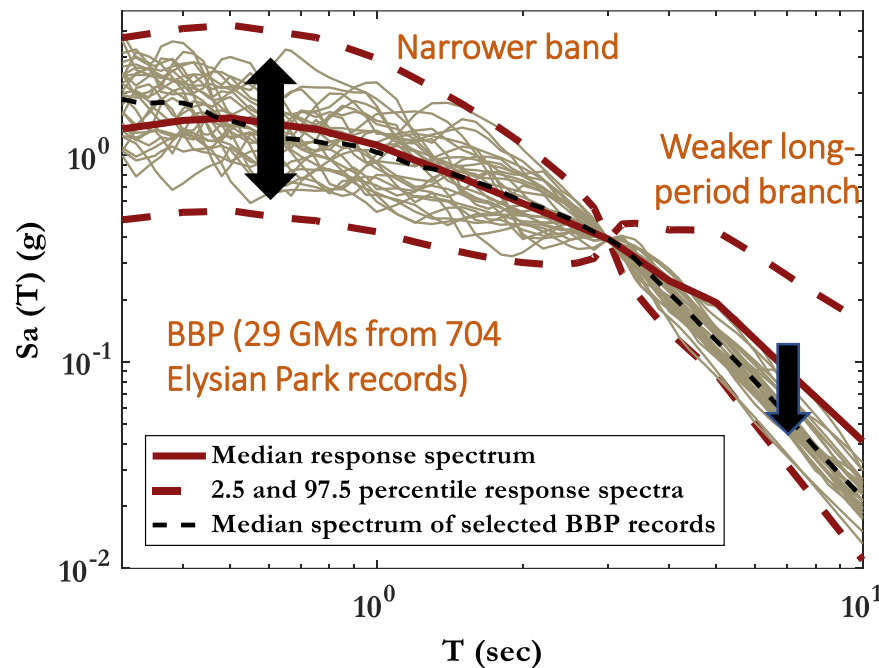
## NGA (29 GMs from NGA-WEST)



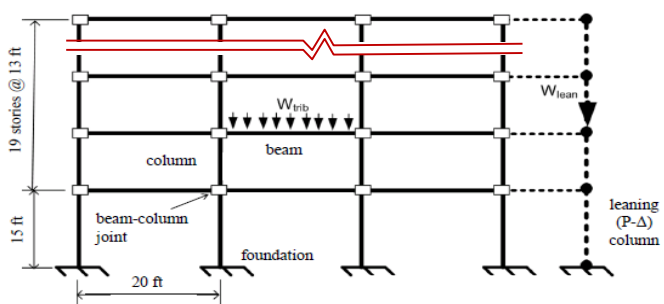
Ground motion selection ( $T_{\text{cond}} = 3 \text{ s}$ , LADT, 2% in 200 years)

## Discrepancies in selected BBP Elysian Park records at 2% in 200 yr hazard

1. *steeper descent in the long period range*
2. *less variability in the short period range*
3. *shorter durations*

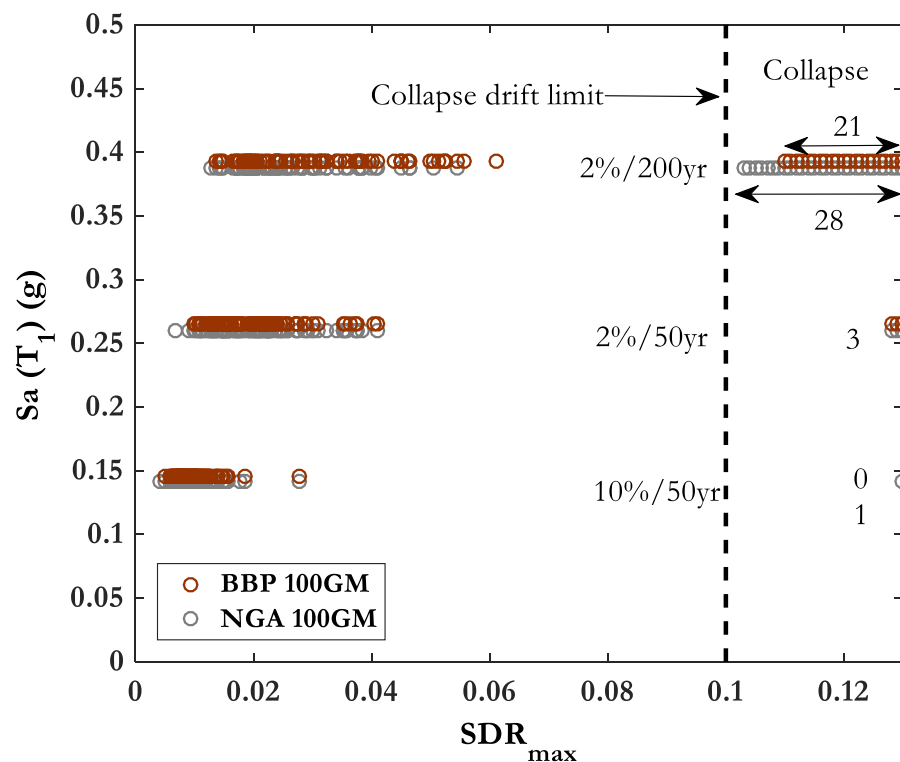


Target vs.  $S_a$  and duration distribution of selected BBP Elysian Park records  
(LADT, 2% in 200yr,  $T_{cond} = 3$  sec)

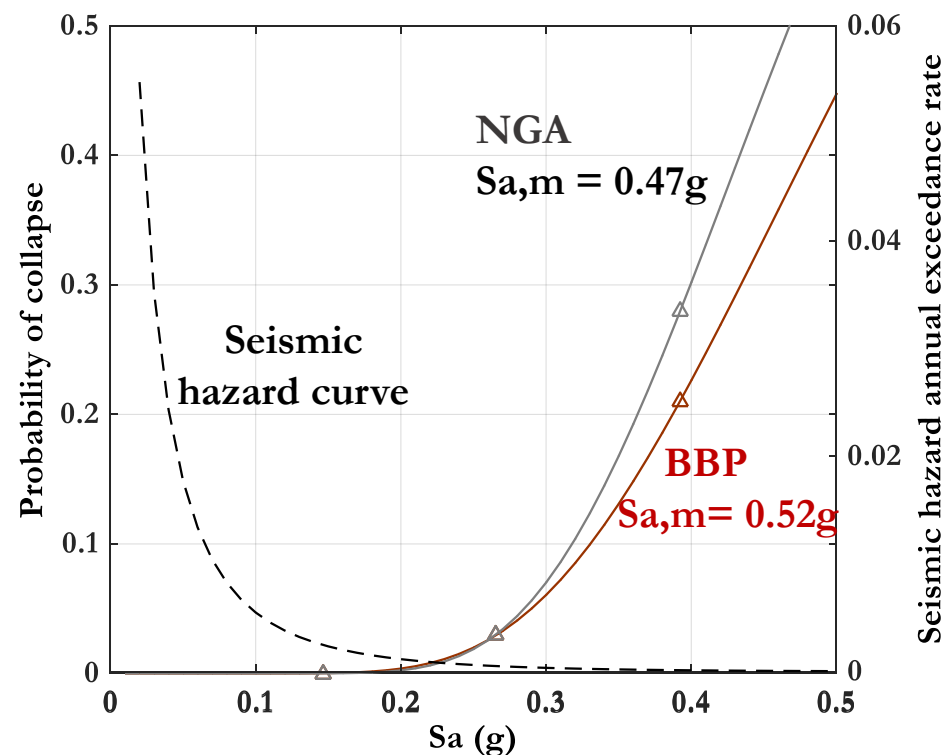


## Collapse risk: 20-story frame (LA Downtown)

- NGA and BBP motions yield same number of collapses up to 2% in 50 years hazard
- BBP has:
  - fewer collapses at 2%/200yr: **BBP 21** vs. **28 NGA**
  - about **10% lower median collapse intensity**
  - about **15% lower risk (MAF) of collapse**



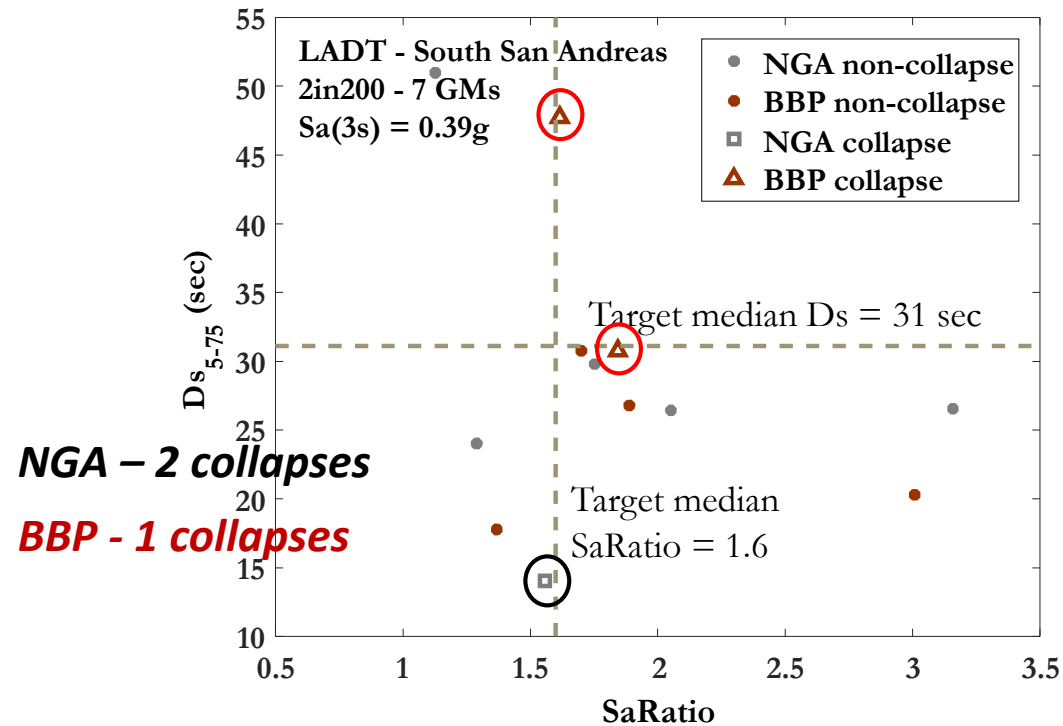
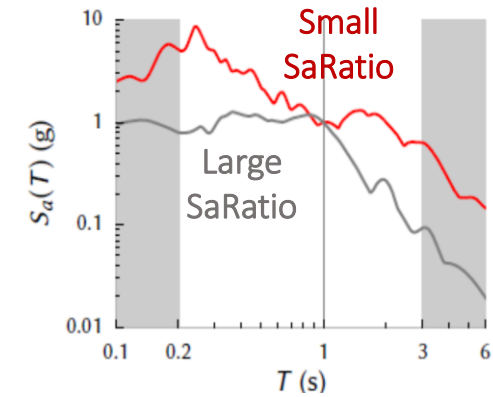
Multi-stripe Story Drift Response



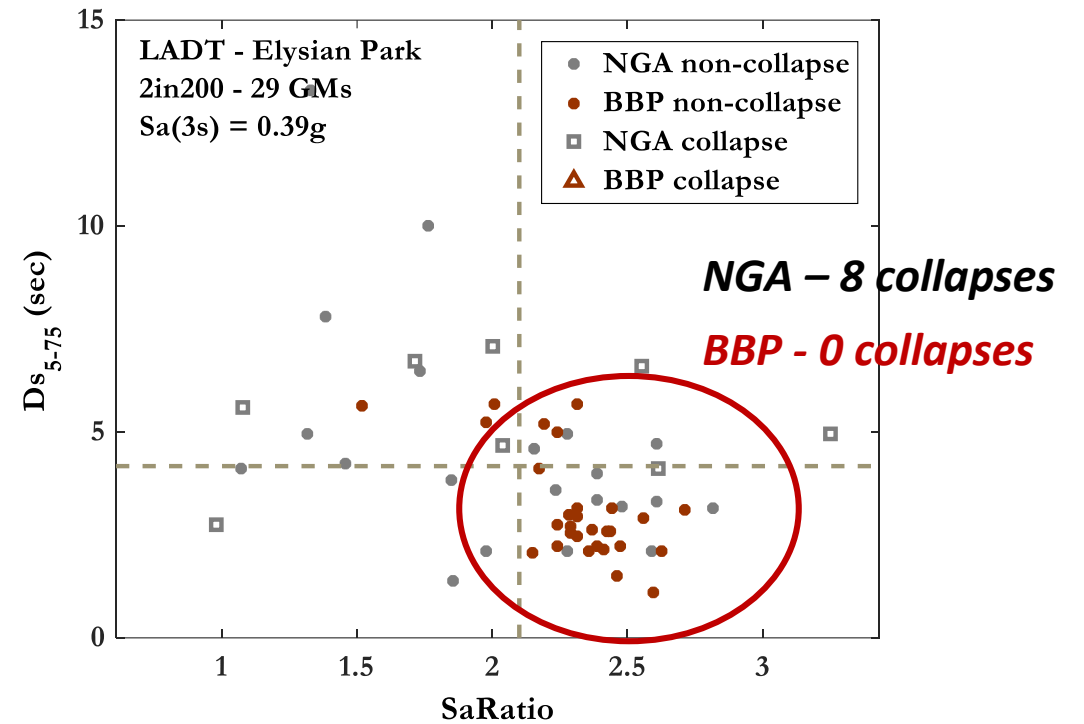
Collapse Fragility & Hazard Curves

## Collapse deaggregation: 20-story frame (LA Downtown)

- Difference at 2%/200yr is checked source by source
- Collapse & non-collapse cases plotted vs. GM Spectral Shape & Duration



**Southern San Andreas**

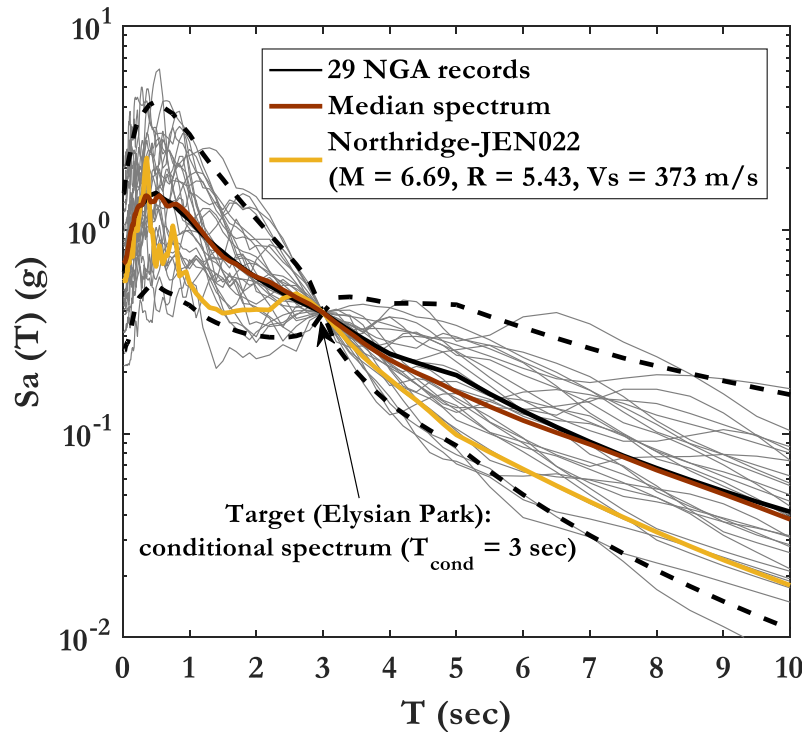


**Elysian Park**

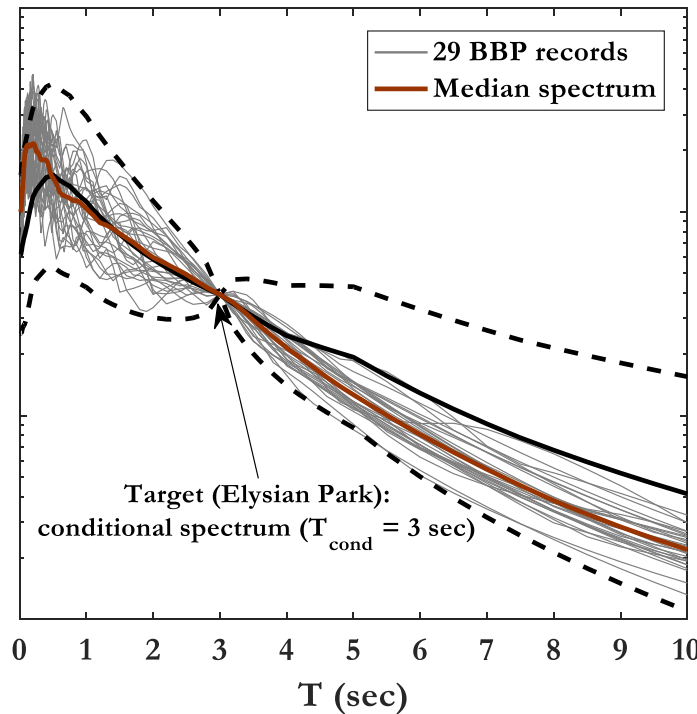


## Elysian Park: NGA & BBP records versus Northridge records

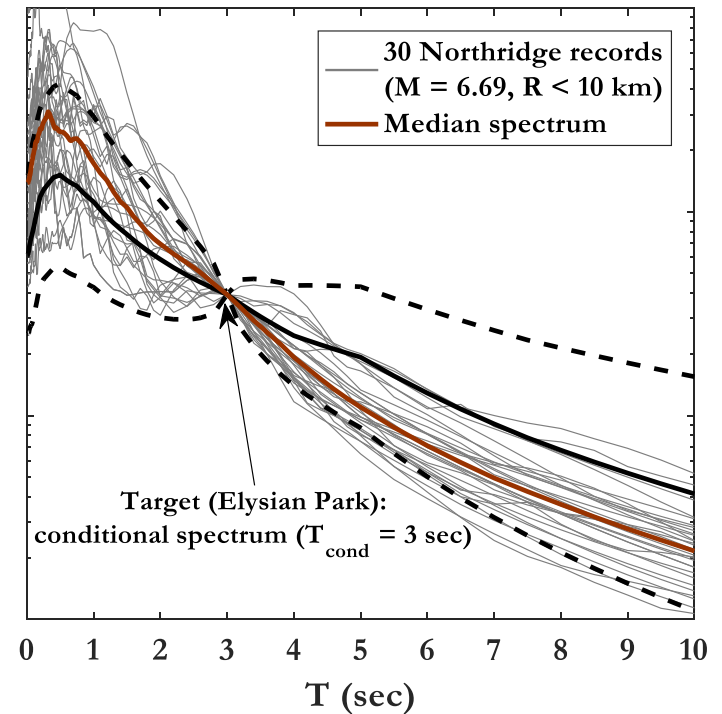
- *NGA best match: median matches the target spectrum, but the only one Northridge differs*
- *BBP records: the long-period branch of median spectrum has steeper descent than the target*
- *Northridge records (w/ M & R): have similar trend with BBP simulation's but more high-frequency content*



**NGA match to GMPE target**



**BBP Elysian Park “match” to GMPE**



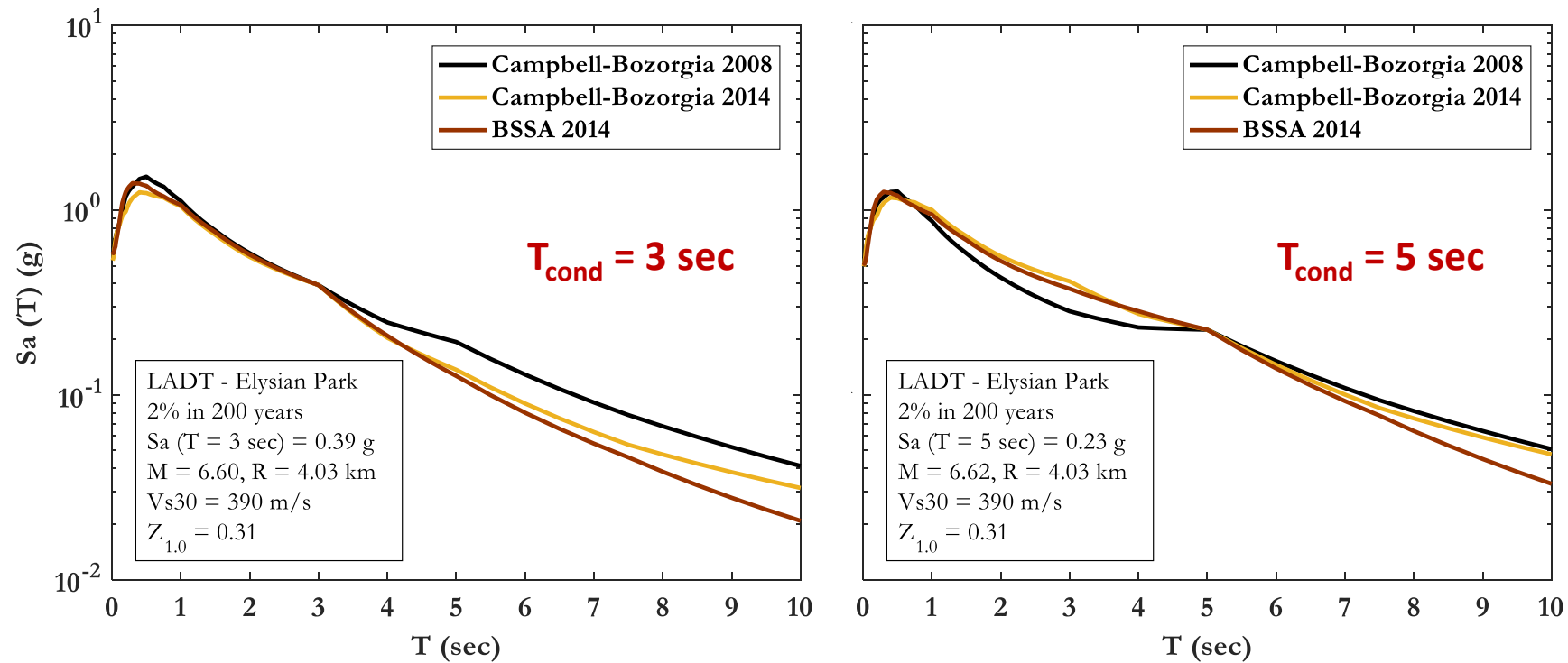
**NGA Northridge records**

Selected records vs. target spectrum (2%/200yr, CB2008).  
Seismic hazard deaggregation:  $S_a = 0.3925$  g,  $R = 4.03$  km,  $M = 6.60$ , contribution = 29.33%.  
Target: CS (GMPE: Campbell-Bozorgnia 2008), Duration (Afshari and Stewart 2016).



## Elysian Park: difference in GMPEs?

Seismic hazard deaggregation (for Elysian Park):  $M = 6.6$ ,  $R = 4.0$  km,  $S_a = 0.39$  g



## Conditional Mean Spectra by three GMPEs

# Reselect records by 4 schemes to BSSA 2014 target

## NGA records

- $M$ : 6~8,  $R$ : 0~175 km
- $V_{s30}$ : 198~629 m/s
- 14 reverse-fault records  
(2 Northridge records)
- *Maximum scaling: 29*

## NGA (causal limits)

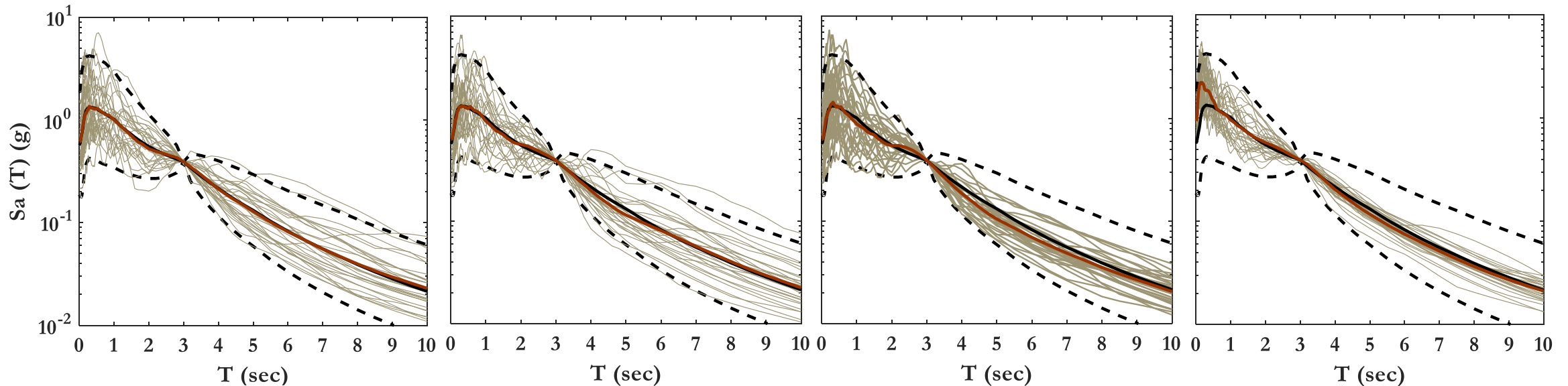
- $M$ : 6~7,  $R$ : 0 ~ 10 km
- $V_{s30}$ : 195 ~ 585 m/s
- 29 reverse-fault records  
(11 Northridge records)
- *Maximum scaling: 23*

## NGA (causal & scaling limits)

- $M$ : 6~7,  $R$ : 0 ~ 10 km
- $V_{s30}$ : 195 ~ 585 m/s
- 29 reverse-fault records  
(17 Northridge records)
- *Maximum scaling: 5*

## BBP records

- $M = 6.60$ ,  $R \sim 4.03$  km
- $V_{s30} \sim 390$  m/s
- *Maximum scaling: 5*



Comparison of selected records ( $T_{\text{cond}} = 3$  sec) by **BSSA-2014** for **Elysian Park (2%/200yr)**.

## 20-story frame collapse by reselect records by 4 record suites

### NGA records

- $M$ : 6~8,  $R$ : 0~175 km
- $V_{s30}$ : 198~629 m/s
- 14 reverse-fault records (2 Northridge records)
- *Maximum scaling: 29*

### NGA (causal limits)

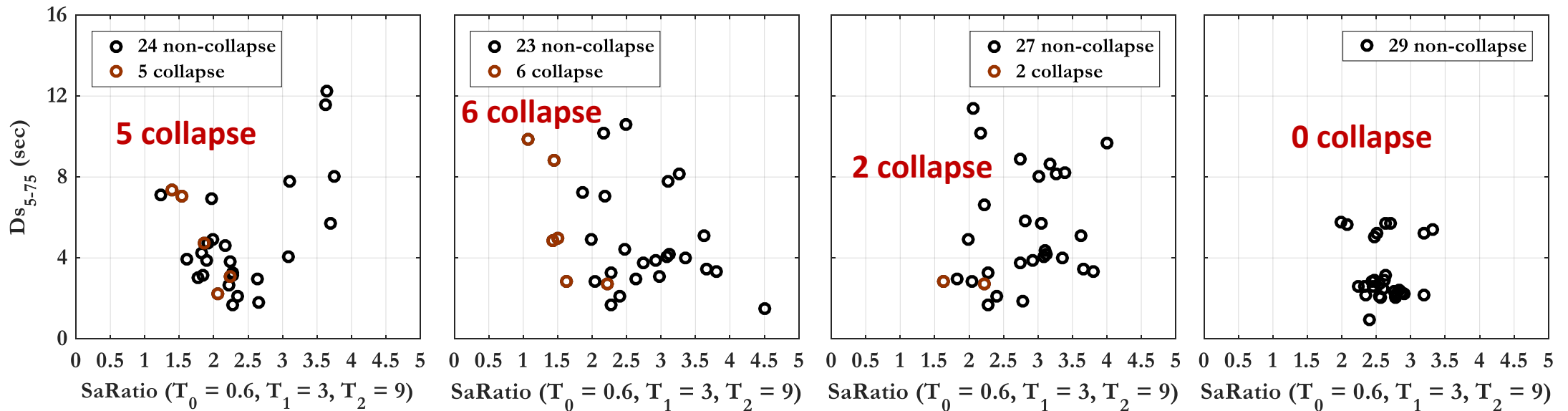
- $M$ : 6~7,  $R$ : 0 ~ 10 km
- $V_{s30}$ : 195 ~ 585 m/s
- 29 reverse-fault records (11 Northridge records)
- *Maximum scaling: 23*

### NGA (causal & scaling limits)

- $M$ : 6~7,  $R$ : 0 ~ 10 km
- $V_{s30}$ : 195 ~ 585 m/s
- 29 reverse-fault records (17 Northridge records)
- *Maximum scaling: 5*

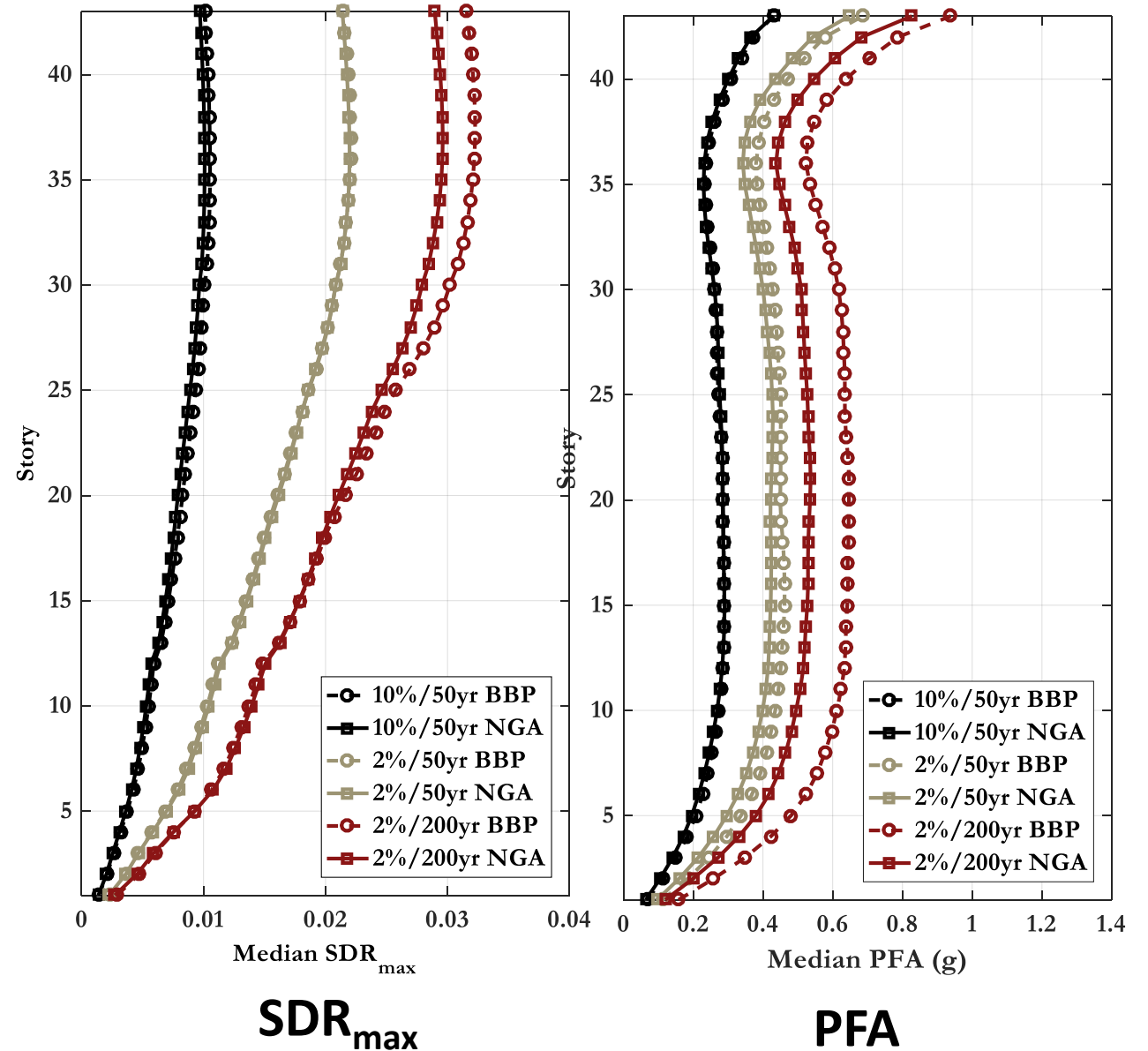
### BBP records

- $M = 6.60$ ,  $R \sim 4.03$  km
- $V_{s30} \sim 390$  m/s
- *Maximum scaling: 5*



## 42-story shear wall building (LADT)

- No statistical difference up to 2% in 50 yr
- ~10% difference under 2% in 200 yr

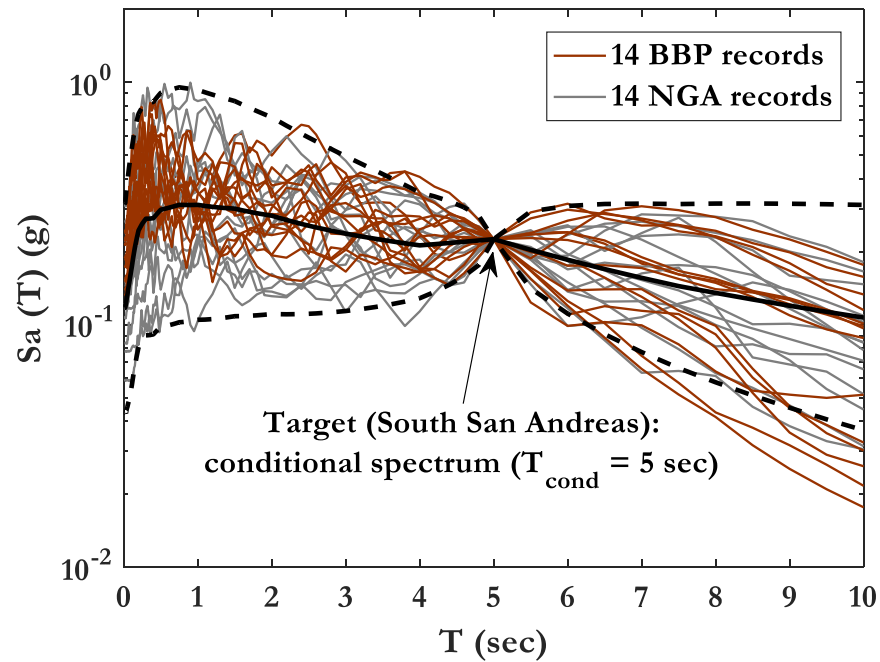


Median structural response demands

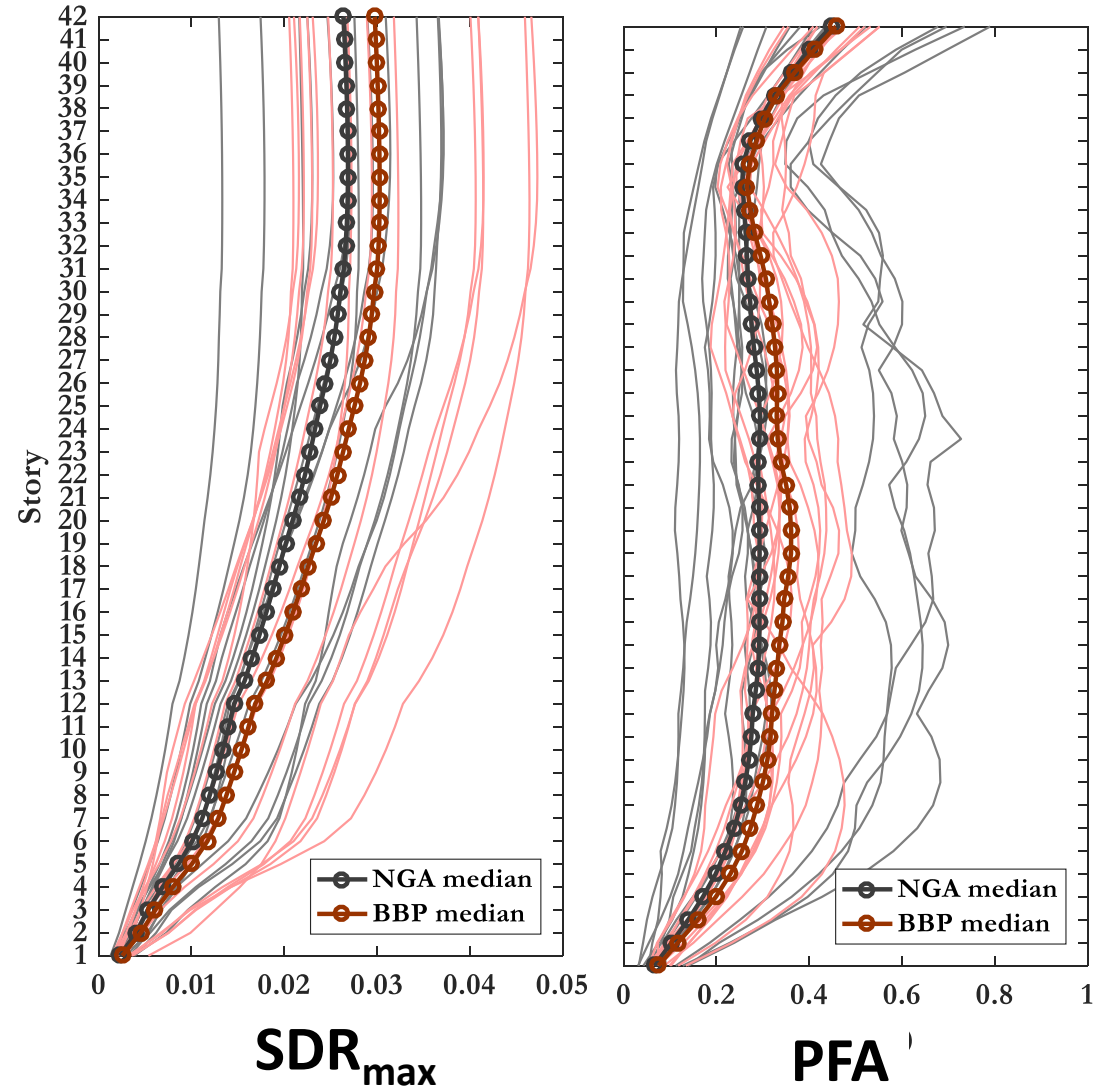
# 42-story shear wall building (LADT)

## San Andreas responses: BBP vs. NGA

- *No difference in estimated median responses*
- *Less dispersion in BBP results*



2%/200yr hazard-level South San Andreas motions (14% of LADT seismic hazard)

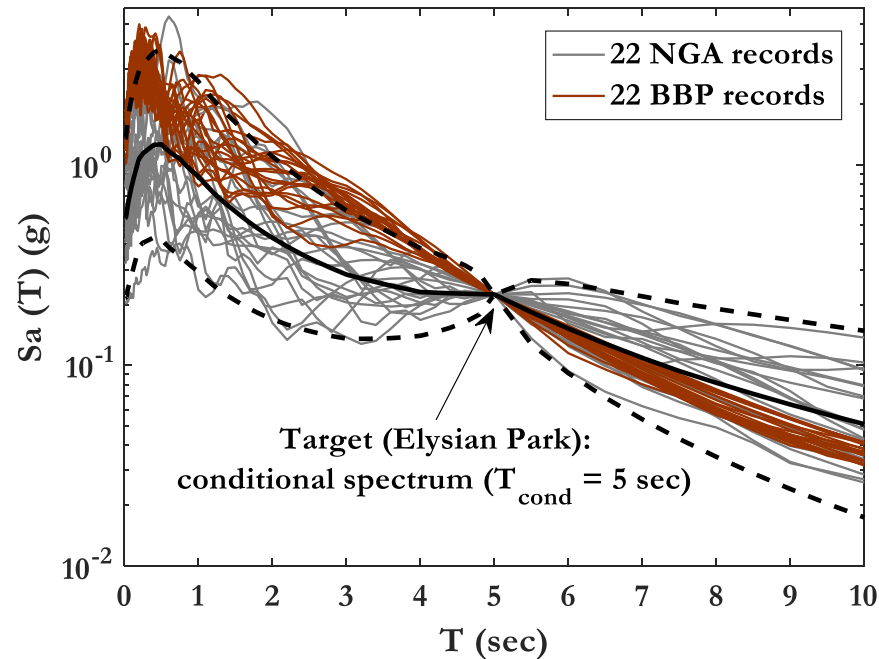


Structural responses under 14 NGA and BBP records

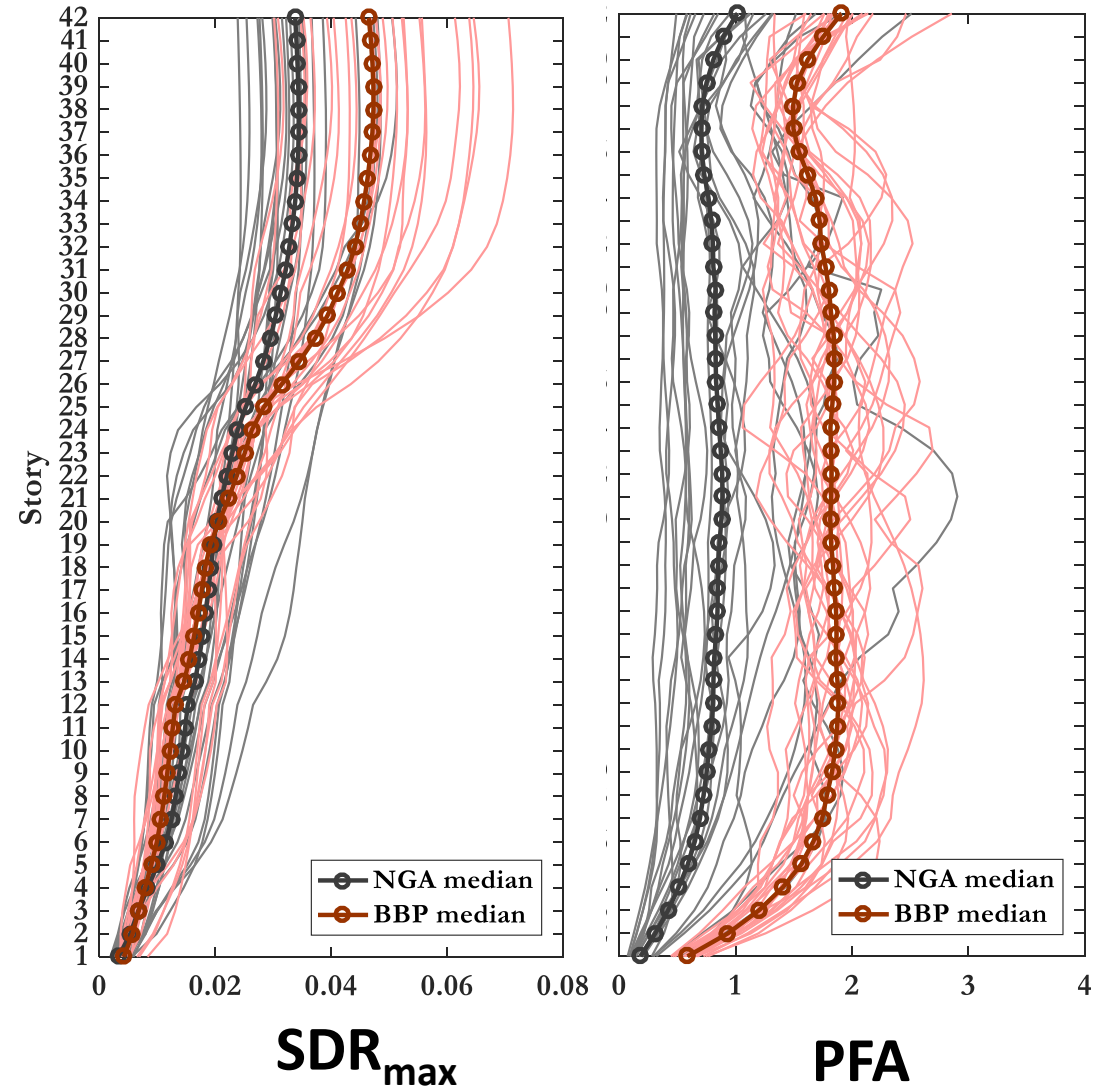
# 42-story shear wall building (LADT)

## Elysian Park responses: BBP vs. NGA

- *BBP records -- higher structural demands*
- *Higher-mode story drifts*
- *Higher-frequency  $S_a$ 's and PFA*



2%/200yr hazard-level Elysian Park motions  
(22% of LADT seismic hazard)



Structural responses - 22 NGA and BBP records

## Summary (LADT Site)

### At 10%/50yr & 2%/50yr level (similar to SF downtown):

1. Simulated (BBP) motions can be selected/scaled to match the PSHA target IMs ( $CS+D_{s5-75}$ ) with *much smaller scaling than existing recorded motions*.
2. When ground motions are selected/scaled to comparable target IMs, there are no statistically significant differences in *calculated structural responses and collapse risks between recorded and simulated motions*.

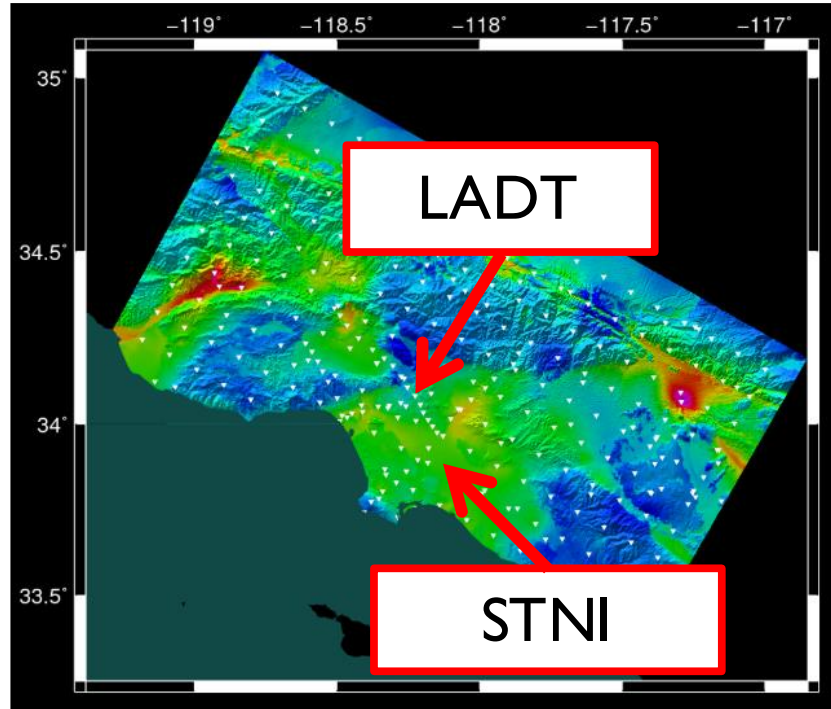
### At 2%/200yr level:

1. *Limitations in our knowledge about rare earthquakes*
2. *The 4 paralleling case studies for Elysian Park scenario indicates that increasing causal and scaling constraints on NGA leads to:*
  - *more difficulty matching GM's to target spectra*
  - *selected records tend to be more "local"*
  - *structural responses tend to converge toward BBP record response*
3. *Importance of high-frequency content for tall buildings: higher-mode drifts, PFA*



# Engineering Utilization of Cybershake (3D) Motions

## Conventional (PSHA w/recorded GMs) vs. CyberShake



### Deep Basin Site

**LADT:**  $V_{s30} = 390 \text{ m/s}$ ;  $Z_{1.0} = 0.3 \text{ km}$

**STNI:**  $V_{s30} = 280 \text{ m/s}$ ;  $Z_{1.0} = 0.9 \text{ km}$

### 3D Simulations

- Velocity Profile (SCEC CVM-S 4.26)
- Wave Propagation

### Physics Based & Stochastic (BB)

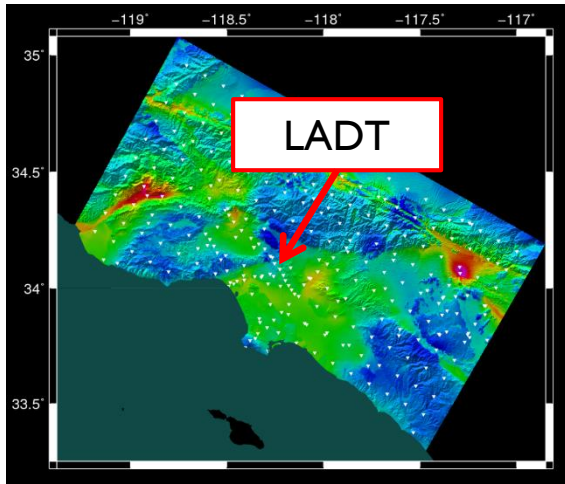
- Physics Based  $T > 1 \text{ second}$
- Splicing period  $\sim 1 \text{ second}$

### PSHA Approach

- Multiple ruptures following UCERF 2
- Faults within 200 km

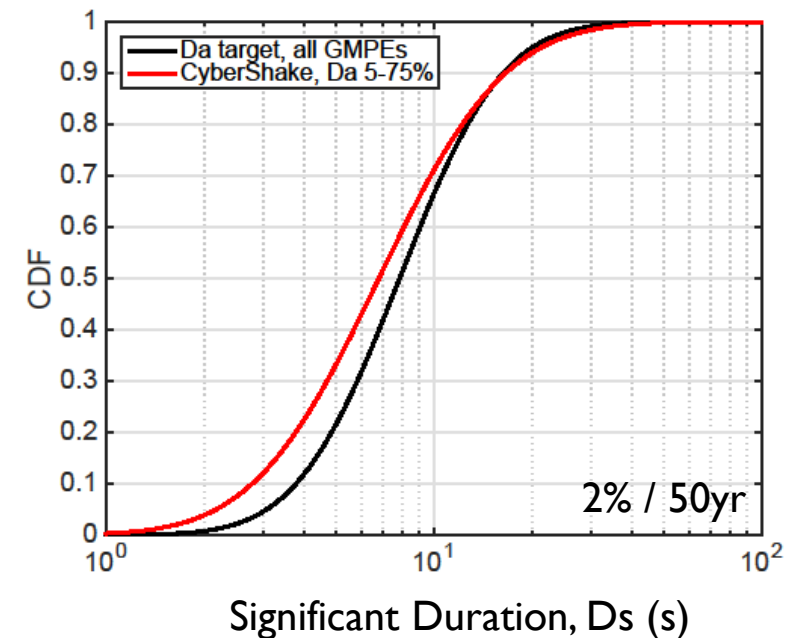
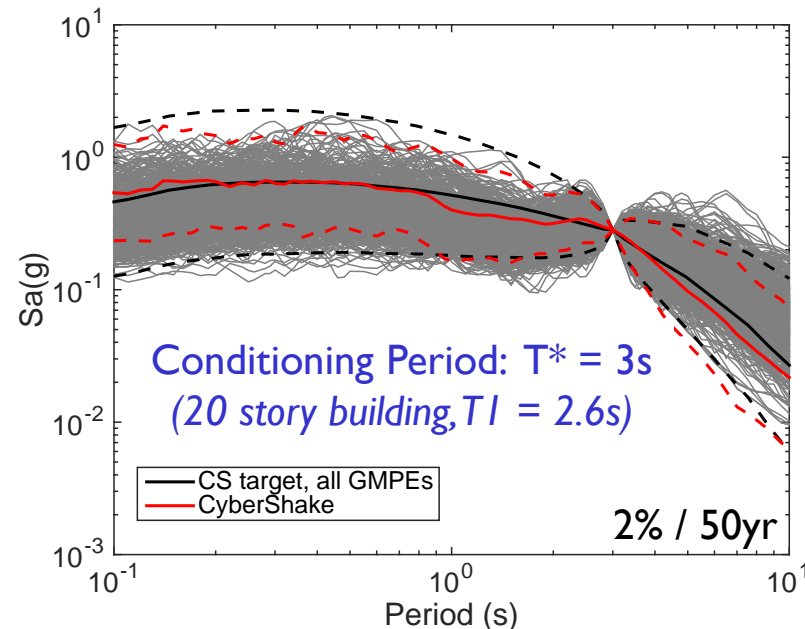
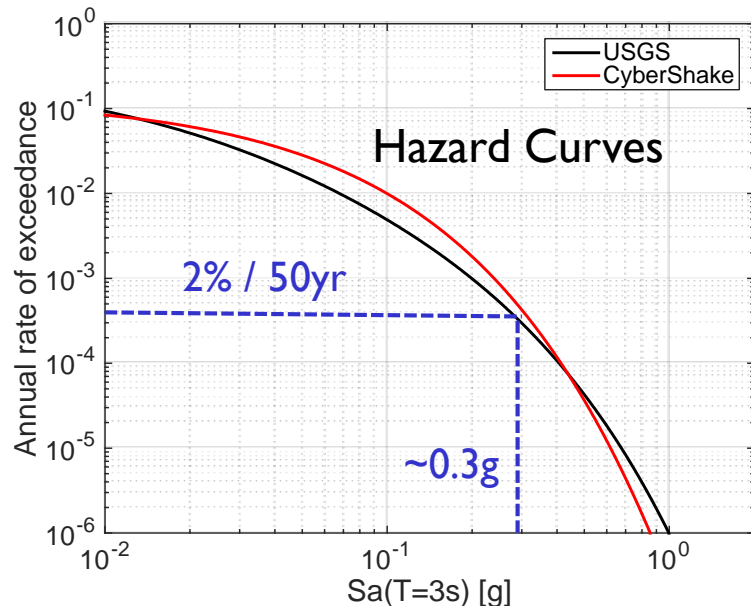


# Direct Simulation with CyberShake

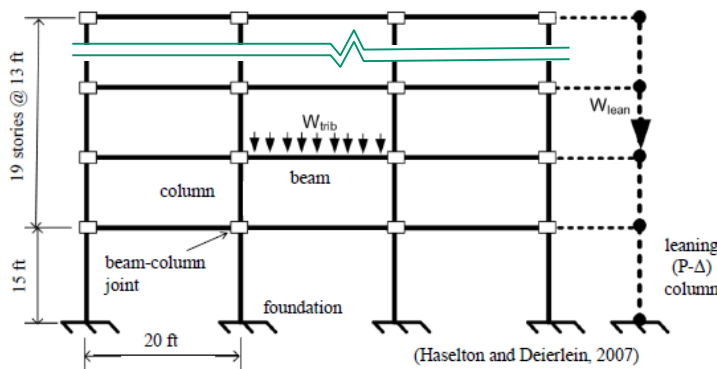
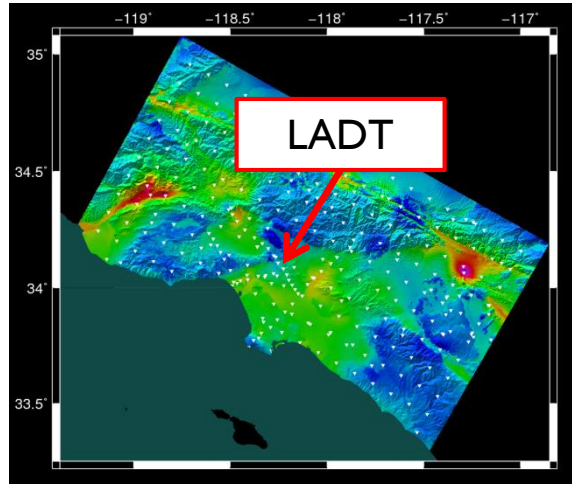


## Comparison – CyberShake and Conventional PSHA

- hazard curve ( $S_a$  for  $T = 3s$ )
- ground motion CS ( $S_a$ ,  $T^* = 3s$ , multiple return periods)
- ground motion  $D_s$  (multiple return periods)



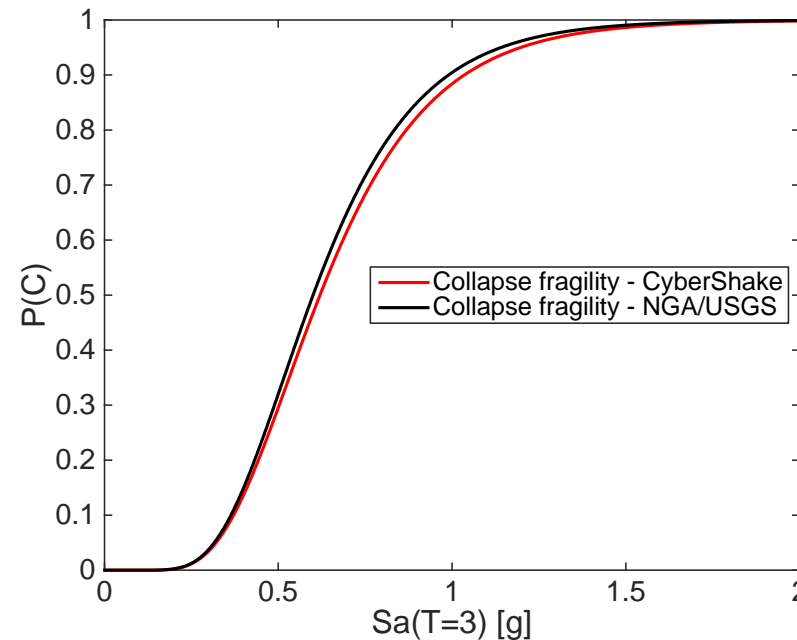
# Direct Simulation with CyberShake



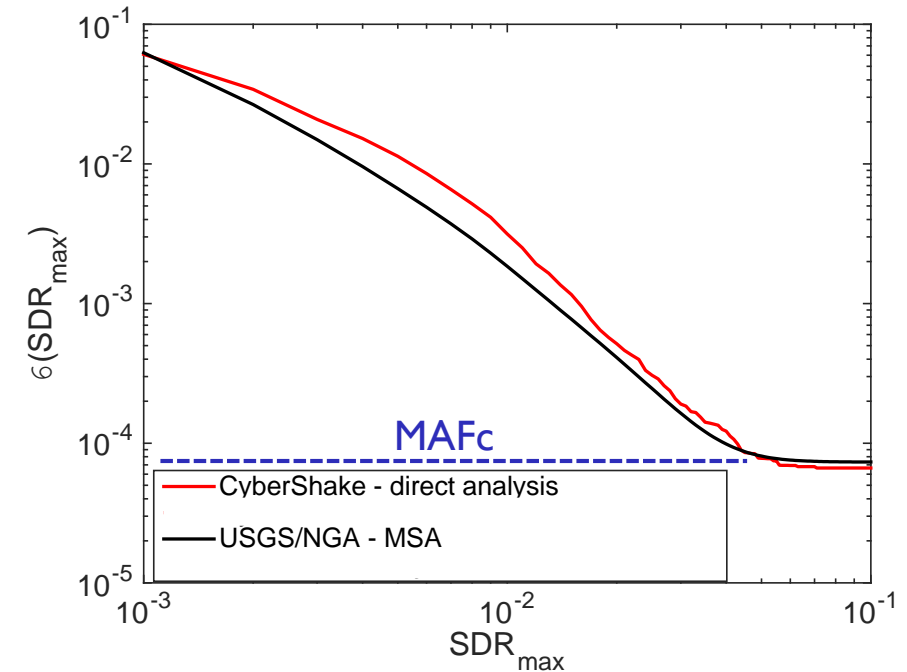
20-story building,  $T_1 = 2.60s$

## Structural Response Comparisons

- Collapse – conditioned on  $S_a(T^*)$
- Story Drift – mean annual frequency of exceedence

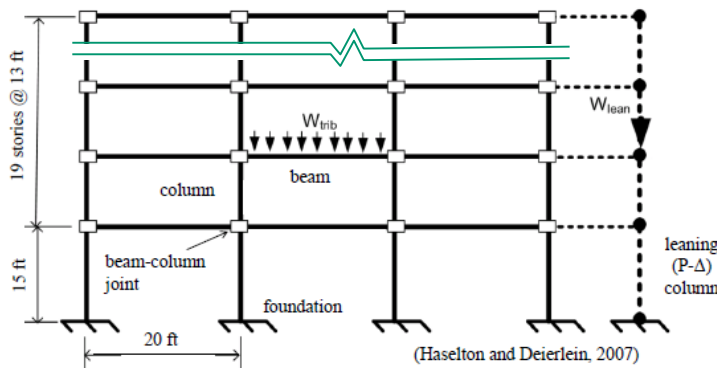
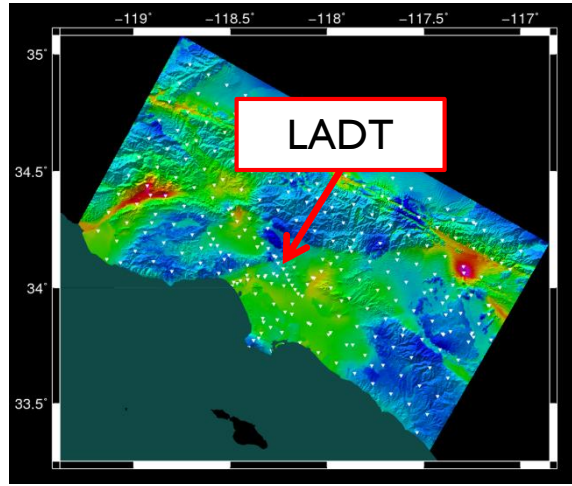


Collapse Fragility



Story Drift Exceedence

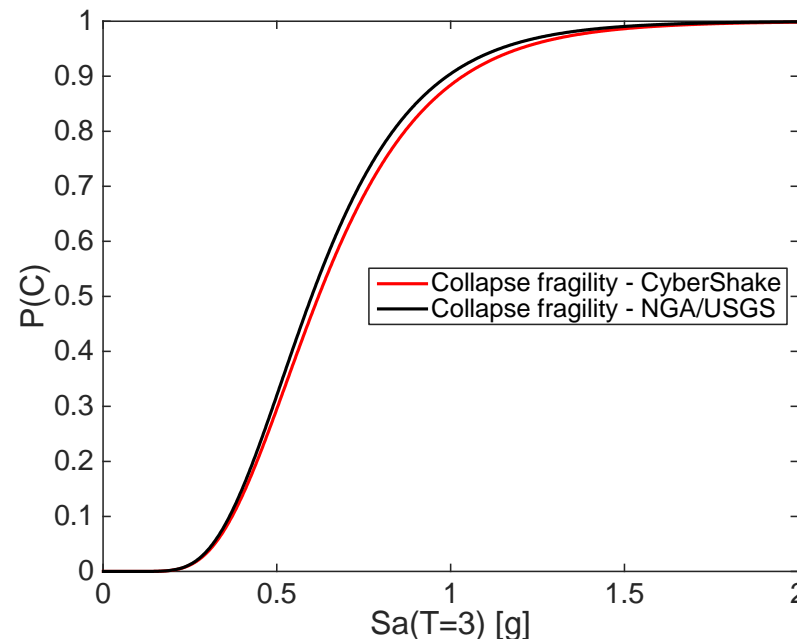
# Direct Simulation with CyberShake



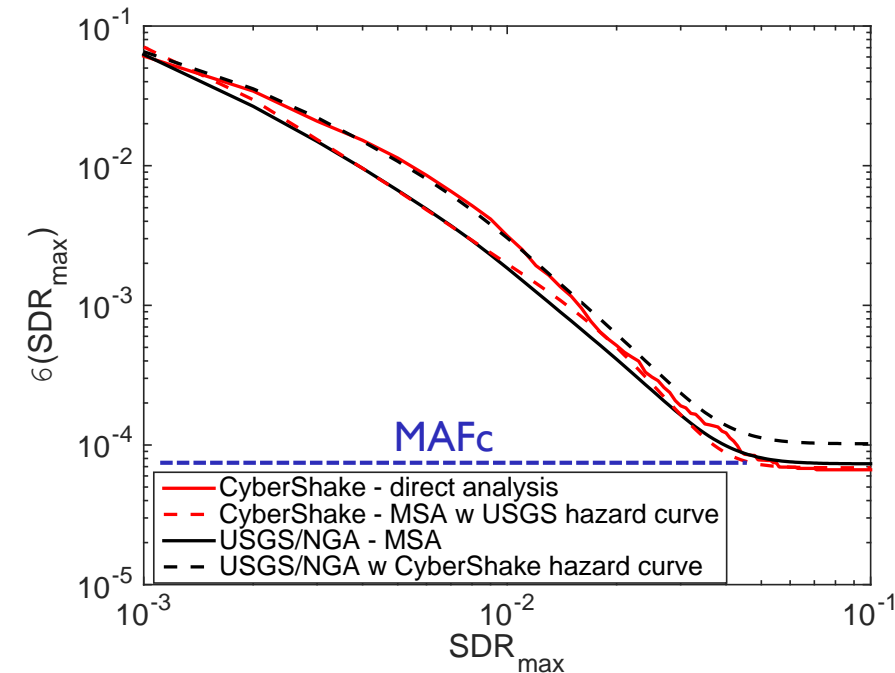
20-story building,  $T_1 = 2.60s$

**Mix and Match:** ground motions with hazard curves

**Observation:** difference in drift exceedence is attributed primarily to differences in hazard curve

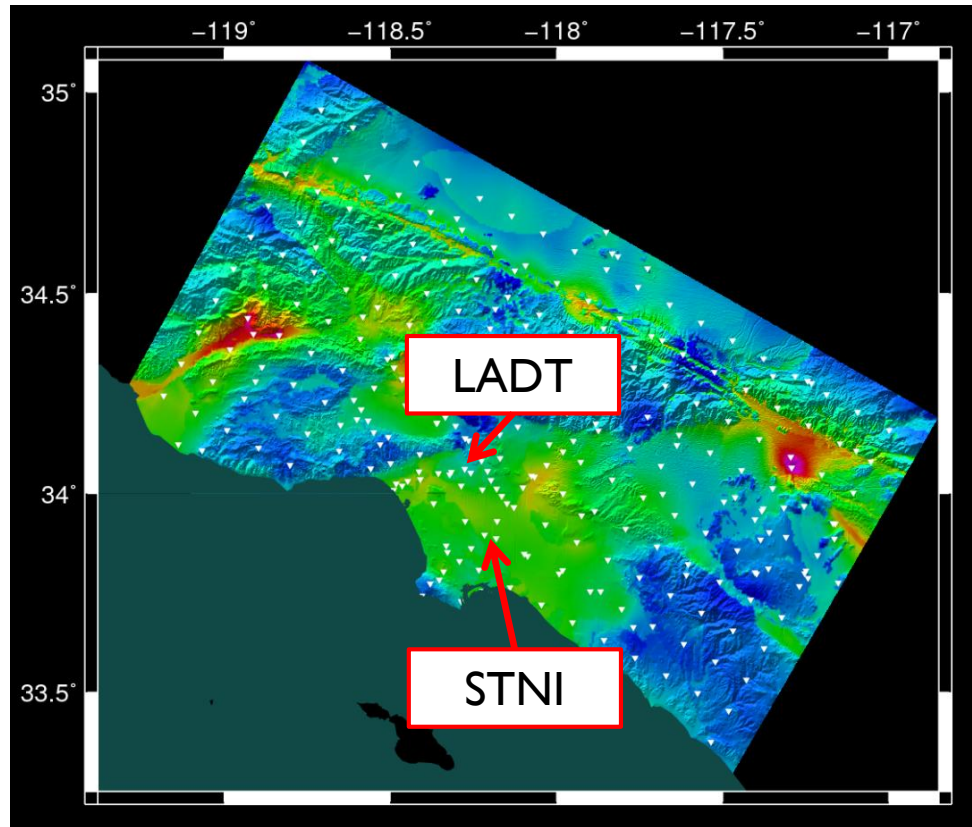


Collapse Fragility



Story Drift Exceedence

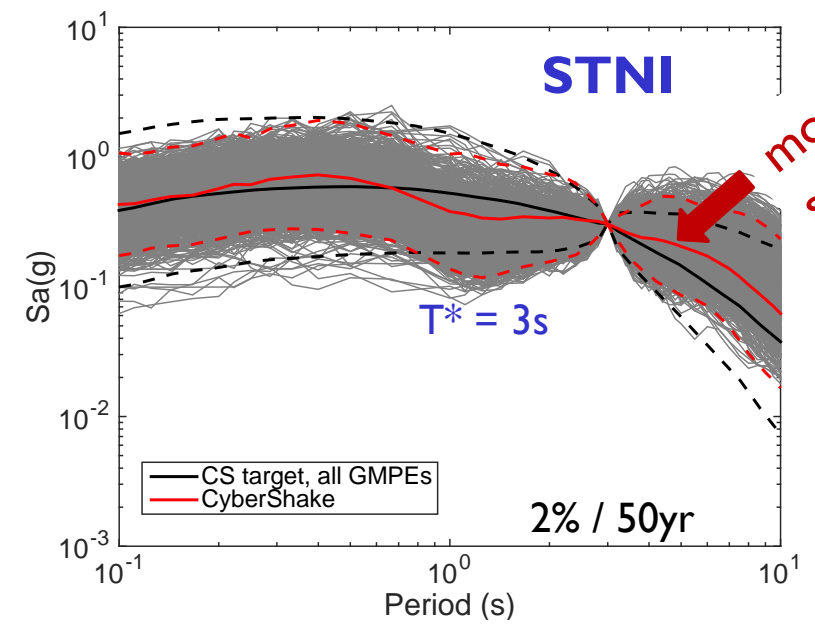
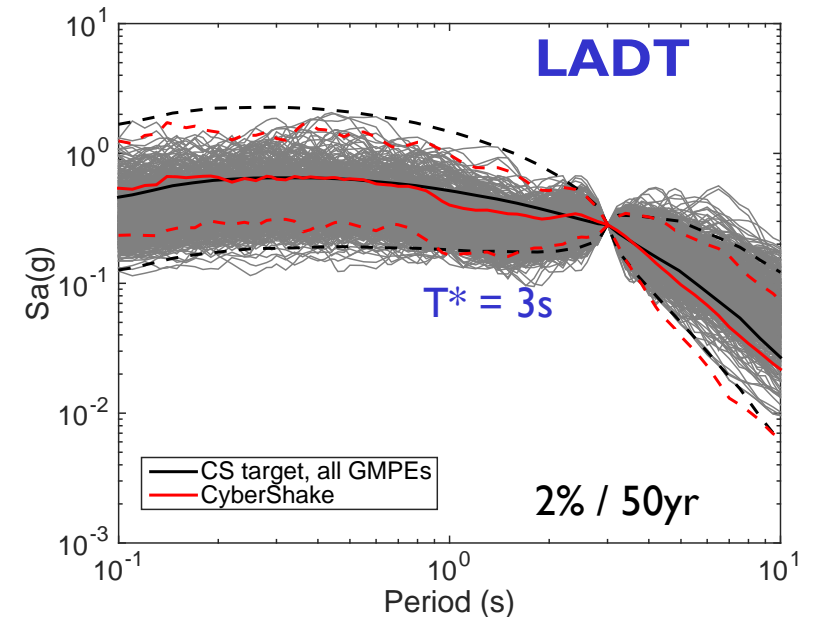
# Direct Simulation with CyberShake



## Deep Basin Site

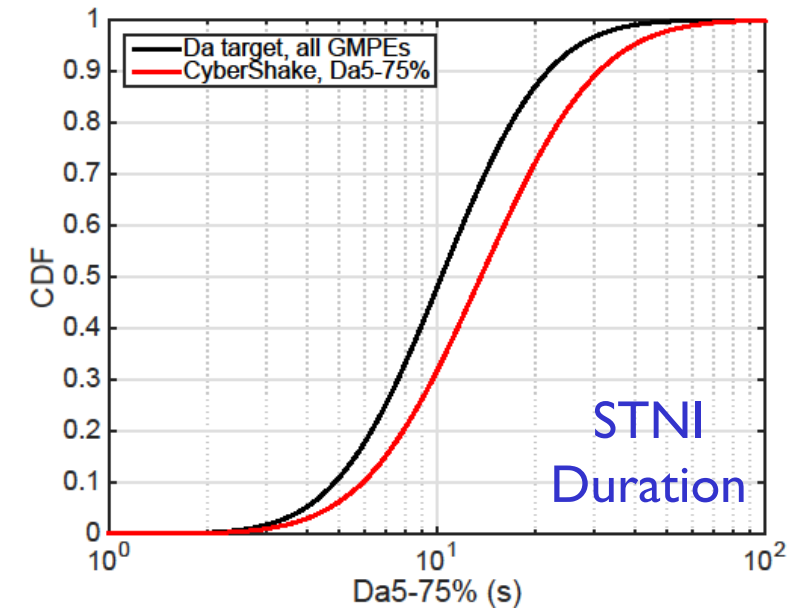
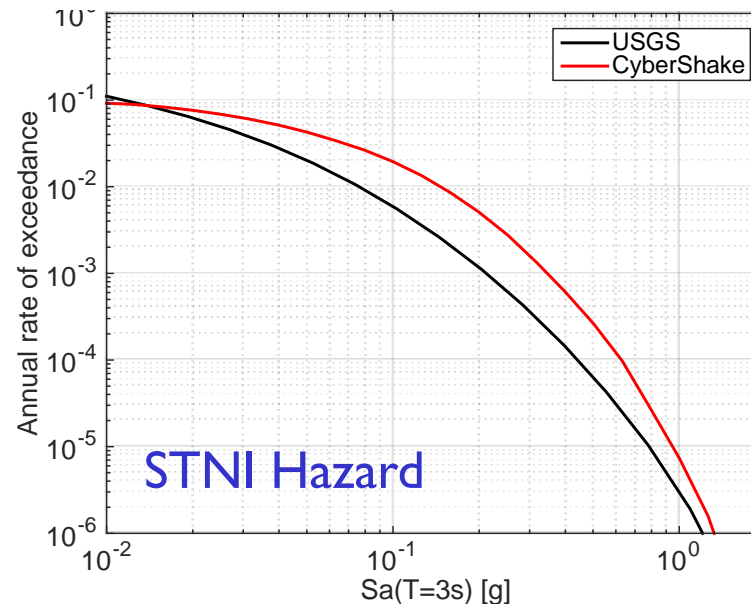
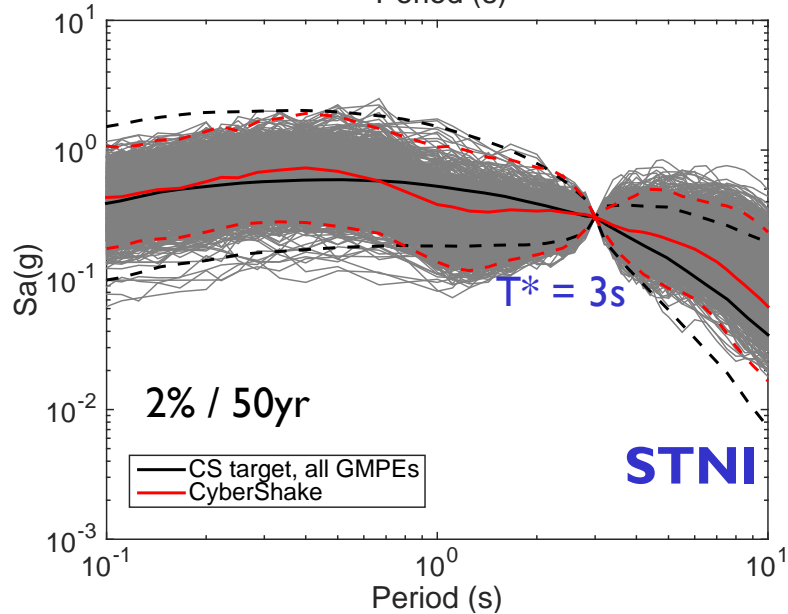
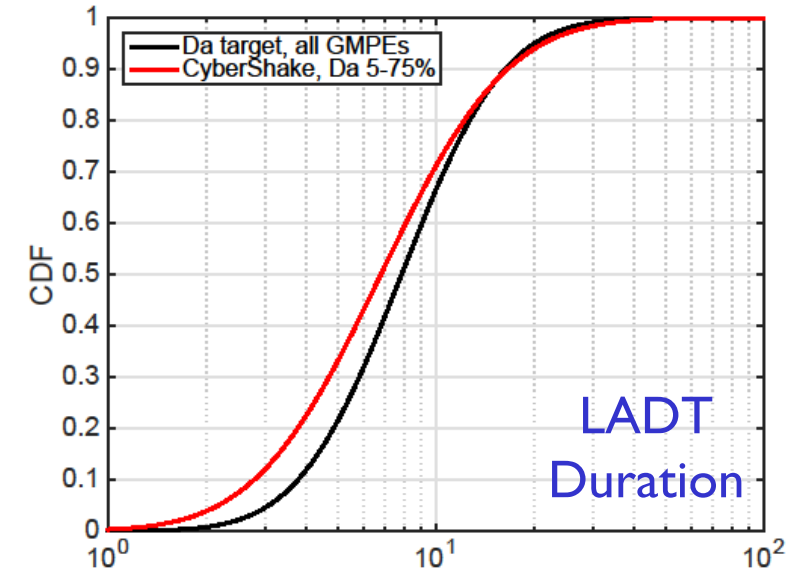
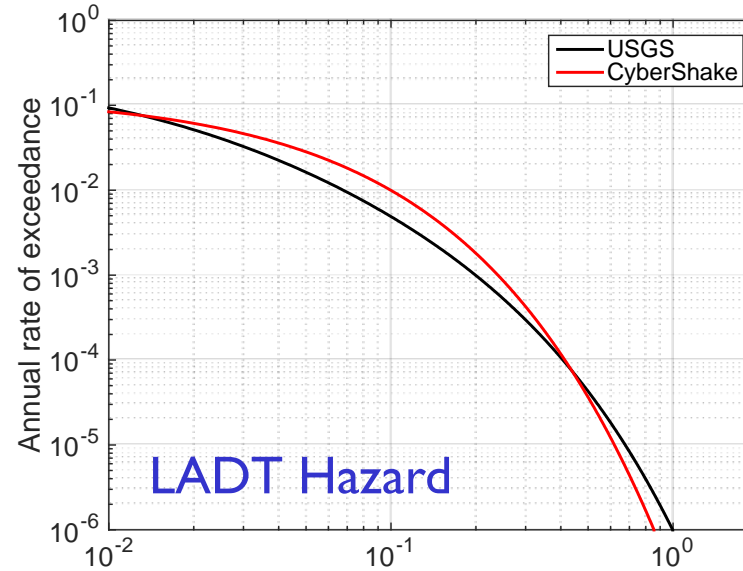
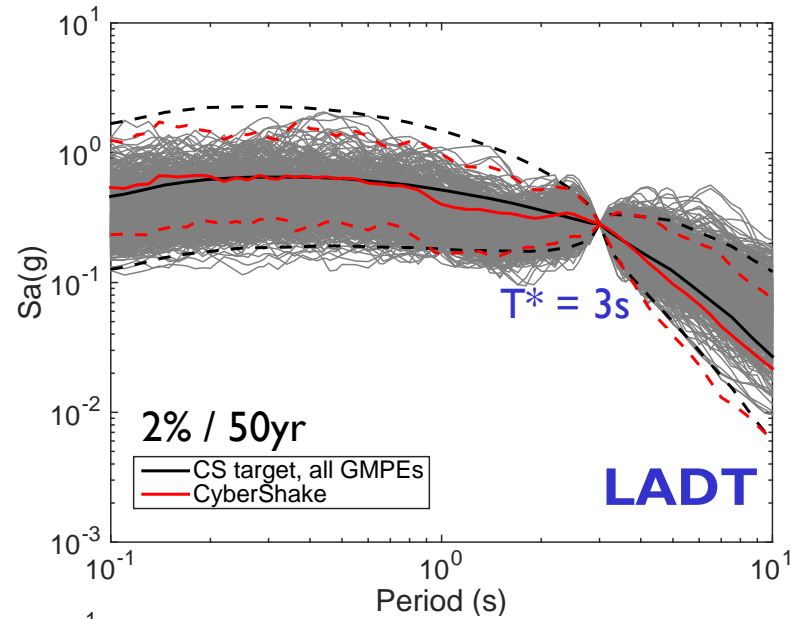
**LADT:**  $V_{s30} = 390$  m/s;  $Z_{1.0} = 0.3$  km

**STNI:**  $V_{s30} = 280$  m/s;  $Z_{1.0} = 0.9$  km



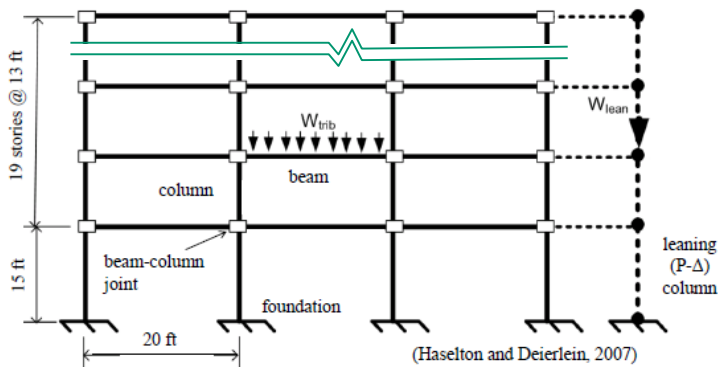
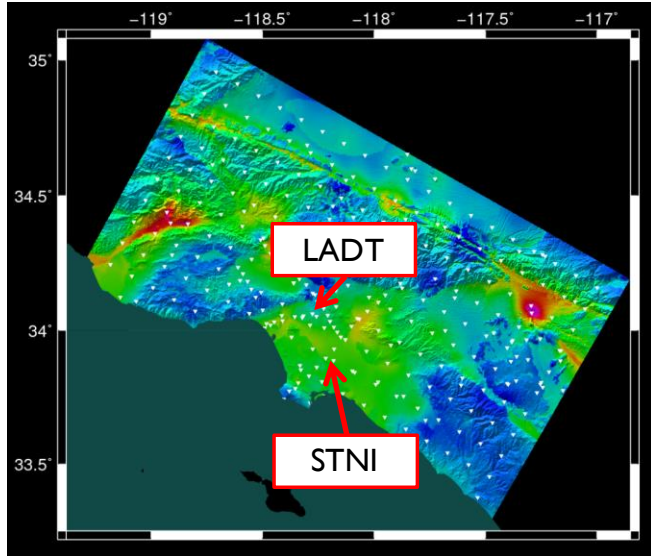
more damaging  
spectra than  
CS target

# Direct Simulation with CyberShake

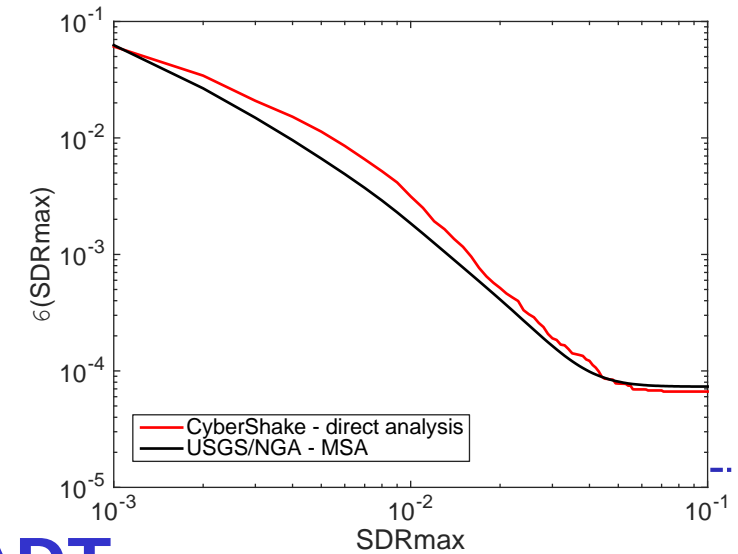
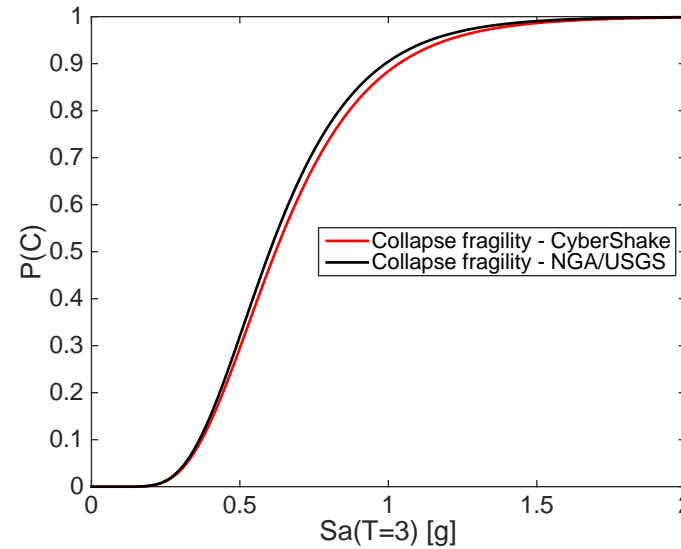




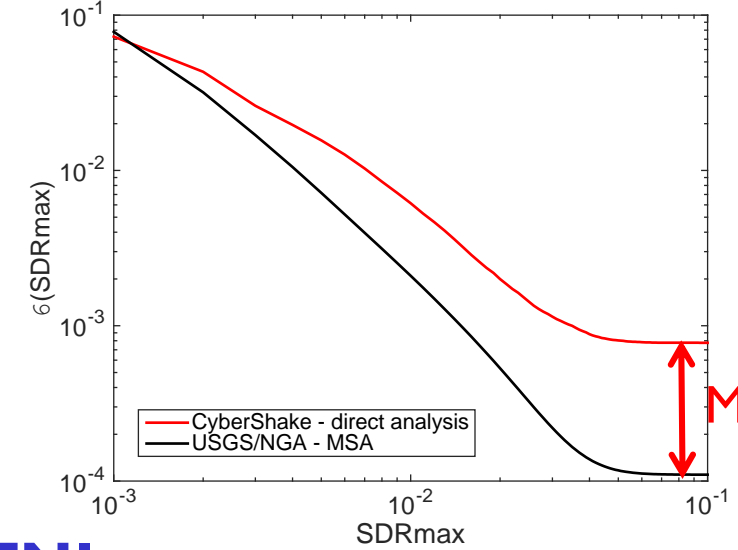
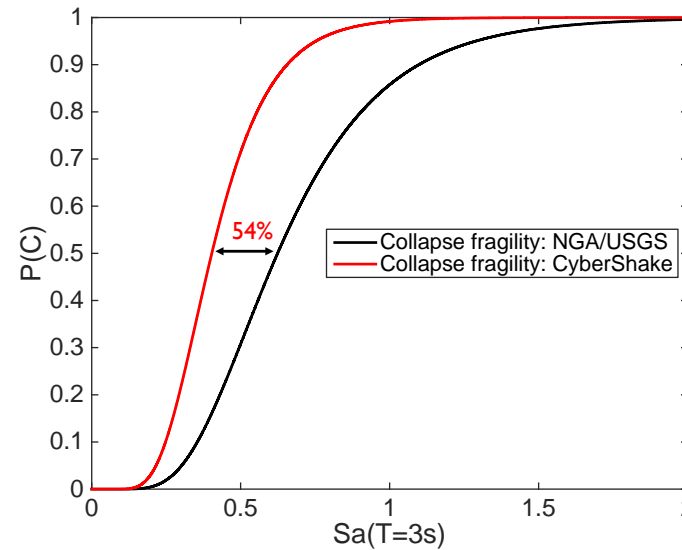
# CyberShake: LA downtown vs STNI sites



20-story building,  $T_1 = 2.60s$



**LADT**



**MAF<sub>c</sub> 10x**

**STNI**

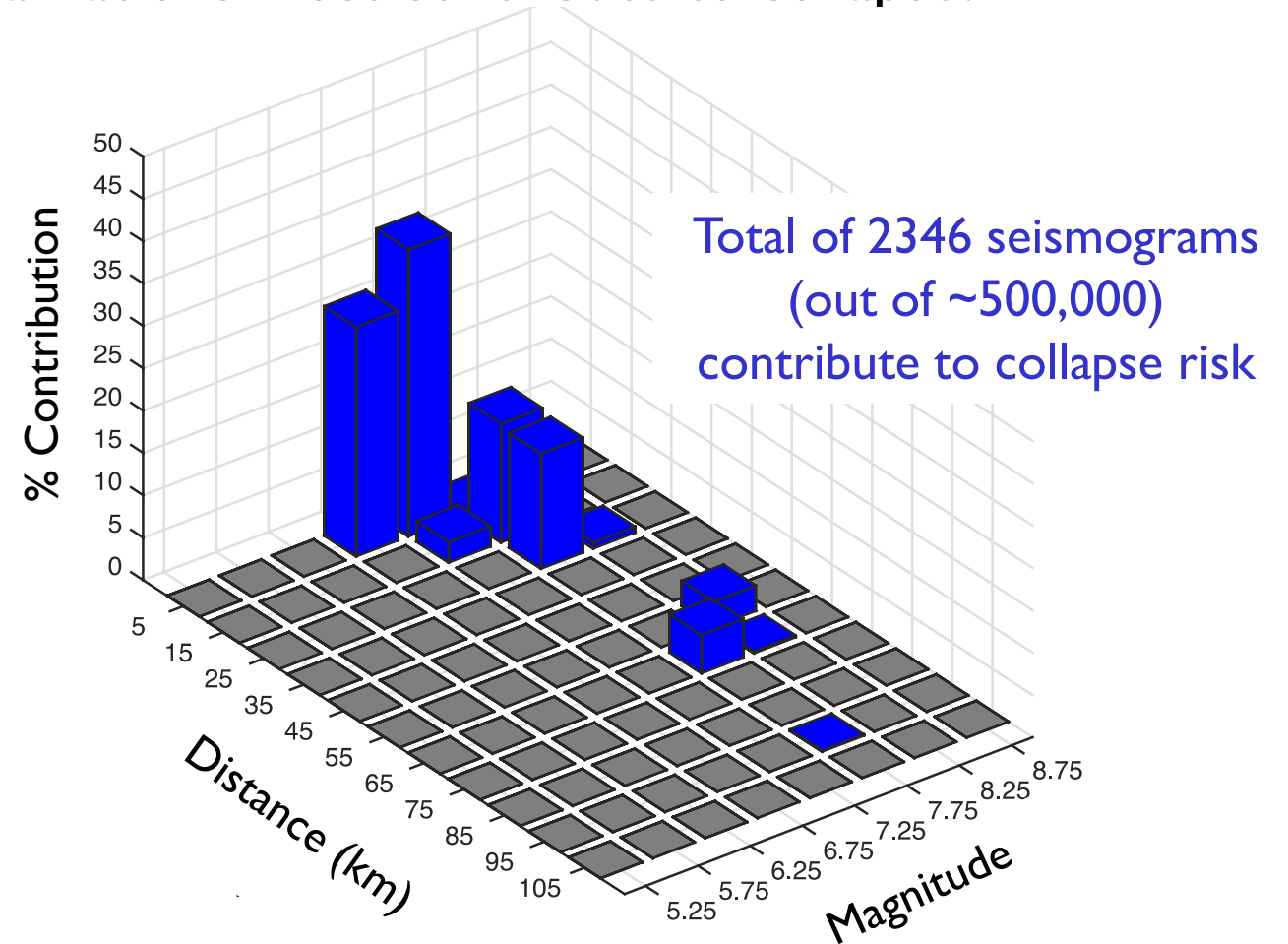
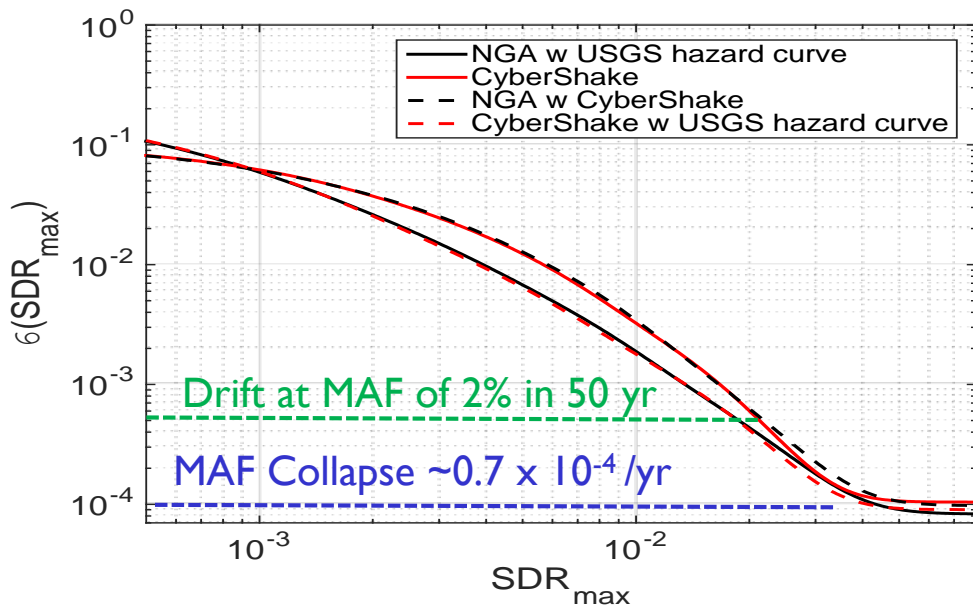
**Collapse Fragility**

**Story Drift Exceedence**

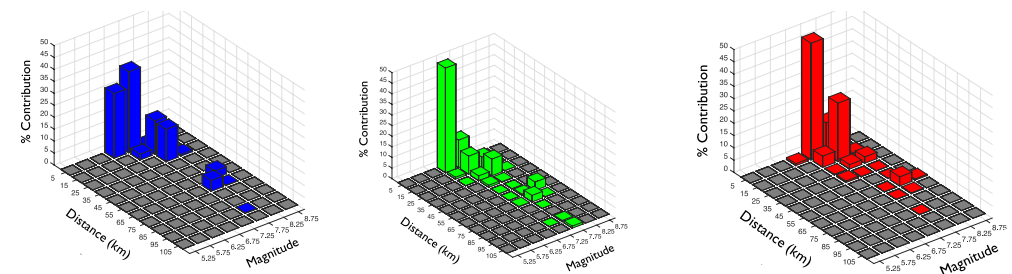
# CyberShake: Deaggregation of Risk

## Deaggregation of Risk:

Which earthquake faults and rupture realizations most contribute to collapse?



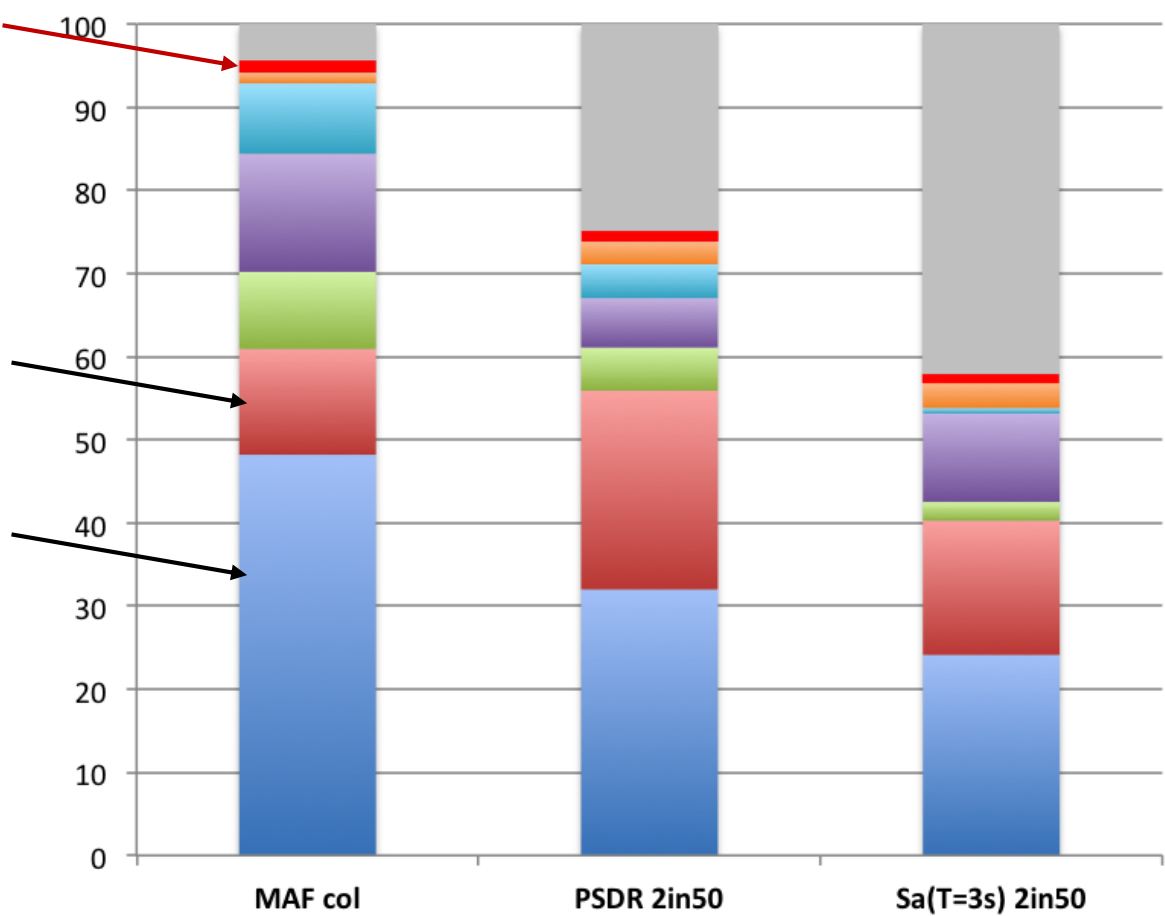
# CyberShake: Deaggregation of Risk versus Hazard



San Andreas

Raymond

Puente Hills

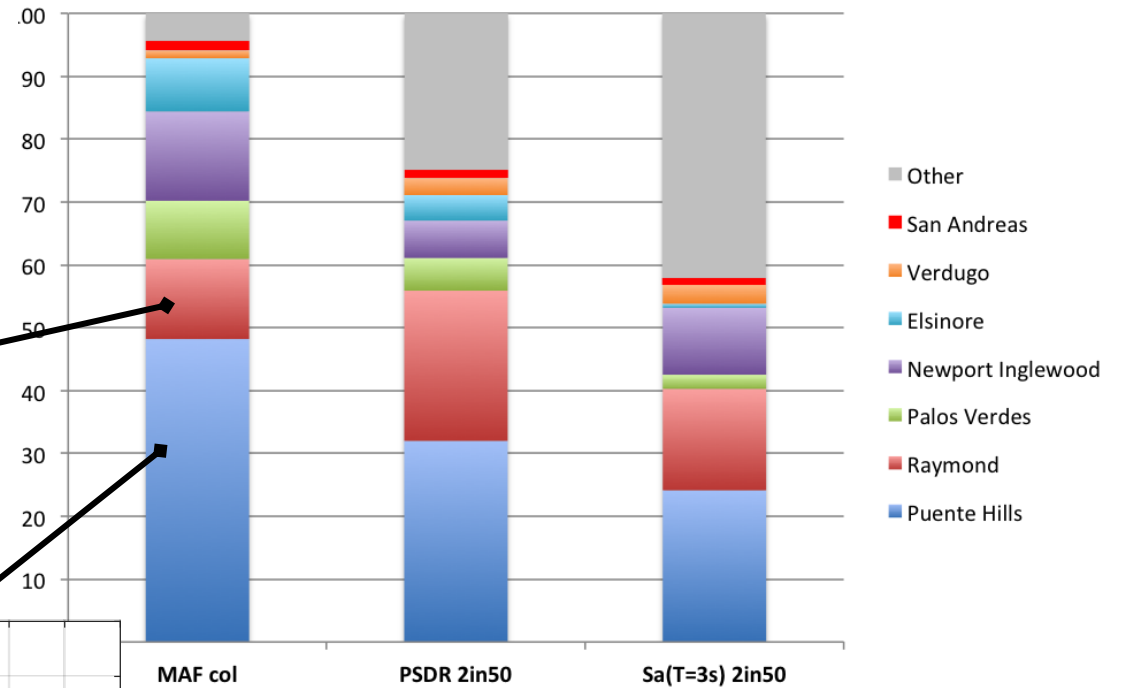
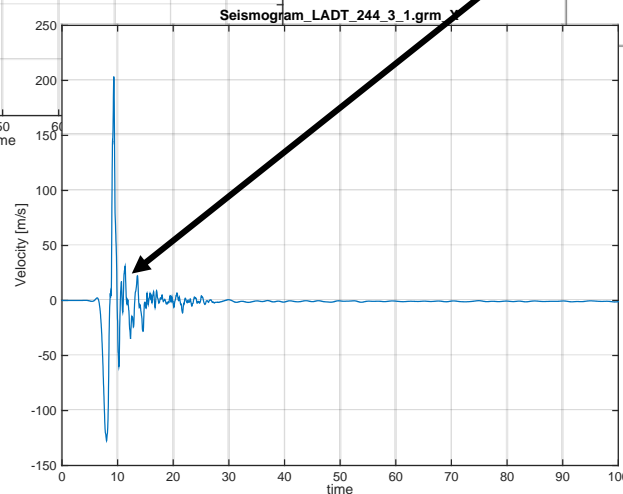
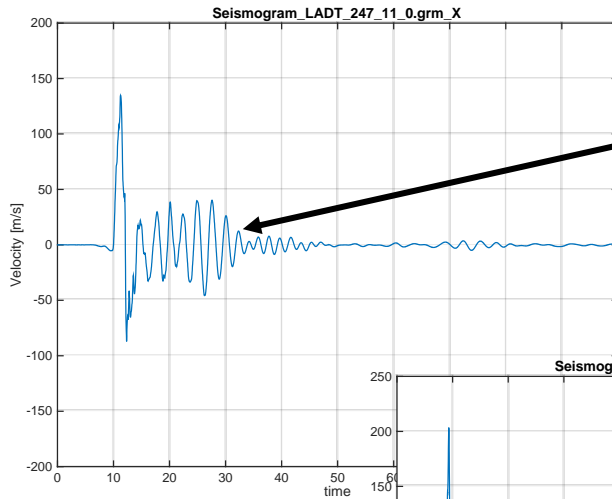


- Other
- San Andreas
- Verdugo
- Elsinore
- Newport Inglewood
- Palos Verdes
- Raymond
- Puente Hills



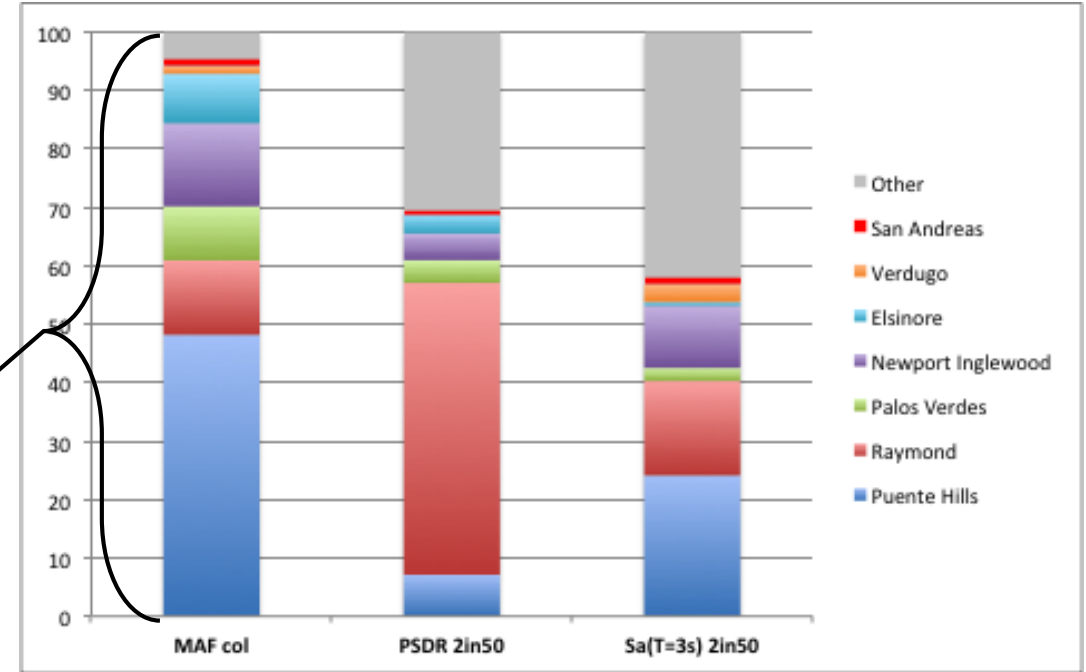
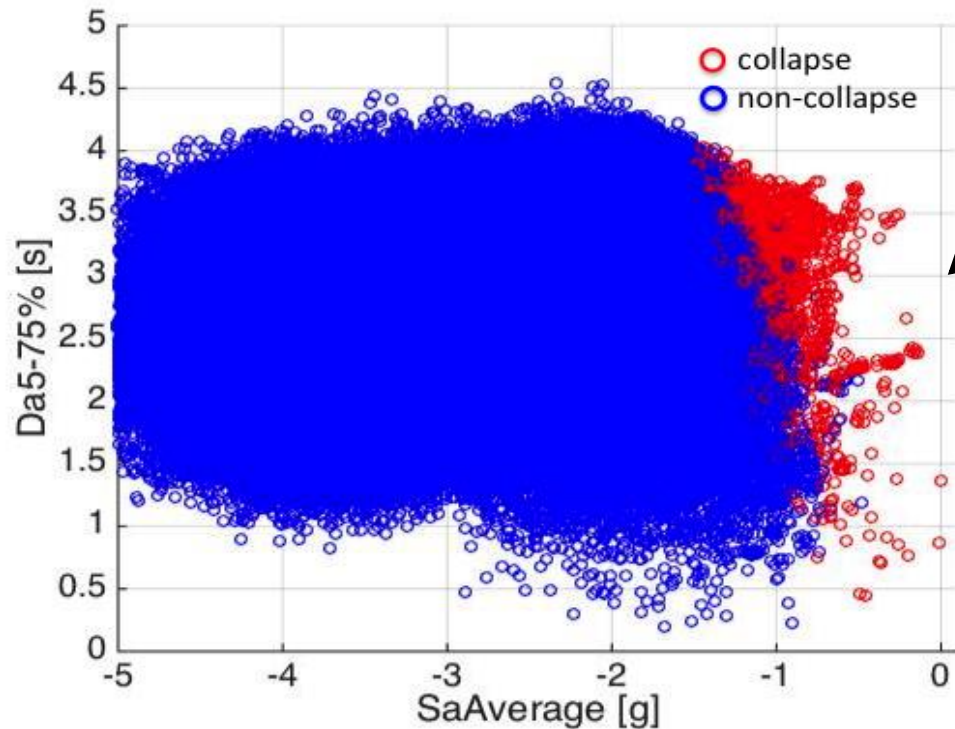
# CyberShake: Characterization of Damaging Ground Motions

What are the characteristics of the ground motions generated by the faults that contribute to collapse?



# CyberShake: Characterization of Damaging Ground Motions

What are the characteristics (*intensity measures*) of the ground motions that contribute to collapse?



Opportunities to utilize machine learning techniques to interrogate **large *site specific* data sets**, identify damaging ground motion characteristics, and relate them to features of the geology and EQ simulation.

# Concluding Thoughts

- Utilization of Simulated Motions
  - IF records are selected and scaled to comprehensive targets ( $S_a$ ,  $C_S$ ,  $D_s$ , correlation/skew), the resulting response is similar between recorded and simulate motions
  - BBP motions and GMPE targets match well up to: 2/200yr - SF, 2/50yr - LADT, 10/50 – SB
  - **Simulated GM's (based on representative events) require less scaling; considered to be more realistic**
  - ASCE 7 emphasis on causal features (fault type, M,R..) and scaling limits help to capture GM characteristics, BUT limit the number of available GM's
- Simulations are most useful where they:
  - Provide **different answers** compared to conventional methods (PSHA w/recorded motions)
  - Address situations that are **outside the range** of conventional methods (large near fault M; basin effects, directivity, etc.).
- Continuing studies
  - Quantitative validation is important, but can only go so far
  - Role of risk deaggregation and sensitivity studies to highlight important features of EQ simulations
  - More education and transparency in confidence in models and assumptions